

SECOND QUARTER MONITORING REPORT

APRIL TO JUNE 2003

KIN-BUC LANDFILL OPERABLE UNITS 1 AND 2

Prepared for

SCA Services, Inc. Edison Township, Middlesex County, New Jersey

July 2003

Prepared by

EMCON/OWT, Inc. Crossroads Corporate Center One International Boulevard, Suite 700 Mahwah, New Jersey 07495

OWT Project 791186



SECOND QUARTER MONITORING REPORT APRIL TO JUNE 2003

KIN-BUC LANDFILL OPERABLE UNITS 1 AND 2

Prepared for

SCA Services, Inc. Edison Township, Middlesex County, New Jersey

July 2003

Prepared by

EMCON/OWT, Inc. Crossroads Corporate Center One International Boulevard, Suite 700 Mahwah, New Jersey 07495

OWT Project 791186

CONTENTS

| LI | ST OF 1 | FABLES AND ILLUSTRATIONS | i |
|-----|---------|--|------------|
| SU | MMAR | Υ | |
| 1 | INT | RODUCTION | 1-1 |
| 2 | DES | SCRIPTION OF MONITORING PROGRAM | 2-1 |
| | 2.1 | Hydrogeologic background | 2-1 2-1 |
| | 2.2 | Remedial Objectives | 2-1 |
| | 2.3 | Hydraulic Control and Monitoring System | 2-1 |
| | 2.4 | Second Quarter Hydraulic Monitoring Activities | 2-2 |
| | 2.5 | Continuous Hydraulic Monitoring Results vs. Manual Elevation | 2-3 |
| | | Measurements | 2-4 |
| 3 | HYI | DRAULIC MONITORING | 3-1 |
| | 3.1 | Assessment of Hydraulic Conditions in the Refuse Unit | 3-1 3-1 |
| | 3.2 | Assessment of Hydraulic Conditions in the Sand & Gravel Unit | 3-1 3-2 |
| | 3.3 | OU2 Hydraulic Monitoring | 3-2 |
| 4 | LEA | CHATE WITHDRAWAL/GROUNDWATER PUMPING | 4-1 |
| 5 | LAN | DFILL GAS MIGRATION MONITORING | 5-1 |
| | 5.1 | Landfill Gas Migration | 5-1 |
| | 5.2 | Gas Monitoring Well Results | 5-1 5-1 |
| | 5.3 | Operational Flare Monitoring Results | 5-2 |
| 6 | CON | CLUSIONS | 6-1 |
| REF | ERENC | CES | |
| FIG | URES | | |
| DRA | WING | | |
| | T DO | | |

CONTENTS (Continued)

APPENDIX A - OU1 REFUSE WELLS CONTINUOUS WATER LEVEL MONITORING RESULTS

APPENDIX B - MONTHLY HYDRAULIC EVALUATIONS

TABLES AND ILLUSTRATIONS

Tables

- 2-1 OU1 Hydraulic Monitoring Well Network/Transects
- 2-2 OU2 Hydraulic Monitoring Network
- 2-3 Second Quarter 2003 Manually Recorded Water Levels
- 2-4 Minimum/Maximum Monthly Water Elevations
- 2-5 Troll Water Level Elevations vs. Manual Water Elevations
- 2-6 Leachate Cleanout Monitoring
- 5-1 Landfill Gas Migration Monitoring Well Network/Results

Figure

1-1 OU2 Groundwater Monitoring Locations

Drawing

1-1 OU1 Site Map

In map pocket

EXECUTIVE SUMMARY

The Kin-Buc Landfill Site is a closed 200-acre industrial/commercial landfill located in Edison, New Jersey, which the USEPA placed on the National Priorities List (NPL) in 1981. A Remedial Investigation/Feasibility Study (RI/FS) was conducted between 1983 and 1988 which resulted in a Record of Decision (ROD) by USEPA in 1990 that called for source control of Operable Unit 1 (OU1).

The remedial action specified in the ROD for OU1 included the construction of a slurry wall around OU1, the collection and treatment of leachate and groundwater from within the containment area, and the capping of the area within the slurry wall. Remedial construction activities for OU1 were completed by the end of August 1995.

In accordance with the RODs, hydraulic monitoring and landfill gas monitoring is conducted on a quarterly basis to evaluate the effectiveness of the remedial actions. This report documents the results of the monitoring activities for the Second Quarter of 2003.

Remedial Objectives

The general remedial objectives of the OU1 closure and collection systems are to contain source leachate and contaminated groundwater, and to prevent further migration of site-related contaminants. The primary objective of the leachate collection system is to impose an inward gradient as measured across the slurry wall in the refuse unit. The primary objectives of the groundwater collection system are to prevent migration of contaminated groundwater towards the slurry wall and impose an upward gradient from the bedrock unit to the sand & gravel unit.

Hydraulic Control and Monitoring System

The hydraulic control system for OU1 consists of leachate and groundwater collection systems. The leachate collection system consists of a perforated pipe that runs parallel to the inside of the perimeter slurry wall and 4 pump stations. The groundwater collection system consists of 4 pumping wells.

The hydraulic monitoring system for OU1 is located along the circumferential slurry wall with many of the wells located in 5 clusters, called transects. The hydraulic monitoring wells at the transects are installed in pairs, within the same hydrogeologic unit, with

1 well inside and 1 well outside the circumferential slurry wall. Twenty-four of the monitoring wells are continuously monitored using water level recorders.

The hydraulic monitoring network consists of wells screened in the refuse, sand & gravel, and bedrock units. Well designations of G, S or R; denote hydraulic units of refuse, sand & gravel or bedrock, respectively.

The OU2 hydraulic monitoring well network is located in the Low-Lying Area and Mound B, and monitors groundwater elevations outside of the OU1 containment area.

Second Quarter Hydraulic Monitoring Activities

Hydraulic monitoring was performed during the period from April through June 2003.

Hydraulic monitoring indicates that intragradient conditions in the refuse unit (lower water levels in the refuse inside the wall relative to water levels outside the wall) were maintained at TL Nos. 1, 2, 3, 4 and 5, throughout the quarter. The fact that the leachate collection system is functioning properly suggests that intragradient conditions are being maintained in the refuse unit at TL No. 1, even though review of the hydrographs has not consistently indicated this condition in the past (However, intragradient conditions were maintained throughout this quarter at TL No. 1). Water level elevation measurements taken from Leachate Collection Cleanout Nos. 14 through 16 are included in Table 2-6, and indicate that the leachate collection system is functioning properly.

Hydraulic control was maintained within OU-1 based on the analysis of the significant influence of S&G #2 in acting as a hydraulic sink for sand and gravel and bedrock groundwater. Groundwater flow in the sand and gravel and bedrock is ultimately captured by the pumping well resulting in overall containment of groundwater in OU-1.

Leachate Withdrawal/Groundwater Pumping

The second quarter average daily groundwater extraction rate for all of the wells was 16,025 gpd. The total volume of groundwater collected for the quarter was 1,458,291 gallons. Leachate was collected at an average daily rate of 1,637 gpd for the quarter, and the total volume of leachate collected was 148,959 gallons.

Landfill Gas Monitoring

Combustible gas was not detected in any of the 6 gas monitoring wells located on the north side of OU1. Based on the non-detection of combustible gas in the monitoring wells, the active gas collection system is functioning properly and there is no apparent off-site gas migration. Monitoring at the flare inlet port by landfill personnel throughout the quarter indicated that the landfill gas collection system was delivering an average of 44.2 percent combustible gas to the flare.

1 INTRODUCTION

The Kin-Buc Landfill Site is a closed 200-acre industrial/commercial landfill located in Edison, New Jersey, which operated under a New Jersey Department of Environmental Protection (NJDEP) permit until 1976. The USEPA placed the Kin-Buc Landfill on the National Priorities List (NPL) in 1981. Between 1983 and 1988, the Respondents conducted a Remedial Investigation/Feasibility Study (RI/FS) which resulted in a Record of Decision (ROD) by USEPA in 1990 which called for source control of Operable Unit 1 (OU1), and an additional RI/FS to determine the nature and extent of contamination outside the source area, thus defining Operable Unit 2 (OU2).

Operable Unit 1 includes both Kin-Buc I and II Mounds, the former Pool C Area and a portion of the Low-Lying Area between Kin-Buc I and the Edison Landfill. The remedial action specified in the ROD for OU1 included the construction of a slurry wall around OU1, the collection and treatment of leachate and groundwater from within the containment area, and the capping of the area within the slurry wall.

Operable Unit 2 includes Mound B, Edmonds Creek and adjacent wetlands, the remaining Low-Lying Area between OU1 and the Edison Landfill, Martins Creek, and the Raritan River. The OU2 ROD called for the excavation and disposal of PCB-contaminated sediments from within the Edmonds Creek Marsh Area, the restoration of disturbed wetland areas, and groundwater/surface water monitoring.

Remedial construction activities for both OU1 and OU2 were completed by the end of August 1995.

In accordance with the RODs, hydraulic monitoring and landfill gas monitoring is conducted quarterly to evaluate the effectiveness of the remedial actions. This report documents the results of the monitoring activities for the Second Quarter of 2003.

2 DESCRIPTION OF MONITORING PROGRAM

2.1 Hydrogeologic background

The primary hydrogeologic units within OU1 from ground surface downward are refuse, meadow mat, sand & gravel, and bedrock. Near the northern portion of the site the bedrock is closer to the surface and there is no sand & gravel unit in that area.

The southern portion of the site is located in close proximity to the Raritan River. As a result, monitoring wells located on the southern side of OU1 are impacted by tidal fluctuations.

2.2 Remedial Objectives

The general remedial objectives of the OU1 closure and collection systems are to contain source leachate and contaminated groundwater, and to prevent further migration of site-related contaminants. The specific remedial objectives for the leachate collection, groundwater collection, and hydraulic monitoring are summarized as follows:

Aqueous Leachate Collection

- Primary
- Collect leachate from the refuse unit within the perimeter slurry wall to impose an inward gradient as measured across the slurry wall (hydraulic containment).
- Additional Benefit
 - Reduce the downward gradient between the refuse unit and the underlying sand & gravel or bedrock units.

Sand & Gravel Groundwater Collection (in Primary OU1 Containment)

- Primary
 - Prevent migration of contaminated groundwater towards the slurry wall.
- Impose an upward gradient from the bedrock unit to the sand & gravel unit (hydraulic containment).
- Additional Benefit
 - Impose an inward gradient within the sand & gravel unit as measured across
 the perimeter slurry wall (hydraulic containment).

Sand & Gravel Aquifer Groundwater Collection (in Oil Seeps Area Containment)

 Collect sand & gravel groundwater from within the Oil Seeps Area if an upward gradient between the sand & gravel and the refuse units cannot be imposed by leachate collection alone.

2.3 Hydraulic Control and Monitoring System

The hydraulic control system for OU1 consists of 4 leachate pump stations and 4 sand & gravel groundwater pumping wells. The leachate collection system consists of a perforated pipe that runs parallel to the inside of the perimeter slurry wall. In addition, a corrugated oily leachate collection conduit is located along the south side of Kin-Buc I mound. The layout of the collection system is shown on Drawing 1.

The hydraulic monitoring system for Operable Unit 1 is located along the circumferential slurry wall with many of the wells located in 5 clusters, called transects. The OU1 hydraulic monitoring well network consists of 11 wells screened in the refuse/fill, 8 wells screened in the sand & gravel, and 10 wells screened within bedrock. A summary of the well network is provided in Table 2-1, and the well locations are shown on Drawing 1.

The hydraulic monitoring wells at the transects are installed in pairs, within the same hydrogeologic unit, with 1 well inside and 1 well outside the circumferential slurry wall. The design of the well network allows groundwater elevations to be monitored on either side of the slurry wall and provides data to evaluate the performance of the slurry wall as a hydraulic barrier.

At TL Nos. 2, 3 and 4, the hydraulic monitoring wells are installed in the refuse, sand & gravel, and bedrock units. At TL Nos. 1 and 5, the hydraulic monitoring wells are installed only in the refuse and bedrock units due to the absence of sand and gravel

deposits in these areas. Well designations of G, S and R, denote hydraulic units of refuse, sand & gravel, and bedrock, respectively.

The OU2 hydraulic monitoring well network is located in the Low-Lying Area and Mound B, and monitors groundwater elevations outside of the OU1 containment area. The hydraulic monitoring system for OU2 consists of 16 wells, as indicated in Table 2-2 and as shown on Figure 1-1. Water elevation measurements from the OU2 wells are taken manually, concurrent with the OU1 monitoring activities.

2.4 Second Quarter Hydraulic Monitoring Activities

Hydraulic monitoring for the Second Quarter of 2003 (April to June) took place according to the procedures and methods outlined in the Draft Operations and Maintenance (O&M) Manual for the Kin-Buc Landfill, prepared on behalf of the Respondents by Wheelabrator EOS in September 1995 and modified by a letter to EPA dated February 28, 1996.

Components of the hydraulic monitoring program consist of continuous and manual water level measurements. Manual measurements were obtained with an electronic water level indicator. Continuous water levels were obtained at 1-hour intervals using 24 In-Situ "miniTROLL", Model SSP-100 data loggers and transducers.

Alkaline batteries were replaced with lithium batteries in each of the miniTROLLS during the last quarter. Since the batteries were changed out and the weather has been more mild, there has not been any maintenance issues with the miniTROLLS. The SP4000 Troll is being used to collect data at Well 15G until the dedicated miniTroll is repaired. In-Situ, Inc. Representative, Jason Evans, was contacted regarding the status of the dedicated miniTroll (serial no. 6559). The miniTroll has been repaired (replaced circuit board) and is being shipped out on July 29, 2003. Information regarding maintenance of the miniTROLLS can also be found in the attached Hydraulic Monitoring Reports for each month (Appendix B).

Three months of continuous water level data have been obtained from the refuse and sand & gravel wells at the site from April 1, 2003 to June 30, 2003. The minimum, maximum, and average recorded water elevations for each month in the quarter are provided in Table 2-4. Continuous groundwater elevation graphs organized by transect location and hydrogeologic unit are provided in Appendix A. Evaluations of the recorded data are performed on a monthly basis and sent to Waste Management. Copies of these monthly evaluations are provided in Appendix B.

Manual groundwater elevation measurements were obtained from the monitoring wells in OU1 and OU2 during site visits on April 1, 2003, May 8, 2003, and June 3 & 30, 2003. The manually recorded water level monitoring results are provided in Table 2-3.

2.5 Continuous Hydraulic Monitoring Results vs. Manual Elevation Measurements

The continuous water level monitoring information collected by the Trolls was compared with the data collected from the manual recordings to provide information on the relative accuracy of manual versus automatic recordings. Table 2-5 shows the difference between the manual water level elevation measurements and Troll recordings for the same day and hour. The average differences between the manual and continuous measurements were at or below 0.3 feet for all wells. Based on the comparison above, the data recorded by the Trolls is satisfactory and reflects accurate groundwater elevations.

3 HYDRAULIC MONITORING

The following presents an evaluation of the results of hydraulic monitoring performed during the second quarter 2003.

3.1 Assessment of Hydraulic Conditions in the Refuse Unit

As defined in the Record of Decision (ROD) for OU-1, the performance objective for the refuse unit calls for the pumping of leachate to establish inward gradients across the slurry wall with the additional benefit of reducing downward flow into the underlying sand and gravel unit. Based on the hydrographs the following is presented.

TL No. 1 (Well 1G/Well 2G) - Hydrograph No. 1

Intragradient conditions were observed throughout the quarter. The average quarterly water elevations for Wells 1G (inside) and 2G (outside) were 11.26 and 12.12 feet msl, respectively. The average head elevation difference between the two wells was approximately 0.86 feet in an inward direction. High water levels in Well 1G have been observed on several previous occasions and may be related to localized conditions around the well.

Water level elevation measurements taken from Leachate Collection Cleanout Nos. 14 through 16 are included in Table 2-6, and indicate that the leachate collection system is functioning properly. The water level elevations observed for Leachate Collection Cleanouts 14 through 15 during the second quarter are all between 9.42 and 9.95 feet msl, and the water level elevations for Cleanouts 16N and 16E were dry (less than the cleanouts invert elevation). This indicates that groundwater flow at this location is from the inside to the Leachate Collection Cleanouts. The leachate collection system is therefore functioning properly and suggests significant capture of leachate. Appendix B (Monthly Hydraulic Evaluations) provides an analysis of the hydraulic performance at Transect 1.

TL No. 2 (Well 3G/Well 4G) - Hydrograph No. 2

Intragradient conditions were maintained at TL No. 2 in the refuse unit throughout the quarter. The average quarterly water elevations for Wells 3G (inside) and 4G (outside)

were 7.36 and 11.45 feet msl, respectively. The average head elevation difference between the two wells was approximately 4.09 feet in an inward direction.

TL No. 3 (Well 5G/Well 6G) - Hydrograph No. 3

Intragradient conditions were maintained at TL No. 3 in the refuse unit throughout the quarter. The average quarterly water elevations for Wells 5G (inside) and 6G (outside) were 9.84 and 13.58 feet msl, respectively. The head elevation difference between the two wells was approximately 3.74 feet in an inward direction.

TL No. 4 Well 15G/Well 13G) Oil Seeps Area – Hydrograph No. 4

Intragradient conditions were maintained at TL No. 4, Oil Seeps Area, in the refuse unit throughout the quarter. The average quarterly water elevations for Wells 15G (inside) and 13G (outside) were 1.52 and 6.73 feet msl, respectively. The head elevation difference between the two wells was approximately 5.21 feet in an inward direction.

TL No. 5 (Well 9G/Well 10G) - Hydrograph No. 5

Intragradient conditions were maintained at TL No. 5 in the refuse unit throughout the quarter. The average quarterly water elevations for Wells 9G (inside) and 10G (outside) were 7.46 and 8.47 feet msl, respectively. The average head elevation difference between the two wells was approximately 1.01 feet in an inward direction.

3.2 Assessment of Hydraulic Conditions in the Sand & Gravel Unit

For the sand and gravel unit, the performance objectives call for pumping of sand and gravel groundwater to prevent flow toward the slurry wall and to impose upward hydraulic gradients from the bedrock to the sand and gravel. An additional benefit would be the establishment of inward gradients across the slurry wall within the sand and gravel unit. The following is a description of the flow characteristics based on visual observation of the hydrographs.

Horizontal Flow

TL No. 2 (Well 3S/Well 4S) - Hydrograph No. 6

Although intragradient conditions were not consistently observed throughout the quarter, they were evident for majority of the quarter. It is evident that containment is being maintained by pumping wells SG-2 and SG-3 (as described below in Section 3.2.1). The average quarterly water elevations for Wells 3S (inside) and 4S (outside) were 1.03 and

1.25 feet msl, respectively. The average head elevation difference between the two wells was approximately 0.22 feet in an inward direction.

TL No. 3 (Well 5S/Well 6S) - Hydrograph No. 7

Slight intragradient conditions were maintained at TL No. 3 in the sand & gravel unit throughout the quarter. The average quarterly water elevation for Wells 5S (inside) and 6S (outside) were 1.88 and 1.94 feet msl, respectively. The head elevation difference between the two wells was approximately 0.06 feet in an inward direction.

TL No. 4 (Well 7S/Well 8S) - Hydrograph No. 8

Intragradient conditions were maintained at TL No. 4 in the sand & gravel unit throughout the quarter. The average quarterly water elevation for Wells 7S (inside) and 8S (outside) was 1.99 and 2.70 feet msl, respectively. The head elevation difference between the two wells was approximately 0.71 feet in an inward direction.

TL No. 4 (Well 15S/Well 13S) Oil Seeps Area - Hydrograph No. 9

Intragradient conditions are being maintained by pumping wells SG-2 and SG-3 although these conditions were not evident by the head elevations for the quarter (see Section 3.2.1). The average quarterly water elevations for Wells 15S (inside) and 13S (outside) were 2.68 and 2.46 feet msl, respectively. The head elevation difference between the two wells was approximately 0.22 feet in an outward direction. Water levels from Well 15G are included in the hydrograph for comparison.

Vertical Flow

TL No. 2 (Well 3S/Well 3RR) - Inside; (Well 4S/Well 4R) - Outside Hydrograph Nos. 10 and 11

Although upward gradient conditions were not consistently observed between the bedrock and overlying sand & gravel units inside the slurry wall at TL No. 2 throughout the quarter, containment is still maintained by pumping wells SG-2 and SG-3 (see Section 3.2.1). The average quarterly water elevation for Well 3S (sand & gravel) and 3RR (bedrock) was 1.03 and 0.96 feet msl, respectively. The difference in average quarterly water elevations was approximately 0.07 feet in a downward direction.

Containment is being maintained by pumping wells SG-2 and SG-3 even though the elevations do not reflect upward gradient conditions between the bedrock and overlying sand & gravel units outside the slurry wall (see Section 3.2.1). The average quarterly water elevation for Wells 4S (sand & gravel) and 4R (bedrock) was 1.25 and 1.14 feet msl, respectively. The difference in average quarterly water elevations was 0.11 feet in an downward direction.

TL No. 3 (Well 5S/Well 5R) – Inside; (Well 6S/Well 6R) – Outside Hydrograph Nos. 12 and 13

Inside the slurry wall at TL No. 3, slight upward gradient conditions were observed between the bedrock and overlying sand & gravel units throughout the quarter. The average quarterly water elevations for Wells 5S (sand & gravel) and 5R (bedrock) were 1.88 and 2.01 feet msl, respectively. The difference in average quarterly water elevations was 0.13 feet in an upward direction.

Outside the slurry wall at TL No. 3, upward gradient conditions were observed between the bedrock and overlying sand & gravel units. The average quarterly water elevations for wells 6S (sand & gravel) and 6R (bedrock) were 1.94 and 2.11, respectively. The difference in average quarterly water elevations was 0.17 feet.

TL No. 4 (Well 7S/Well 7R) – Inside; (Well 8S/Well 8RR) – Outside Hydrograph Nos. 14 and 15

Slight upward gradient conditions were maintained between the bedrock and overlying sand & gravel units inside the slurry wall at TL No. 4 throughout the quarter. The average quarterly water elevations for Wells 7S (sand & gravel) and 7R (bedrock) were 1.99 and 2.09 feet msl, respectively. The difference in average quarterly water elevations was 0.1 feet.

Outside the slurry wall at TL No. 4, containment was achieved through pumping wells SG-2 and SG-3 although the elevations do not reflect upward gradient conditions between the bedrock and overlying sand & gravel units (see Section 3.2.1). Since the average water elevations are so close, a dominant flow direction cannot be established. The average quarterly water elevations for Wells 8S (sand & gravel) and 8RR (bedrock) were 2.70 feet and 2.66 feet msl, respectively. The difference in average quarterly water elevations was 0.04 feet.

3.2.1 Analysis

While initial review of the hydrographs indicate that certain performance objectives may not be met, (uniform achievement of upward gradients from the bedrock to the sand and gravel, and inward gradients across the slurry wall) containment was still maintained this quarter by the pumping well SG-2 with a combination of SG-3, SG-4, or SG-1. Figures 1 through 4 (See Appendix B) depict horizontal or vertical flow vectors within the sand and gravel or bedrock units. These diagrams show that although downward groundwater flow from the sand and gravel to the bedrock may occur locally within the slurry wall, the zone of influence of the pumping wells includes the sand and gravel units and the upper portion of the bedrock within the slurry wall. Regardless of whether groundwater is flowing vertically upward or downward within the slurry wall in the sand and gravel and

upper bedrock, it will eventually migrate toward the pumping wells, and will be captured. Examination of the pumping results indicates that this process is more efficient if SG-3 is pumped in conjunction with SG-2.

3.3 OU2 Hydraulic Monitoring

The synoptic groundwater elevations obtained during the Second Quarter of 2003 indicate both upward and downward hydraulic gradients.

4 LEACHATE WITHDRAWAL/GROUNDWATER PUMPING

The performance of the site hydraulic controls is largely dependent upon groundwater pumping and leachate withdrawal rates. The design aqueous leachate and groundwater (GW) collection rates called for a ratio of 3:1, groundwater to leachate of 30,000 gpd groundwater, and 10,000 gpd leachate. The collection rates differed from the design rates due to variations between design assumptions and actual site conditions. Collection rates are also adjusted based on changing site and operational conditions.

Operation records are maintained at the site and contain estimated daily averages for leachate and groundwater withdrawal. The monthly volumes collected and the daily average collection rate are provided below:

| Monitoring Period | Groundwater S&G No. 1 | Groundwater S&G No. 2 | Groundwater S&G No. 3 | Groundwater S&G No. 4 | Leachate |
|----------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------|
| April | 0 gal. | 330,378 gal. | 122,889 gal. | 0 gal. | 50,252 gal. |
| , | 0 gpd | 11,013 gpd | 4,096 gpd | 0 gpd | 1,675 gpd |
| May | 0 gal. | 398,760 gal. | 51,233 gal. | 28,251 gal. | 43,717 gal. |
| | 0 gpd | 12,863 gpd | 1,652 gpd | 911 gpd | 1,410 gpd |
| June | 2,160 gal. | 466,095 gal. | 38,124 gal. | 20,401 gal. | 54,990 gal. |
| | 72 gpd | 15,537 gpd | 1,271 gpd | 680 gpd | 1,833 gpd |
| Quarter | 2,160 gal. | 1,195,233 gal. | 212,246 gal. | 48,652 gal. | 148,959 gal. |
| | 23.7 gpd | 13,134 gpd | 2,332 gpd | 535 gpd | 1,637 gpd |

The volume of groundwater collected in the first quarter is 1,458,291 gallons. The average daily groundwater withdrawal rate for the first quarter is 16,025 gpd.

5 LANDFILL GAS MIGRATION MONITORING

Landfill gas migration monitoring was performed at the operational flare port inlet and the 6 gas migration monitoring wells located along the northern edge of the landfill boundary.

5.1 Landfill Gas Migration

The purpose of the gas migration monitoring program is to monitor for off-site gas migration in those areas where gas migration or accumulation could lead to explosive conditions. Six gas migration monitoring wells are located outside of the circumferential slurry wall along the northern edge of the landfill boundary. The well locations are depicted on Drawing 1 and are spaced in 200-foot increments.

All areas of OU1 exterior to the slurry wall contain waste materials except along the northern edge of the landfill boundary. High levels of gas are not expected to be detected along the northern boundary because the slurry wall will act as an effective barrier, and the presence of an active gas extraction system and the high water table will inhibit gas migration.

Gas monitoring in other areas of the site containing waste materials will likely reveal combustible gas. However, since no on-site OU1 buildings are present (except the leachate treatment facility, which has its own engineered gas monitoring and control system), gas migration monitoring in the waste areas is not required by the O&M manual.

5.2 Gas Monitoring Well Results

Measurements of percent combustible gas (% GAS) and percent lower explosive limit (% LEL) were performed in the 6 gas migration monitoring wells along the northern boundary of the site on June 3, 2003. The wells were monitored in accordance with Attachment 1, Section 3.0 - Routine Operations and Maintenance of the Kin-Buc Landfill Draft O&M Manual (Wheelabrator, 1995). A Landtec GEM 500 sampling device was used to measure the concentration of combustible gas at each well by attaching the meter's sample tubing to the well head petcock and drawing the sample through the meter. Detectable levels of percent combustible gas and percent lower explosive limit

were not observed in any gas monitoring wells. The results for the 6 gas migration monitoring wells are shown in Table 5-1.

5.3 Operational Flare Monitoring Results

The percent combustible gas by volume (% methane) at the landfill's operational flare port inlet was recorded throughout the second quarter of 2003. All readings were collected with a Landtec GEM 500 Gas Analyzer, equipped with a charcoal filter. Monitoring performed on June 3, 2003 revealed combustible gas at 41.8 percent at the flare port inlet.

The following summarizes the flare station operation during the Second Quarter of 2003:

| Date | Gas Flow (SCFM) | Methane % by volume |
|---------------------|--------------------|------------------------|
| 4/7/03 | 114 | 44 |
| 4/21/03 | 147 | 46.8 |
| 5/5/03 | 115 | 42.9 |
| 5/19/03 | 107 | 48 |
| 6/3/03 | 109 | 39.2 |
| 6/16/03 | 122 | 44.3 |
| Averages for Second | | |
| Quarter | 119 | 44.2 |

Note: Flare station data provided by Landfill personnel.

6 CONCLUSIONS

Significant conclusions for the Second Quarter of 2003 monitoring program are as follows:

- In the refuse unit, intragradient conditions were maintained over the entire quarter at Transects 1, 2, 3, 4, and 5. An average daily leachate extraction rate of 1,637 gpd was collected.
- Intragradient conditions were indicated by the monitoring wells (although they usually are not) in the refuse unit at Transect 1. Levels in the leachate collection system indicate intragradient conditions are present at this location.
- Hydraulic control was maintained within OU-1 this quarter based on the analysis
 of the significant influence of S&G#2 with a combination of S&G#3, S&G#4,
 and S&G#1 acting as a hydraulic sink for sand and gravel and bedrock
 groundwater. Groundwater flow in the sand and gravel and bedrock is
 ultimately captured by the pumping wells resulting in overall containment of
 groundwater in OU-1.
- In view of the analysis presented herein, it is recommended that the combined groundwater pumping rates in the sand and gravel be maintained at 15,000 gpd with S&G#2 and S&G#3 pumping at 10,000 gpd and 5,000 gpd, respectively. These lower pumping rates will be evaluated to confirm continued hydraulic control of OU-1 groundwater.
- Maintaining a leachate collection rate of 1,500 gpd is recommended.
- Combustible gas as a percent of total gas and the lower explosive limit was not detected in the 6 monitoring wells located on the northern boundary of the site. The flare was operational and the average percent methane for the quarter at the flare port inlet was 44.2 percent. Based on the non-detection of combustible gas in the monitoring wells, the active gas collection system is functioning properly and there is no off-site gas migration.

REFERENCES

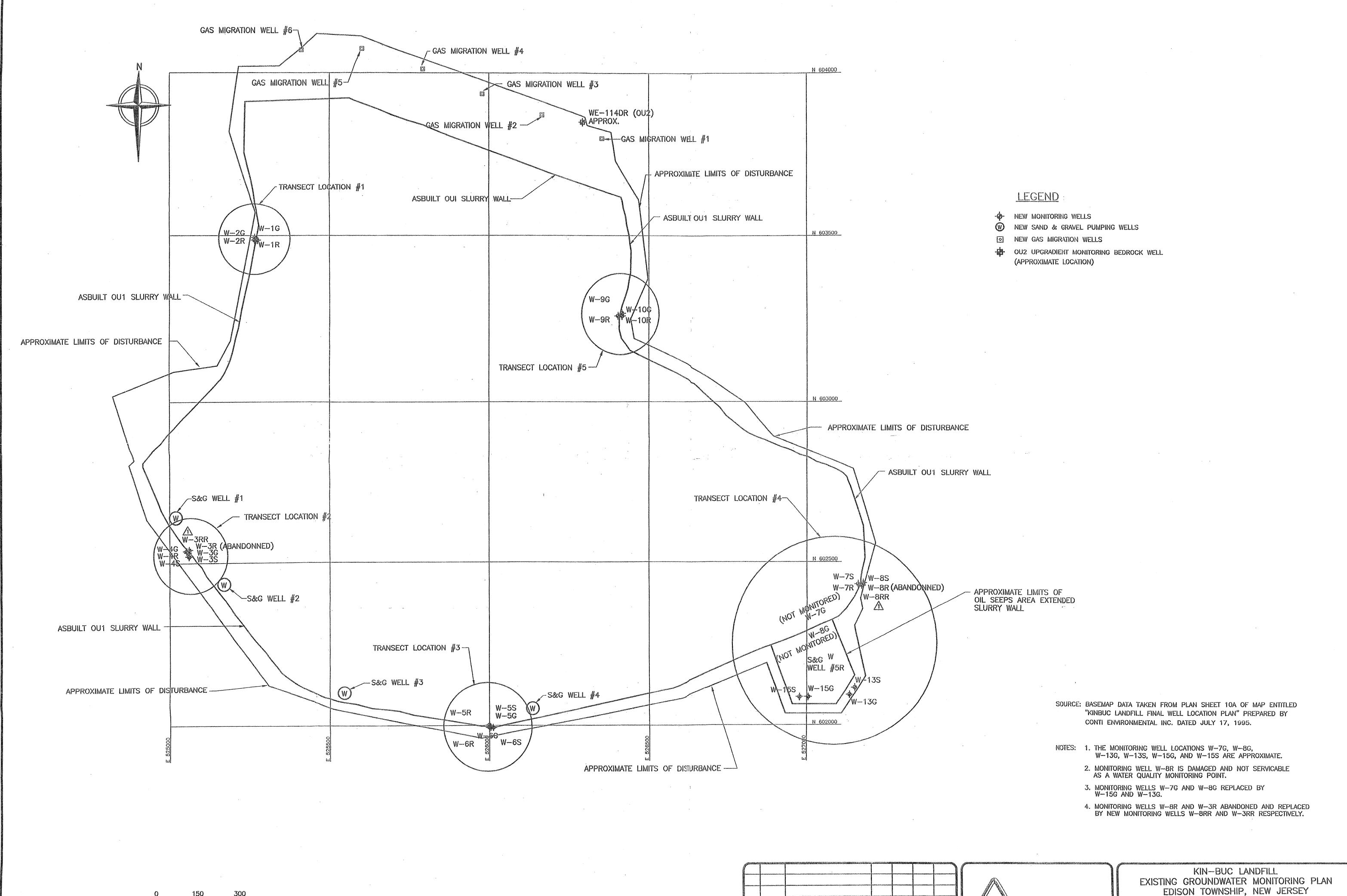
- Proposed Groundwater Monitoring Plan for the Kin-Buc Landfill Operable Unit 1 RD/RA, Wehran Engineering Corporation, Middletown, New York, December 1992.
- Final Addendum 1 to the Proposed Groundwater Monitoring Plan for the Kin-Buc Landfill Operable Unit 1 Closure Plan Re: OU2 Groundwater and Surface Water Monitoring, Wehran Engineering Corporation, Middletown, New York, August 1994.
- Draft Operations and Maintenance Manual for the Kin-Buc Landfill, Wheelabrator EOS, Inc., Pittsburgh, PA, August 1995.
- Remedial Action Report for Operable Unit 2 for the Kin-Buc Landfill Superfund Site, Blasland, Bouck & Lee, Inc., January 1996.
- Appendix C Groundwater, Surface Water, Wetlands and Biota Monitoring Plans for the Kin-Buc Landfill Operable Units 1 and 2, Wheelabrator EOS, Inc., Pittsburgh, PA, August 1995.
- Remedial Action Report Volume I Remedial Action Report, Tables, Appendices A1-A5 for the Kin-Buc Landfill Operable Unit 1, Blasland, Bouck & Lee, Inc., September 1995, Revised February 1996.
- Draft Remedial Investigation Report for Kin-Buc Landfill Operable Unit 2, Wehran Engineering Corporation, Middletown, New York, October 1990.
- Influent Equalization Logs, (Wheelabrator), Inc., Kin-Buc Landfill Treatment Plant, January 1997, February 1997, March 1997.
- Kin-Buc Landfill Leachate Treatment Plant Operation and Site Post-Closure Care, Monthly Reports, Wheelabrator EOS, April, May, June 1997.
- Groundwater Pumping Well Performance Evaluation Report, IT Corporation, July 2000.

Figure

LYING AREA **LEGEND GROUNDWATER** GEI-7G MONITORING LOCATION ĘΑ SCALE IN FEET FIGURE 1-1 KINBUC LANDFILL EDISON TOWNSHIP, NEW JERSEY
OU2 GROUNDWATER
MONITORING LOCATIONS REV. PROJECT NO. 12568-001.000

9 Xrefs: MAKBWE01, MAKETW01, MAKBBD01 11/98 Time: 1:38 PM Operator: FDEGEORG ENE-MTOWNZ/DATA: N:\DWG\12568001\WAKBF-01.dwg

Drawing



SCALE IN FEET

2/99 ADD NEW WELLS

DATE OF ISSUE DWN BY SDT RB

DESCRIPTION

REV DATE

DWN BY DES BY CHK BY APP BY

Shaw ENCONOWT, Inc.

PROJECT NO.

OPERABLE UNIT 1 MONITORING NETWORK

01862-025.000

DRAWING NO.

TABLES

Table 2-1

Kin-Buc Landfill **Operable Unit 1** Continuous Hydraulic Monitoring Well Network/Transects

| Transect Location No. | Screened Hydrogeologic Unit | Well Location Inside Slurry Wall | Well Location Outside Slurry Wall |
|--------------------------|--------------------------------|-------------------------------------|-----------------------------------|
| 1 | Refuse/Fill | W-1G | W-2G |
| | Refuse/Fill | W-3G | W-4G |
| 2 | Sand and Gravel | W-3S | W-4S |
| · | Bedrock | W-3RR | W-4R |
| | Refuse/Fill | W-5G | W-6G |
| 3 | Sand and Gravel | W-58 | W-6S |
| | Bedrock | W-5R | W-6R |
| | Refuse/Fill(1) | W-15G | W-13G |
| 4 | Sand and Gravel(1) | W-158 | W-13S |
| | Sand and Gravel(2) | W-7S | W-8S |
| | Bedrock (2) | W-7R | W-8RR |
| 5 . | Refuse/Fill | W-9G | W-10G |

Notes:

Wells located across the extended slurry wall.
Wells located across the OU1 circumferential slurry wall.

Table 2-2

Kin-Buc Landfill Operable Unit 2 Hydraulic Monitoring Network

| Well Location | Screened Hydrogeologic Unit |
|---------------|--------------------------------|
| Low-L | ying Area |
| GEI-10G | Fill/Refuse |
| WE-10S | Sand & Gravel |
| WE-10R | Bedrock |
| GEI-3G | Fill/Refuse |
| WE-3S | Sand & Gravel |
| WE-3R | Bedrock |
| Mo | ound B |
| GEI-5G | Fill/Refuse |
| WE-5S | Sand & Gravel |
| WE-5R | Bedrock |
| GEI-6G | Fill/Refuse |
| GEI-6S | Sand & Gravel |
| WÉ-6R | Bedrock |
| GEI-7G | Fill/Refuse |
| WE-7S | Sand & Gravel |
| WE-7R | Bedrock |
| Upg | radient |
| WE-114DR | Bedrock |

Table 2-3 KinBuc Landfill Operable Units 1 and 2 Modified Monitoring Program Second Quarter 2003 Manually Recorded Water Level Elevations

| 1 1 | TOC | TOC Ref | April 1, 2003 | | May 8 | , 2003 | June 3, 2003 | | |
|----------------------|--------|-----------|---------------|-----------|------------|-----------|--------------|-----------|--|
| Well ID | Bottom | Elevation | TOC Static | Elevation | TOC Static | Elevation | TOC Static | Elevation | |
| OU1 | | | | | | | | | |
| W-1G | 20.50 | 30.78 | 19.51 | 11,27 | 19.52 | 11,26 | 19.52 | 11.26 | |
| W-1R | 35.34 | 30.79 | 20.89 | 9.90 | 20.62 | 10.17 | 20,74 | 10.05 | |
| W-2G | 20.38 | 30.77 | 18.71 | 12.06 | 19.03 | 11.74 | 19.15 | 11.62 | |
| W-2R | 35.33 | 30.64 | 23.79 | 6.85 | 23.75 | 6.89 | 23.59 | 7.05 | |
| W-3G (oil) | 19.07 | 20.73 | 11.01 | 9.72 | 10.95 | 9.78 | 11.07 | 9.66 | |
| W-3G | 19.07 | 20.73 | 13.05 | 7.68 | 13.39 | 7.34 | 13.04 | 7.69 | |
| W-3S | 31.48 | 20.79 | 20.09 | 0.70 | 19.81 | 0.98 | 20,04 | 0.75 | |
| W-3RR | 54.40 | 21.16 | 20.51 | 0.65 | 20.41 | 0.75 | 20.59 | 0.57 | |
| W-4G | 17.57 | 20.23 | 8.60 | 11.63 | 8.91 | 11.32 | 9.12 | 11.11 | |
| W-4S | 31.58 | 19.71 | 18.64 | 1.07 | 18.80 | 0.91 | 18.93 | 0.78 | |
| W-4R | 54.92 | 20.61 | 19.54 | 1.07 | 19.73 | 0.88 | 19,81 | 0.80 | |
| W-5G | 24.36 | 23.94 | 14.12 | 9.82 | 14.03 | 9.91 | 14.19 | 9.75 | |
| W-5S | 30.33 | 24.33 | 22.85 | 1.48 | 22.58 | 1.75 | 22.74 | 1.59 | |
| W-5R | 41.64 | 24.11 | 22.68 | 1.43 | 22.44 | 1.67 | 22.63 | 1.48 | |
| W-6G | 23.99 | 23.69 | 10.02 | 13.67 | 10.40 | 13.29 | 10.42 | 13.27 | |
| W-6S | 38.49 | 24.00 | 22.38 | 1.62 | 22.16 | 1.84 | 22.34 | 1.66 | |
| W-6R | 50.43 | 23.99 | 22.33 | 1.66 | 21.93 | 2.06 | 22.20 | 1.79 | |
| W-7G | 19.91 | 18.30 | 8.59 | 9.71 | 8.54 | 9.76 | 8.73 | 9.57 | |
| W-7S | 29.34 | 11.61 | 9.88 | 1.73 | 9.69 | 1.92 | 9.83 | 1,78 | |
| W-7R | 45.13 | 11.05 | 9,24 | 1,81 | 9.01 | 2.04 | 9.14 | 1.91 | |
| W-8S | 28.86 | 10.92 | 8.57 | 2,35 | 8.21 | 2.71 | 8.22 | 2.70 | |
| W-8RR | 41.60 | 9.51 | 7.23 | 2.28 | 6.89 | 2.62 | 6.84 | 2.67 | |
| W-9G | 21.93 | 27.34 | 20.08 | 7.26 | 19.94 | 7.40 | 19.75 | 7.59 | |
| W-9R | 39.05 | 27.68 | 21.35 | 6.33 | 21.29 | 6.39 | 21.24 | 6.44 | |
| W-10G | 22.56 | 27.43 | 19.17 | 8.26 | 19.11 | 8.32 | 19.02 | 8.41 | |
| W-10R | 34.01 | 27.43 | 19.48 | 7.95 | 19.56 | 7.87 | 19.26 | 8.17 | |
| W-13G | 10.30 | 10.17 | 3.33 | 6.84 | 3.48 | 6.69 | 3.40 | 6.77 | |
| W-13S | 29.32 | 10.10 | 7.99 | 2.11 | 7.63 | 2.47 | 7.71 | 2.39 | |
| W-15G ⁽¹⁾ | 16.99 | 16.18 | 14.72 | 1.46 | 14.69 | 1.49 | 14.70 | 1.48 | |
| W-15S | 33.36 | 16.05 | 13.81 | 2.24 | 13.61 | 2.44 | 13.68 | 2.37 | |
| OU2 | | | 1 | | | | | | |
| GEI-10G | 13.91 | 13.65 | 0.54 | 13.11 | 1.07 | 12.58 | 1.03 | 12.62 | |
| WE-10S | 29.57 | 14.99 | 13.42 | 1.57 | 13.17 | 1.82 | 13.31 | 1.68 | |
| WE-10R | 41.74 | 13.96 | 12.37 | 1.59 | 12.11 | 1.85 | 12.25 | 1,71 | |
| GEI-3G | 13.54 | 16.73 | 3.55 | 13.18 | 4.27 | 12.46 | 4.29 | 12.44 | |
| WE-3S | 25.67 | 15,12 | 14.15 | 0.97 | 13.70 | 1.42 | 13.92 | 1.20 | |
| WE-3R | 46.51 | 14.99 | 14.49 | 0.50 | 13.43 | 1.56 | 13.76 | 1.23 | |
| GEI-5G | 14.60 | 16.08 | 8.95 | 7.13 | 9.19 | 6.89 | 9.27 | 6.81 | |
| WE-5S | 25.84 | 15.04 | 14.83 | 0.21 | 13.34 | 1.70 | 13.80 | 1.24 | |
| WE-5R | 49.64 | 15.31 | 15.16 | 0.15 | 13.70 | | 14.07 | 1.24 | |
| GEI-6G | 14.97 | 19.76 | 11.66 | 8.10 | 11.69 | 8.07 | 11.81 | 7.95 | |
| GEI-6S | 43.67 | 20.99 | 21.36 | -0.37 | 18.73 | 2,26 | 19.74 | 1.25 | |
| WE-6R | 47.12 | 19.62 | 20.35 | -0.73 | 17.70 | 1.92 | 18.61 | 1.01 | |
| GEI-7G | 13.74 | 17.23 | dry | <3.49 | dry | <3.49 | dry | <3.49 | |
| WE-7\$ | 30.07 | 15.86 | 16.85 | -0.99 | 13.92 | 1.94 | 14.60 | 1.26 | |
| WE-7R | 72.88 | 15.93 | 15.82 | 0.11 | 14.84 | 1.09 | 15.02 | 0.91 | |
| WE-114DR | 44.84 | 23.76 | 17.66 | 6.10 | 17.52 | 6.24 | 17.53 | 6.23 | |

NOTE

(1) All level, reference, bottom measurements recorded to the top of PVC inner casing.

Table 2-4
KinBuc Landfill Operable Units 1 and 2
Continuous Hydraulic Monitoring Results
Second Quarter 2003
Minimum/Maximum/Average Water Elevations

| | | Inside Slurry Wa <u>i</u> l | | • | | | Outside Slurry Wall | | |
|---------|----------------------|--|--|---------------------------------|---------|----------------------|---------------------------------------|---------------------------------------|---------------------------------|
| Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) | Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) |
| N-1G | April | 11.25 | 11.27 | 11.25 | W-2G | April | 11.79 | 12.16 | 12.00 |
| | May | 11.23 | 11.25 | 11.24 | | May | 11:47 | 11.93 | 11.68 |
| | June | 11,12 | 11.78 | 11.28 | | June | 11,60 | 13.34 | 12.71 |
| | 2nd Quarter | 11,12 | 11.78 | 11.26 | 1 | 2nd Quarter | 11.47 | 13,34 | 12.12 |
| V-3G | April | 7.02 | 7.65 | 7,36 | W-4G | April | 11.29 | 12.04 | 11.63 |
| i | Maý | 6.84 | 7.58 | 7.32 | | May | 10.80 | 11.48 | 11.17 |
| i | June | 7.17 | 7.61 | 7.41 | 1 | June | 11.10 | 11.84 | 11.57 |
| | 2nd Quarter | 6.84 | 7.65 | 7.36 | | 2nd Quarter | 10.80 | 12.04 | 11.45 |
| V-3S | April | 0.31 | 1.83 | 1.02 | W-4S | April | -0.19 | 2.78 | 1.23 |
| | May | 0.43 | . 1.53 | 0.97 | | May | 0.00 | 2.46 | 1.17 |
| | June | 0.63 | 1,58 | 1.11 | 1 | June | 0.26 | 2.83 | 1,36 |
| | 2nd Quarter | 0.31 | 1.83 | 1.03 | 1 1 | 2nd Quarter | -0.19 | 2.83 | 1.25 |
| V-5G | April | 9.50 | 10.14 | 9.84 | W-6G | April | 13.09 | 14.60 | 13.75 |
| - 1 | May | 9.59 | 10.07 | 9.82 | | May | 12.76 | 13,74 | 13.22 |
| i | June | 9.64 | 10.10 | 9.85 | 1 1 | June | 13.17 | 14.10 | 13.77 |
| ŀ | 2nd Quarter | 9.50 | 10.14 | 9.84 | ļ. l | 2nd Quarter | 12.76 | 14.60 | 13.58 |
| V-5S | April | 1,21 | 2.68 | 1.89 | W-6S | April | 1.27 | 2.77 | 1.96 |
| | May | 1.13 | 2.50 | 1.81 | 1 | Mav | 1.21 | 2.57 | 1.86 |
| | June | 1.35 | 2.50 | 1.93 | 1 1 | June | 1.45 | 2.57 | 2.01 |
| | 2nd Quarter | 1.13 | 2.68 | 1.88 | 1 | 2nd Quarter | 1.21 | 2.77 | 1.94 |
| V-7S | April | 1.42 | 2.69 | 2.00 | W-8S | April | 2.10 | 5.27 | 2.70 |
| | May | 1.49 | 2.52 | 1.92 | ''' | May | 2.12 | 5.02 | 2.64 |
| | June | 1.66 | 2.48 | 2.06 | | June | 2.21 | 4.92 | 2.77 |
| 1 | 2nd Quarter | 1.42 | 2.69 | 1.99 | 1 1 | 2nd Quarter | 2.10 | 5.27 | 2.77 2.70 |
| V-15S | April | 1.10 | 4.35 | 2.62 | W-13S | April | 1.90 | 3.73 | 2.45 |
| | May | 1.38 | 4.05 | 2.64 | | May | 1.89 | 3.52 | 2.45 |
| ļ | June | 1.66 | 4.11 | 2.77 | 1 1 | June | 2.06 | 3.72 | 2.54 |
| i | 2nd Quarter | 1.10 | 4.35 | 2.68 | f l | 2nd Quarter | 1.89 | 3.72 | 2.54 |
| /-15G | April | 1,22 | 1.71 | 1.50 | W-13G | April | 6.48 | 6.91 | 6.70 |
| | May | 1.28 | 1.69 | 1.53 | 111-130 | May | 6.47 | 7.00 | 6.69 |
| | June | 1.28 | 1.69 | 1.54 | | June | 6.47 | 7.00 7.05 | 6.79 |
| i | 2nd Quarter | 1.22 | 1.71 | 1.52 | 1 1 | 2nd Quarter | 6.47 | 7.05 | 6.73 |
| /-9G | April | 7.13 | 7.60 | 7.35 | W-10G | April | 8.25 | 7.05 8.44 | 8.35 |
| | May | 7.06 | 7.65 | 7.35 7.31 | 1,1,100 | May | 8.18 | 8.38 | 8.35 8.28 |
| | June | 7.51 | 7.96 | 7.74 | | Jüne | 8:37 | 9.18 | 8.80 |
| 1 | 2nd Quarter | 7.06 | 7.96 | 7.74 7.46 | | 2nd Quarter | 8.18 | 9.18 | |
| /-3RR | April | 0.03 | 1.94 | 0.94 | W-4R | | -0.27 | 2.85 | 8.47 |
| -500 | May | -0.10 | 1.94 | 0.89 | AA-4L | April | -0.27 -0.25 | 2.85 | 1.20 |
| Ì | Jüne | 0.23 | 2.18 | | | May | | | 1.04 |
| i | 2nd Quarter | -0.10 | 2.18 2.18 | 1.04 0.96 | | June 2nd Quarter | -0.05 -0.27 | 2.81 2.85 | 1.17 1.14 |

Table 2-4 KinBuc Landfill Operable Units 1 and 2 Continuous Hydraulic Monitoring Results Second Quarter 2003

Minimum/Maximum/Average Water Elevations

| | | | | ann maximum/A | 7.432 | CO. BIOTAGO | 7113 | | |
|---------|----------------------|--|--|---------------------------------|---------|----------------------|---------------------------------------|--|---------------------------------|
| | | Inside Sturry Wall | | | | | Outside Slurry Wall | | |
| Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) | Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) |
| W-5R | April | 1.38 | 2.84 | 2.05 | W-6R | April | 1.47 | 2.91 | 2.13 |
| | May | 1.24 | 2.61 | 1.93 | | May | 1.47 | 2.66 | 2.03 |
| | June | 1.47 | 2.62 | 2.07 | | June | 1.64 | 2.69 | 2.16 |
| | 2nd Quarter | 1.24 | 2.84 | 2.01 | | 2nd Quarter | 1.47 | 2.91 | 2.10 |
| W-7R | April | 1.51 | 2.77 | 2.09 | W-8RR | April | 2.05 | 5.21 | 2.66 |
| | May | 1.59 | 2.62 | 2.01 | | May | 2.09 | 4.97 | 2.60 |
| | June | 1.77 | 2.58 | 2.16 | | June | 2.17 | 4.89 | 2.73 |
| | 2nd Quarter | 1.51 | 2.77 | 2.09 | | 2nd Quarter | 2.05 | 5.21 | 2.66 |

Table 2-5 KinBuc Landfill Operable Unit 1 Second Quarter 2003 Troll Water Elevations vs. Manual Water Elevations

| OU 1 | | May 8, | 2003 | | June 3, | 2003 | , | June 30, | 2003 | Average |
|---------|-------|--------|------------|-------|---------|------------|-------|----------|------------|---------|
| Well ID | Troll | Manual | Difference | Troll | Manuai | Difference | | | Difference | |
| W-1G | 11.27 | 11.26 | 0.01 | 11.25 | 11.26 | 0.01 | 11.89 | 11.86 | 0.03 | 0.02 |
| W-2G | 11.73 | 11.74 | 0.01 | 11.60 | 11.62 | 0.02 | 12.92 | 12.91 | 0.01 | 0.01 |
| W-3G | 7.39 | 7.34 | 0.05 | 7.21 | 7.69 | 0.48 | 7.39 | 7.85 | 0.46 | 0.33 |
| W-3S | 0.91 | 0.98 | 0.07 | 0.67 | 0.75 | 0,08 | 0.70 | 0.73 | 0.03 | 0.06 |
| W-3RR | 0.74 | 0.75 | 0.01 | 0.55 | 0.57 | 0.02 | 0.66 | 0.63 | 0.03 | 0.02 |
| W-4G | 11.32 | 11.32 | 0.00 | 11.10 | 11,11 | 0.01 | 11.53 | 11.53 | 0.00 | 0.01 |
| W-4S | 0.91 | 0.91 | 0.00 | 0.78 | 0.78 | 0.00 | 1.18 | 1.18 | 0.00 | 0.00 |
| W-4R | 0.85 | 0.88 | 0.03 | 0.71 | 0.80 | 0.09 | 0.98 | 1.12 | 0.14 | 0.09 |
| W-5G | 9.86 | 9.91 | 0.05 | 9.68 | 9.75 | 0.07 | 9.84 | 9.90 | 0.06 | 0.06 |
| W-5S | 1.73 | 1.75 | 0.02 | 1.57 | 1.59 | 0.02 | 1.51 | 1.51 | 0.01 | 0.01 |
| W-5R | 1.64 | 1.67 | 0.03 | 1.44 | 1.48 | 0.04 | 1.39 | 1.43 | 0.04 | 0.04 |
| W-6G | 13.29 | 13.29 | 0.00 | 13.24 | 13.27 | 0.03 | 13.38 | 13.38 | 0.00 | 0.01 |
| W-6S | 1.80 | 1.84 | 0.04 | 1.62 | 1.66 | 0.04 | 1.65 | 1.68 | 0.03 | 0.04 |
| W-6R | 2.04 | 2.06 | 0.02 | 1.73 | 1.79 | 0.06 | 1.76 | 1.80 | 0.04 | 0.04 |
| W-7S | 1.88 | 1.92 | 0.04 | 1.75 | 1.78 | 0.03 | 1.67 | 1.72 | 0.05 | 0.04 |
| W-7R | 2.00 | 2.04 | 0.04 | 1.88 | 1.91 | 0.03 | 1.82 | 1.87 | 0.05 | 0.04 |
| W-8S | 2.66 | 2.71 | 0.05 | 2.69 | 2.70 | 0.01 | 2.36 | 2.37 | 0.01 | 0.02 |
| W-8RR | 2.64 | 2.62 | 0,02 | 2.67 | 2.67 | 0.00 | 2.35 | 2.31 | 0.04 | 0.02 |
| W-9G | 7.38 | 7.40 | 0.02 | 7.55 | 7.59 | 0.04 | 7.78 | 7.82 | 0.04 | 0.03 |
| W-10G | 8.31 | 8.32 | 0.01 | 8.42 | 8.41 | 0.01 | 9.12 | 9.12 | 0.00 | 0.01 |
| W-13G | 6.70 | 6.69 | 0.01 | 6.70 | 6.77 | 0.07 | 6.60 | 6.62 | 0.02 | 0.03 |
| W-13S | 2.47 | 2.47 | 0.00 | 2.38 | 2.39 | 0.01 | 2.14 | 2.15 | 0.01 | 0.01 |
| W-15G | 1.49 | 1.49 | 0.00 | 1.47 | 1.48 | 0.01 | 1.54 | 1.19 | 0.35 | 0.12 |
| W-15S | 2.41 | 2.44 | 0.03 | 2.32 | 2.37 | 0.05 | 2.20 | 2.24 | 0.04 | 0.04 |

Table 2-6 Kin-Buc Landfill Leachate Cleanout Monitoring 2003

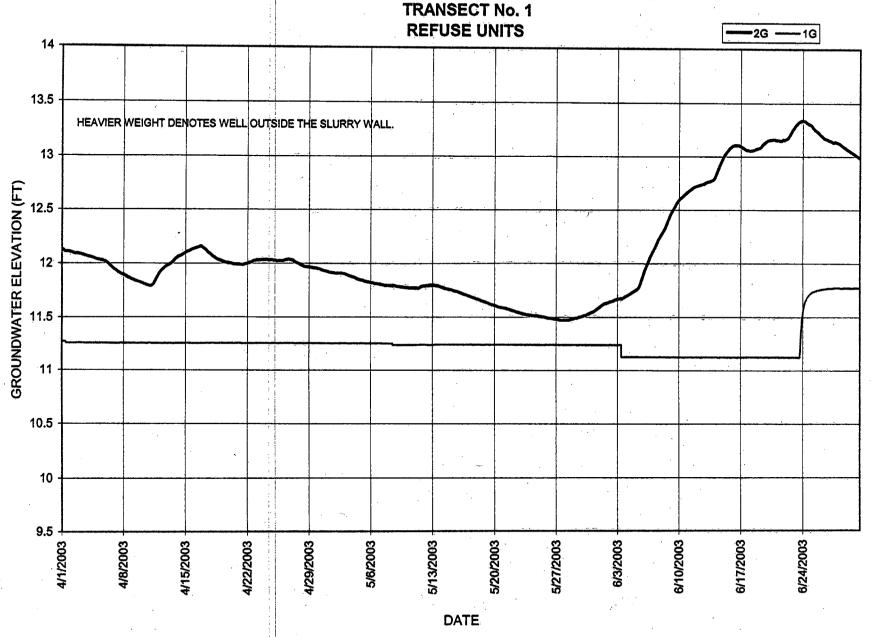
| Cleanout location | | 4N | | 4E | 1 | 5N | 1 | 5E | 1 | 6N | 1 | 6E |
|-----------------------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|------------------|-----------|----------|--------------------|
| Elevation @ Sea Level | | 2,87 | 22 | 2.77 | 26 | 3,51 | 20 | 3.51 | 3 | 1.36 | | 1.32 |
| | depth to | | depth to | | depth to | | depth to | | depth to | | depth to | |
| | water | elevation | water | elevation | water | elevation | | elevation | water | elevation | _ | elevation |
| Elevation Average | | 10.09 | | 10.06 | | 9.85 | | 9.93 | | na | | na |
| DATE | | | | | | | | | sa jurin seliji. | | | Nasaki ili ili ili |
| 12/10/2001 | 12.5 | 10.37 | 12.42 | 10.35 | 16.31 | 10.20 | 16.33 | 10.18 | dry | na | dry | na na |
| 1/3/2002 | 12.37 | 10.50 | 12.31 | 10.46 | 16.21 | 10.30 | 16.22 | 10.29 | dry | na | dry | na |
| 2/13/2002 | 12.70 | 10.17 | 12.63 | 10.14 | 16.57 | 9.94 | 16.62 | 9.89 | dry | na | dry | na |
| 3/27/2002 | 12.61 | 10.26 | 12.55 | 10.22 | 16.52 | 9.99 | 16.47 | 10.04 | dry | na | dry | na |
| 4/19/2002 | 12.75 | 10.12 | 12.68 | 10.09 | 16.64 | 9.87 | 16.61 | 9.90 | dry | na | dry | na |
| 5/3/2002 | 13.03 | 9.84 | 12.96 | 9.81 | 16.97 | 9.54 | 16.94 | 9.57 | dry | na | dry | na |
| 6/5/2002 | 13.04 | 9.83 | 12.97 | 9.80 | 16.63 | 9.88 | 16.95 | 9.56 | dry | na | dry | na |
| 7/8/2002 | 12.86 | 10.01 | 12.79 | 9.98 | 16.77 | 9.74 | 16.72 | 9.79 | dry | na | dry | na |
| 8/2/2002 | 12.86 | 10.01 | 12.79 | 9.98 | 16.8 | 9.71 | 15.73 | 10.78 | dry | na | dry | na |
| 9/5/2002 | 12.86 | 10.01 | 12.78 | 9.99 | 16.77 | 9.74 | 16.75 | 9.76 | dry | na | dry | na |
| 9/26/2002 | 12.94 | 9.93 | 12.85 | 9.92 | 16.85 | 9.66 | 16.83 | 9.68 | dry | na | dry | na |
| 11/6/2002 | 12.64 | 10.23 | 12.58 | 10.19 | 16.59 | 9.92 | 16.48 | 10.03 | dry | na | dry | na |
| 12/6/2002 | 13.02 | 9.85 | 12.94 | 9.83 | 16.97 | 9.54 | 16.95 | 9.56 | dry | na | dry | na |
| 1/2/2003 | 13.07 | 9.80 | 13.00 | 9.77 | 17.03 | 9.48 | 17.01 | 9.50 | dry | na | dry | na |
| 2/12/2003 | 13.20 | 9.67 | 13.12 | 9.65 | 17.19 | 9.32 | 17.16 | 9.35 | dry | na | dry | na |
| 3/4/2003 | 13.21 | 9.66 | 13.15 | 9.62 | 17.22 | 9.29 | 17.20 | 9.31 | dry | na | dry | na |
| 4/1/2003 | 12.90 | 9.97 | 12.83 | 9.94 | 16.82 | 9.69 | 16.79 | 9.72 | dry | na | dry | na |
| 5/8/2003 | 13.05 | 9.82 | 12.97 | 9.80 | 17.01 | 9.50 | 16.96 | 9.55 | dry | na | dry | na |
| 6/3/2003 | 13.11 | 9.76 | 13.14 | 9,63 | 17.09 | 9.42 | 17.04 | 9.47 | dry | na | dry | na |
| 6/30/2003 | 12.92 | 9.95 | 12.85 | 9.92 | 16.83 | 9.68 | 16.79 | 9.72 | dry | na | dry | na |
| | | | | | | * | | | | | | |

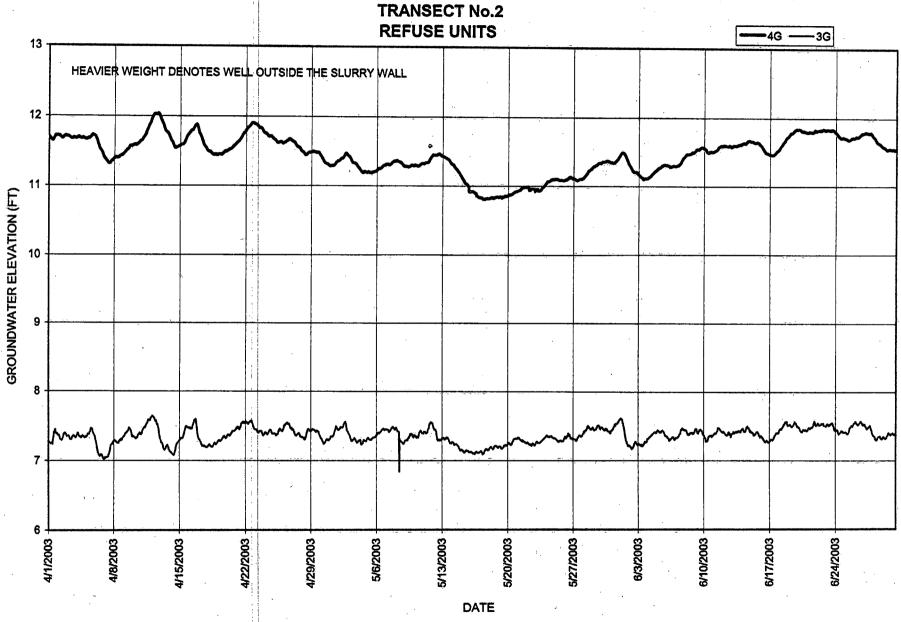
Table 5-1

Kin-Buc Landfill Operable Unit 1 Second Quarter 2003 Modified Program Gas Monitoring Well Network/Results

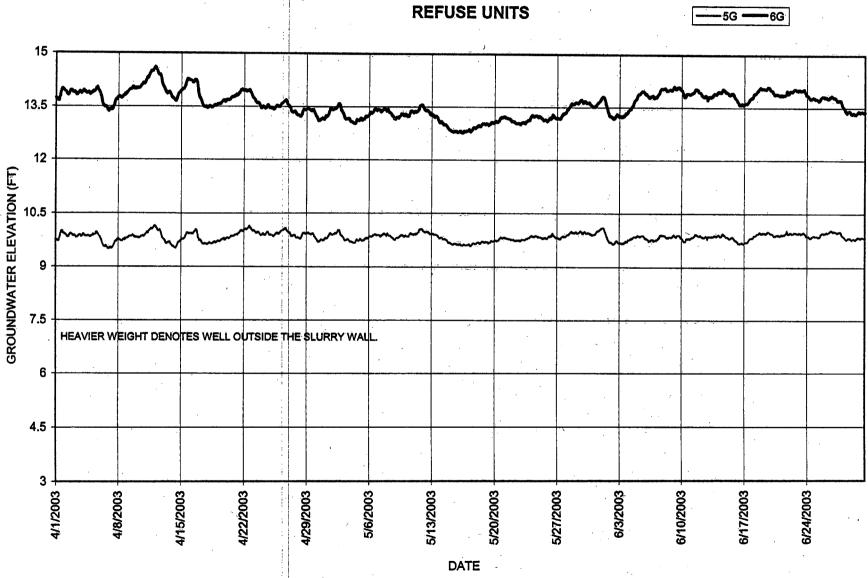
| | Monitoring Result | | | | | |
|-------------------------|-------------------|-------|--|--|--|--|
| Well (Network) Location | % LEL | % GAS | | | | |
| GMW-01 | 0 | 0 | | | | |
| GMW-02 | 0 | 0 | | | | |
| GMW-03 | 0 | 0 | | | | |
| GMW-04 | 0 | 0 | | | | |
| GMW-05 | 0 | 0 | | | | |
| GMW-06 | 0 | 0 | | | | |
| Operational Flare Inlet | NA | 41.8 | | | | |

APPENDIX A CONTINUOUS WATER LEVEL MONITORING RESULTS

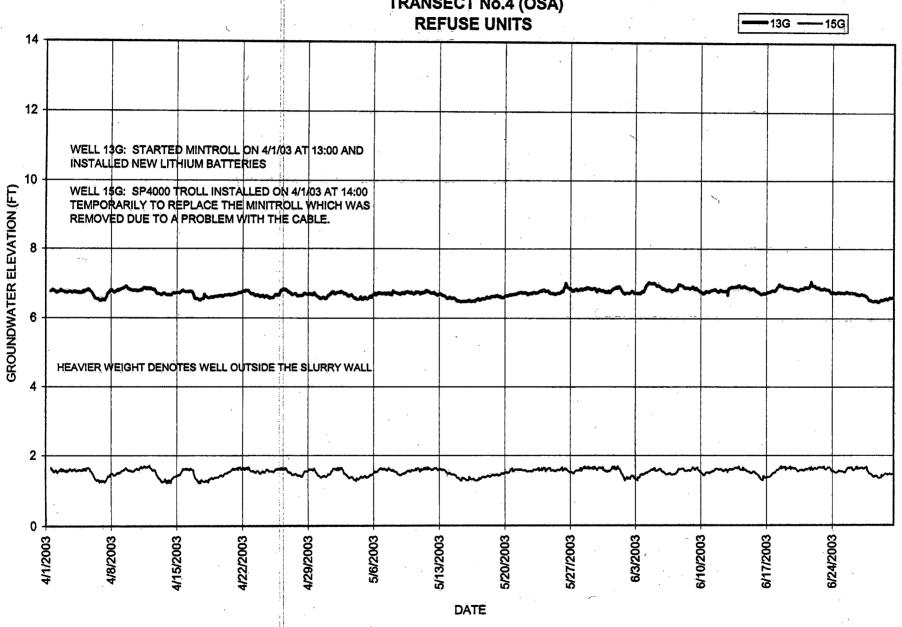




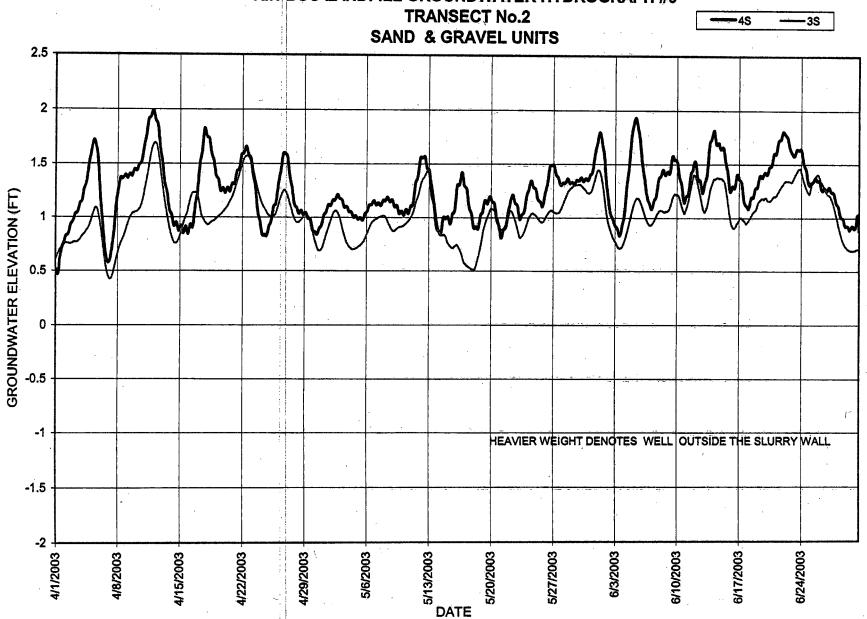
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH # 3 TRANSECT No.3

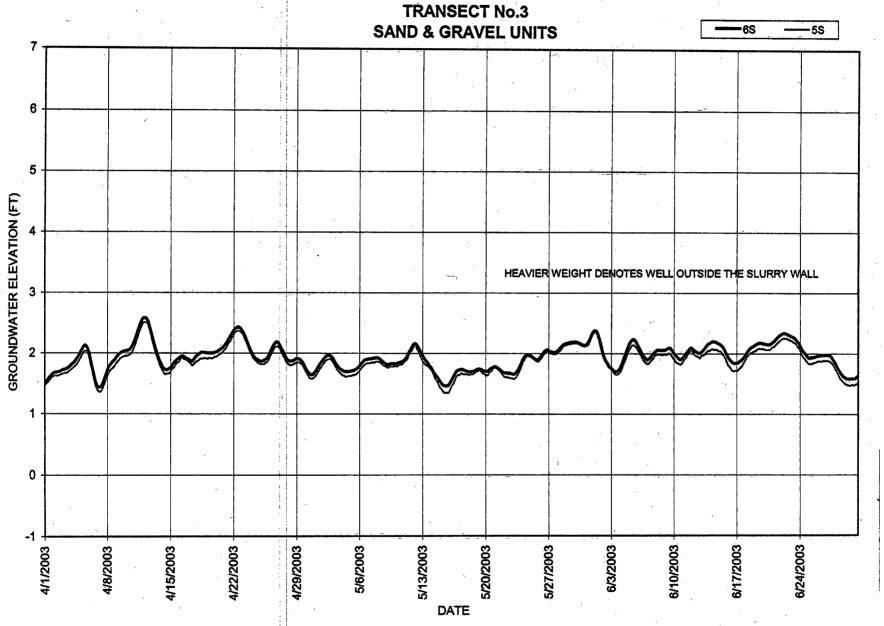


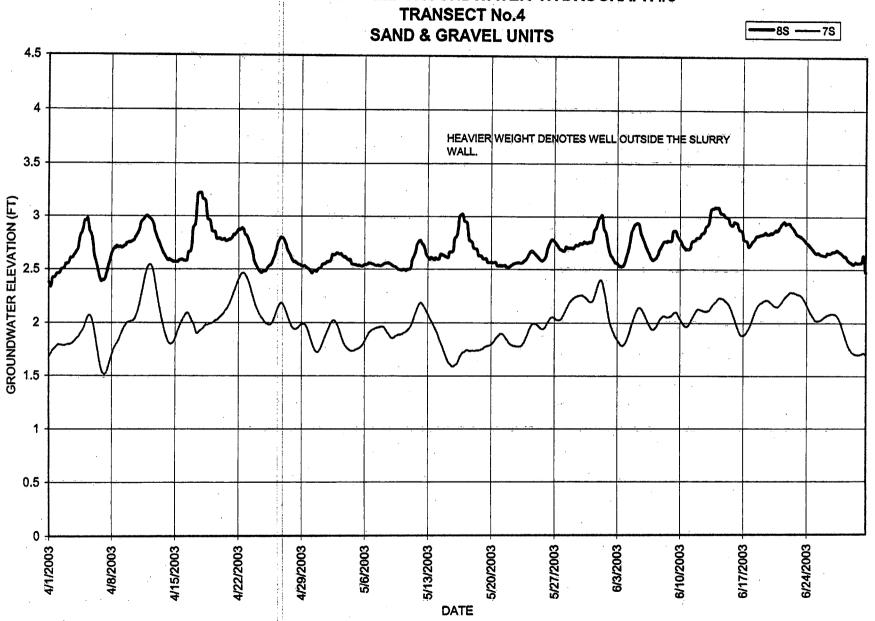
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #4 TRANSECT No.4 (OSA)



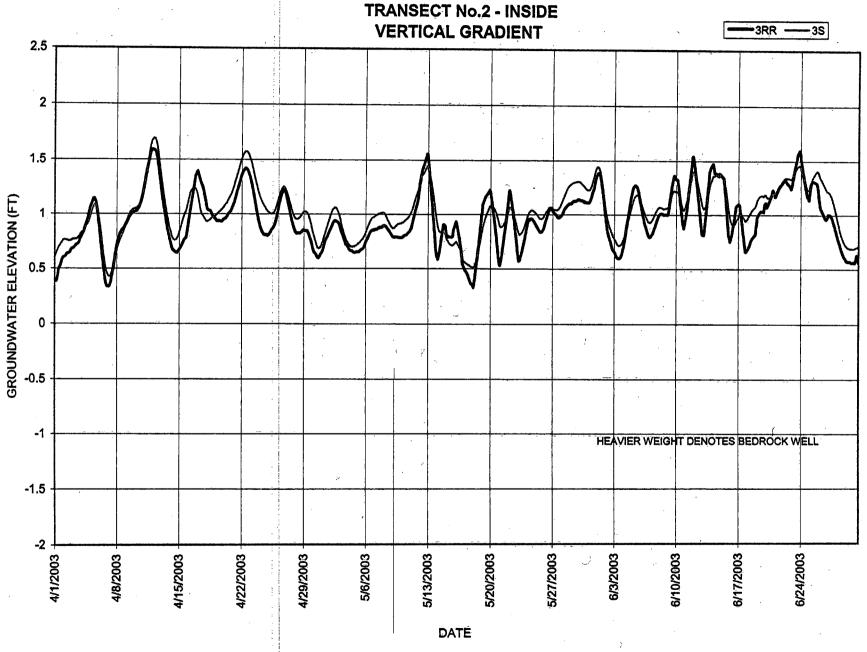
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #5 **TRANSECT No.5 REFUSE UNITS** -10G -•9G 9.5 つ 9 8.5 GROUNDWATER ELEVATION (FT) HEAVIER WEIGHT DENOTES WELL OUTSIDE THE SLURRY WALL 6 5.5 o 4/1/2003 | − 6/3/2003 5/6/2003 4/29/2003 5/13/2003 5/20/2003 5/27/2003 6/10/2003 6/17/2003 6/24/2003 4/8/2003 4/15/2003 4/22/2003







KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #9 TRANSECT No.4 (OSA) SAND & GRAVEL UNIT -13S ---- 15S -- 15G 10 8 HEAVIER WEIGHT DENOTES WELL OUTSIDE THE SLURRY WALL. GROUNDWATER ELEVATION (FT) 0 5/6/2003 6/3/2003 4/1/2003 4/8/2003 6/10/2003 6/17/2003 4/15/2003 4/22/2003 4/29/2003 5/13/2003 5/27/2003 6/24/2003



KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #11 **TRANSECT No.2 - OUTSIDE VERTICAL GRADIENT** -4R -3.5 3 2.5 GROUNDWATER ELEVATION (FT) HEAVIER WEIGHT DENOTES BEDROCK WELL 1.5 0,5 0 -0.5 4/1/2003 4/8/2003 5/6/2003 6/3/2003 6/10/2003 6/17/2003 4/15/2003 4/22/2003 4/29/2003 5/13/2003 5/20/2003 5/27/2003 6/24/2003

KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #12 **TRANSECT No.3 - INSIDE** -5R **VERTICAL GRADIENT** 3.5 3 2.5 GROUNDWATER ELEVATION (FT) HEAVIER WEIGHT DENOTES BEDROCK WELL 0 -0.5 5/6/2003 5/27/2003 6/3/2003 6/24/2003 6/10/2003 6/17/2003 4/1/2003 4/8/2003 4/15/2003 4/22/2003 4/29/2003 5/13/2003 5/20/2003

KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #13 **TRANSECT No.3 - OUTSIDE VERTICAL GRADIENT** 6 5 GROUNDWATER ELEVATION (FT) HEAVIER WEIGHT DENOTES BEDROCK WELL 0 6/3/2003 4/22/2003 4/29/2003 5/6/2003 4/8/2003 6/10/2003 6/17/2003 6/24/2003 4/1/2003 4/15/2003 5/13/2003 5/20/2003 5/27/2003

KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #14 TRANSECT No.4- INSIDE -7S **VERTICAL GRADIENT** 3.5 3 GROUNDWATER ELEVATION (FT) HEAVIER WEIGHT DENOTES BEDROCK WELL 0.5 0 -4/1/2003 5/6/2003 6/3/2003 4/8/2003 6/24/2003 6/10/2003 6/17/2003 4/15/2003 4/29/2003 5/13/2003 5/20/2003 5/27/2003 4/22/2003

KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #15 **TRANSECT No.4- OUTSIDE** 8RR -85 **VERTICAL GRADIENT** 4.5 4 3.5 GROUNDWATER ELEVETION (FT) 2.5 1.5 HEAVIER WEIGHT DENOTES BEDROCK WELL 0.5 0 4/1/2003 4/29/2003 5/6/2003 5/27/2003 6/3/2003 4/8/2003 6/10/2003 6/17/2003 6/24/2003 4/15/2003 4/22/2003 5/13/2003

APPENDIX B MONTHLY HYDRAULIC EVALUATIONS



One International Boulevard, Suite 700 Mahwah, NJ 07495-0086 201.512.5700 Fax 201.512.5786

June 10, 2003 Project 791186

Mr. Carl Januszkiewicz Waste Management, Inc. Kin-Buc Landfill Treatment Plant 383 Meadow Road Edison, NJ 08817

Re: Hydraulic Monitoring for April 2003

Dear Mr. Januszkiewicz:

A site visit was completed on May 8, 2003 to download the April water level recorder data and obtain manual water level measurements. The following is an update of the hydraulic monitoring for the month of April 2003 at the Kin-Buc Landfill. This information is to be included in the quarterly report, which is to be submitted to the EPA by mid-August 2003.

The minimum, maximum, and average water elevations recorded at each well are included in Table 1. Table 2 shows the troll water elevations versus the manual water elevations. The continuous water level elevation data when compared with manual readings indicated that the miniTrolls are functioning properly and are recording accurate data. The SP4000 Troll is still recording continuous hydraulic data in Well 15G. A representative from In-Situ, Inc. was contacted regarding the complications with the miniTroll.

Also, the data supplied for wells SG-1 and SG-3 showed the same water level for the period. The automated water level recording device in these wells need to be checked so that accurate readings can be obtained in the future.

Hydrographs have been prepared for each of the transect locations and are enclosed for your reference as Attachment No. 1. The water levels in wells on the outside of the slurry wall vary over the course of the day due to the tidal influence at the site. For clarity, Hydrograph Nos. 6 through 15 show the average water level in the well over a 24-hour period (12 hours before, and 12 hours after).

Refuse

As defined in the Record of Decision (ROD) for OU-1, the performance objective for the refuse unit calls for the pumping of leachate to establish inward gradients across the slurry wall with the additional benefit of reducing downward flow into the underlying sand and gravel unit. Based on the hydrographs the following is presented.

Mr. Carl Januszkiewicz June 10, 2003 Page 2

Transect 1-Refuse (1G/2G)/Hydrograph No. 1 - Intragradient conditions were observed during the entire month of April. The average monthly water elevation for April at Well 1G (inside) and Well 2G (outside) was 11.25 and 12.00 feet msl, respectively. Water level elevation measurements taken from Leachate Collection Cleanouts Nos. 14 through 16 are included in Table 3, and indicate that the leachate collection system is functioning properly. The fact that the leachate collection system is functioning properly suggests significant capture of leachate. The evaluation of the hydraulic conditions in the refuse at Transect 1 is provided in Attachment No.2.

Transect 2-Refuse (3G/4G)/Hydrograph No. 2 — Intragradient conditions were maintained throughout the month of April. The average monthly water elevation for the month at Well 3G (inside) and Well 4G (outside) was 7.36 and 11.63 feet msl, respectively

Transect 3-Refuse (5G/6G)/Hydrograph No. 3 — Intragradient conditions were maintained throughout the month of April. The average monthly water elevation for the month of April at Well 5G (inside) and Well 6G (outside) was 9.84 and 13.75 feet msl, respectively.

Transect 4-Refuse Oil Seeps Area (13G/15G)/Hydrograph No. 4 — Intragradient conditions were not maintained throughout the month of April. The average monthly water elevation for the month of April at Well 15G (inside) and Well 13G (outside) was 15.62 and 6.70 feet msl, respectively.

Transect 5-Refuse (9G/10G)/Hydrograph No. 5 — Intragradient conditions were maintained throughout the month of April. The average monthly water elevation for the month of April at Well 9G (inside) and Well 10G (outside) was 7.35 and 8.35 feet msl, respectively.

Sand and Gravel/Bedrock

For the sand and gravel unit, the performance objectives call for pumping of sand and gravel groundwater to prevent flow toward the slurry wall and to impose upward hydraulic gradients from the bedrock to the sand and gravel. An additional benefit would be the establishment of inward gradients across the slurry wall within the sand and gravel unit. The following is a description of the flow characteristics based on visual observation of the hydrographs.

Horizontal Flow

Transect 2-Sand and Gravel (3S/4S)/Hydrograph No. 6 — Although intragradient conditions were not consistently maintained throughout the month of April, there were periods where intragradient conditions are evident. Containment is being maintained by

Mr. Carl Januszkiewicz June 10, 2003 Page 3

pumping wells (see discussion in Conclusion). The average monthly water elevations for the month of April at Well 3S (inside) and Well 4S (outside) was 1.02 and 1.23 feet msl, respectively.

Transect 3-Sand and Gravel (5S/6S)/Hydrograph No. 7 — Slight intragradient conditions were maintained throughout the month of April. The average monthly water elevation for Well 5S (inside) and Well 6S (outside) was 1.89 and 1.96 feet msl, respectively.

Transect 4-Sand and Gravel (78/88)/Hydrograph No. 8- Intragradient conditions were maintained throughout the month of April. The average monthly water elevation for the month of April at Well 7S (inside) and Well 8S (outside) was 2.00 and 2.70 feet msl, respectively.

Transect 4 Sand and Gravel Oil Seeps Area (13S/15S)/Hydrograph No. 9—Intragradient conditions were not evident during most of the month of April. The average monthly water elevation for the month of April at Well 15S (inside) and Well 13S (outside) was 2.62 and 2.45 feet msl, respectively. Water levels from Well 15G in the refuse unit are included on the hydrograph for comparison.

Vertical Flow-Inside Slurry Wall

Transect 2-Vertical Gradient (3S/3RR)-Inside/Hydrograph No.10 — Upward gradient conditions were not observed between the bedrock and overlying sand & gravel units inside the slurry wall for most of the month of April. The average monthly water elevation for the month of April at Well 3S (sand & gravel) and Well 3RR (bedrock) was 1.02 and 0.94 feet msl, respectively.

Transect 3-Vertical Gradient (5R/5S)-Inside/Hydrograph No. 12 — Upward gradient conditions were observed between the bedrock and overlying sand & gravel units inside the slurry wall for the month of April. The average monthly water elevation for the month of April at Well 5S (sand & gravel) and Well 5R (bedrock) was 1.89 and 2.05 feet msl, respectively.

Transect 4-Vertical Gradient (7R/7S)-Inside/Hydrograph No. 14 — Upward gradient conditions were observed between the bedrock and overlying sand & gravel units inside the slurry wall throughout the month of April. The average monthly water elevation for the month of April at Well 7S (sand & gravel) and Well 7R (bedrock) was 2.00 and 2.09 feet msl, respectively.

Mr. Carl Januszkiewicz June 10, 2003 Page 4

Vertical Flow-Outside Slurry Wall

Transect 2-Vertical Gradient (4S/4R)-Outside/Hydrograph No. 11 — Upward gradient conditions were not observed between the bedrock and overlying sand & gravel units outside the slurry wall for the month of April. The average monthly water elevation for the month of April at Well 4S (sand & gravel) and Well 4R (bedrock) was 1.23 and 1.20 feet msl, respectively.

Transect 3-Vertical Gradient (6R/6S)-Outside/Hydrograph No. 13 — Upward gradient conditions were observed between the bedrock and overlying sand & gravel units outside the slurry wall for the month of April. The average monthly water elevation for the month of April at Well 6S (sand & gravel) and Well 6R (bedrock) was 1.96 and 2.13 feet msl, respectively.

Transect 4-Vertical Gradient (8RR/8S)-Outside/Hydrograph No. 15 — Upward gradient conditions were not observed between the bedrock and overlying sand & gravel units outside the slurry wall throughout the month of April. The average monthly water elevation for the month of April at both Well 8S (sand & gravel) and Well 8RR (bedrock) was 2.70 and 2.66 feet msl, respectively. The difference in average monthly water elevations for April was 0.06 feet.

An initial review of the hydrographs indicates that certain performance objectives associated with the sand and gravel and bedrock units may not be met, specifically associated with the uniform achievement of upward gradients from the bedrock to the overlying sand and gravel inside the wall (e.g. Hydrograph 10), and inward gradients across the slurry wall within the sand and gravel (Hydrographs 6 and 9). However previous investigations performed at the site would indicate that complete control of OU-1 groundwater can be achieved notwithstanding indications of downward flow from the sand and gravel to the bedrock, or outward flow across the slurry wall within the sand and gravel unit. This is based on the findings of the considerable pumping influence of the sand and gravel pumping wells, in particular S&G#2, in achieving hydraulic control at the site (see Groundwater Pumping Well Performance Evaluation Report, July 2000).

The influence of the pumping well can be demonstrated by review of a plan view groundwater contour map of the sand and gravel (Figure 1) and equipotential profiles and vector diagrams (Figures 1, 2, 3, and 4) that have been prepared for a period of time when the vertical gradient between the sand and gravel and the bedrock was downward at Transect 2. For this evaluation, a snapshot of groundwater elevations from the monitoring wells and pumping wells was obtained for April 22, 2003. At this time, S&G#2 was pumping at a rate of about 5.6 gallons per minute (gpm), while S&G#4 was pumping at a rate of 1 gpm. This resulted in a total of approximately 6.6 gpm or about 12,416 gallons per day. There was a downward vertical gradient observed the majority of the time

between the sand and gravel and the bedrock inside and outside the slurry wall at Transect No.2 in April as evidenced by higher heads in the sand and gravel wells relative to bedrock wells. Periodically, there was also a higher head within the sand and gravel inside the slurry wall relative to the sand and gravel outside the slurry wall at Transect No. 2 in April.

Figures 1-4 incorporate the heads induced by pumping and show the considerable pumping influence of S&G#2. Specifically, groundwater flowing downward from the sand and gravel into the bedrock subsequently flows toward the pumping well. This occurs both inside and outside of the slurry wall. Also, groundwater within the sand and gravel unit flows toward the pumping well. The considerable pumping influence demonstrated at S&G#2, in conjunction with the fact that natural groundwater gradients in both the sand & gravel and bedrock flow predominantly towards the area of S&G#2, result in the complete capture of OU-1 groundwater at these pumping rates.

Groundwater and Leachate Collection

Based on data provided by U.S. Filter, the following volumes of groundwater and leachate were extracted from the sand & gravel wells and leachate collection system for the period from April 1 to April 30, 2003:

| S&G No. 1 Groundwater | S&G No. 2 Groundwater | S&G No. 3 Groundwater | S&G No. 4 Groundwater | Leachate | | |
|--------------------------|--------------------------|--------------------------|--------------------------|-------------|--|--|
| 0 gal. | 330,378 gal. | 122,889 gal. | 0 gal. | 50,252 gal. | | |
| 0 gpd | 11,013 gpd | 4,096 gpd | 0 gpd | 1,675 gpd | | |

For the month of April, a total of 453,267 gallons of groundwater was collected. The average daily groundwater extraction rate for all of the wells was 15,109 gpd. The extraction rate from S&G No. 2 was 11,013 gpd and the extraction rate from S&G No. 3 was 4,096 gpd. The leachate extraction rate was 1,675 gpd for the month of April.

CONCLUSIONS

Intragradient conditions were maintained in the refuse unit at Transects 1, 2, 3, and 5.

Intragradient conditions are not usually maintained by the monitoring wells at Transect 1 (although they were for the month of April), although each month levels in the leachate collection system indicate intragradient conditions are present at this location.

Transducers in S&G#1 and S&G#3 need to be checked. The data for April 22, 2003 showed no change in water level throughout the day, suggesting that the transducers are not functioning properly.

Hydraulic control was maintained within OU-1 based on the analysis of the significant influence of S&G#2 in acting as a hydraulic sink for sand and gravel and bedrock groundwater. Groundwater flow in the sand and gravel and bedrock is ultimately captured by the pumping wells (S&G#2 and S&G#3 or 4) resulting in overall containment of groundwater in OU-1.

In view of the analysis presented herein, it is recommended that the combined groundwater pumping rates in the sand and gravel be maintained at 15,000 gpd with S&G#2 and S&G#3 pumping at 10,000 gpd and 5,000 gpd, respectively. These lower pumping rates will be evaluated to confirm continued hydraulic control of OU-1 groundwater.

We trust you find this information useful. If you have any questions, please do not hesitate to contact us.

EMCON/OWT, INC.

Tim Pagano, CPG

Senior Hydrogeologist

Laura Kisala

Environmental Scientist

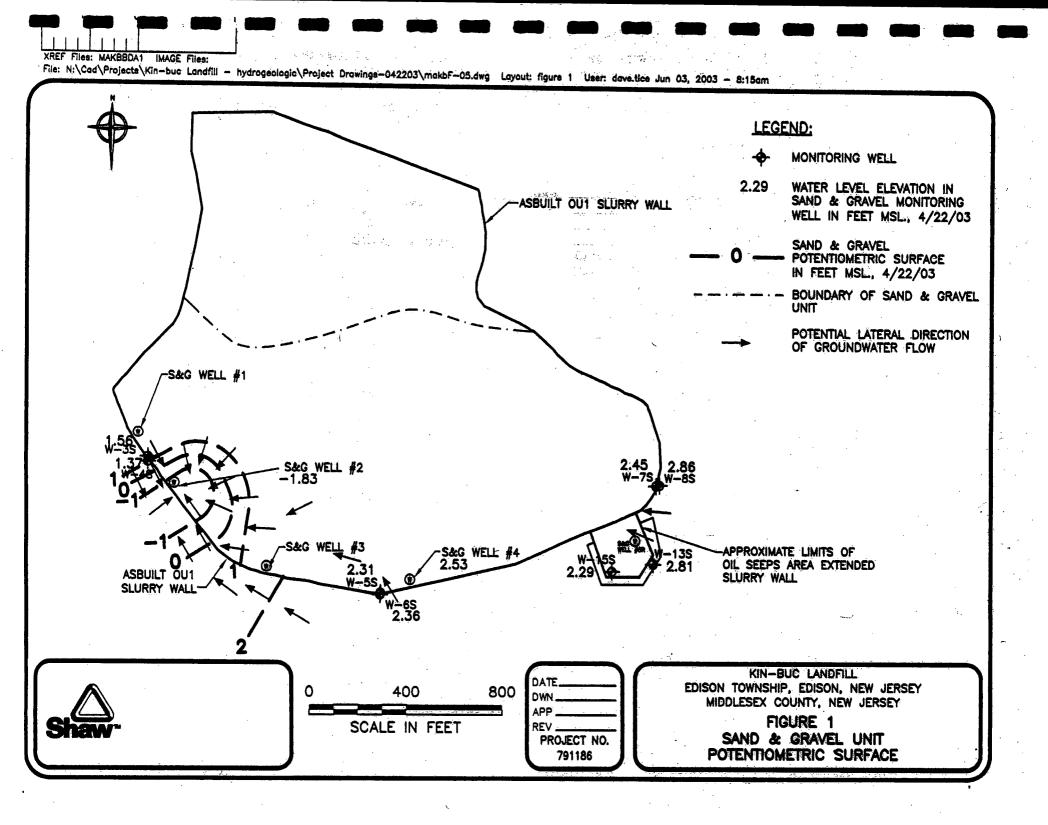
Attachments

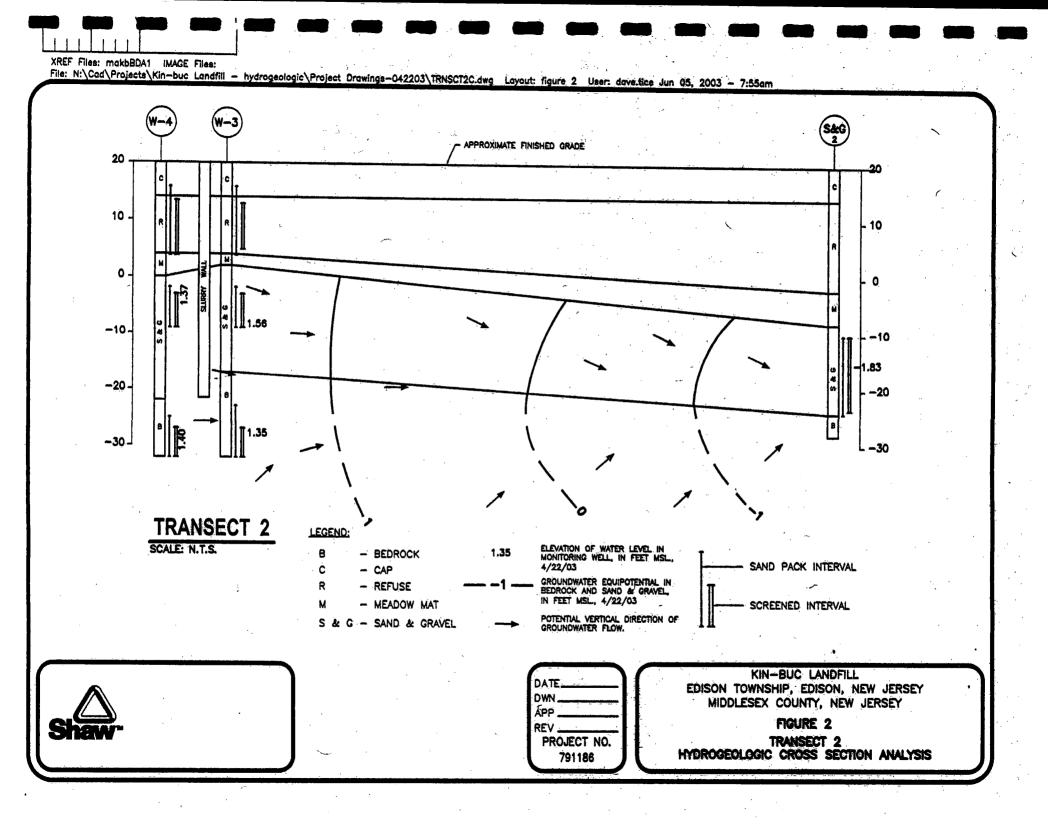
cc: Glenn Grieb, US Filter

Steve Golberg, EMCON/OWT, Inc.

Jeff Shanks, WM, Inc.

Justy 5 Pegans





XREF Files: makbBDA1 IMAGE Files: File: N:\Cad\Projects\Kin-buc Landfill - hydrogeologic\Project Drawings-031903\TRNSCT3B.dwg Layout: figure 3 User: dave tice May 30, 2003 - 10:26am APPROXIMATE FINISHED GRADE 20 10 0 -10 -20 -20 -30 **TRANSECT 3** LEGEND: SCALE: N.T.S. ELEVATION OF WATER LEVEL IN MONITORING WELL, IN FEET MSL., 2.31 - BEDROCK 4/22/03 SAND PACK INTERVAL - CAP GROUNDWATER EQUIPOTENTIAL IN BEDROCK AND SAND & GRAVEL, IN FEET MSL., 4/22/03 - REFUSE - MEADOW MAT SCREENED INTERVAL POTENTIAL VERTICAL DIRECTION OF GROUNDWATER FLOW. - SAND & GRAVEL KIN-BUC LANDFILL EDISON TOWNSHIP, EDISON, NEW JERSEY MIDDLESEX COUNTY, NEW JERSEY APP FIGURE 3 REV. **TRANSECT 3** PROJECT NO. HYDROGEOLOGIC CROSS SECTION ANALYSIS 791186

XREF Files: makbBDA1 IMAGE Files: File: N:\Cad\Projects\Kin-buc Landfill - hydrogeologic\Project Drawinge-031903\TRNSCT4B.dwg Layout: Layout: User: dave.tice Jun 04, 2003 - 7:48am 20 APPROXIMATE FINISHED GRADE 10 10 ٥ -10 -20 -30-**TRANSECT** LEGEND: ELEVATION OF WATER LEVEL IN MONITORING WELL, IN FEET MSL., 4/22/03 SCALE: N.T.S. - BEDROCK 2.45 SAND PACK INTERVAL - CAP GROUNDWATER EQUIPOTENTIAL IN BEDROCK AND SAND & GRAVEL, IN FEET MSL, 4/22/03 - REFUSE SCREENED INTERVAL - MEADOW MAT POTENTIAL VERTICAL DIRECTION OF GROUNDWATER FLOW. - SAND & GRAVEL KIN-BUC LANDFILL EDISON TOWNSHIP, EDISON, NEW JERSEY MIDDLESEX COUNTY, NEW JERSEY FIGURE 4 REV. **TRANSECT 4** PROJECT NO. HYDROGEOLOGIC CROSS SECTION ANALYSIS 791186

Table 1 KinBuc Landfill Operable Units 1 and 2 Continuous Hydraulic Monitoring Results 2003

Minimum/Maximum/Average Water Elevations

| inside Siurry Wall | | | | | | Outside Slurry Wall | | | | | | |
|--------------------|----------------------|---------------------------------------|--|---------------------------------|---------|----------------------|--|---------------------------------------|---------------------------------|--|--|--|
| Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) | Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) | | | |
| W-1G | April | 11.25 | 11.27 | 11.25 | W-2G | April | 11.79 | 12.16 | 12.00 | | | |
| N-3G | April | 7.02 | 7.65 | 7:36 | W-4G | April | 11.29 | 12.04 | 11.63 | | | |
| W-3S | April | 0.31 | 1.83 | 1.02 | W-4S | April | -0.19 | 2.78 | 1.23 | | | |
| W-5G | April | 9.50 | 10.14 | 9.84 | W-6G | April | 13.09 | 14.60 | 13.75 | | | |
| W-5S | April | 1.21 | 2.68 | 1.89 | W-6S | April | 1.27 | 2.77 | 1.96 | | | |
| N-7S | April | 1,42 | 2.69 | 2.00 | W-8S | April | 2.10 | 5.27 | 2.70 | | | |
| W-15S | April | 1,10 | 4.35 | 2.62 | W-13S | April | 1.90 | 3.73 | 2.45 | | | |
| V-15G | April | 15.30 | 15.86 | 15.62 | W-13G | April | 6.48 | 6.91 | 6.70 | | | |
| W-9G | April | 7.13 | 7.60 | 7.35 | W-10G | April | 8.25 | 8.44 | 8.35 | | | |
| V-3RR | April | 0.03 | 1.94 | 0.94 | W-4R | April | -0.27 | 2.85 | 1.20 | | | |
| V-5R | April | 1.38 | 2.84 | 2.05 | W-6R | April | 1.47 | 2.91 | 2.13 | | | |
| V-7R | April | 1,51 | 2.77 | 2.09 | W-8RR | April | 2.05 | 5.21 | 2.66 | | | |

Table 2
KinBuc Landfill Operable Unit 1
April 2003
Troll Water Elevations vs. Manual Water Elevations

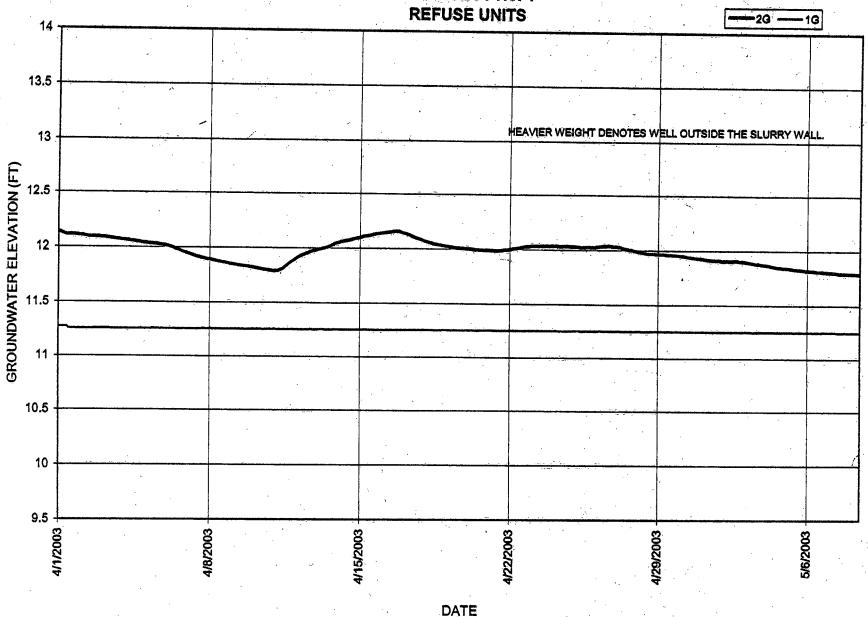
| OU 1 | May 8, 2003 | | | | | | | | |
|---------|-------------|--------|------------|--|--|--|--|--|--|
| Well ID | Troll | Manual | Difference | | | | | | |
| W-1G | 11.27 | 11.26 | 0.01 | | | | | | |
| W-2G | 11.73 | 11.74 | 0.01 | | | | | | |
| W-3G | 7.39 | 7.34 | 0.05 | | | | | | |
| W-3S | 0.91 | 0.98 | 0.07 | | | | | | |
| W-3RR | 0.74 | 0.75 | 0.01 | | | | | | |
| W-4G | 11.32 | 11.32 | 0.00 | | | | | | |
| W-4S | 0.91 | 0.91 | 0.00 | | | | | | |
| W-4R | 0.85 | 0.88 | 0.03 | | | | | | |
| W-5G | 9.86 | 9.91 | 0.05 | | | | | | |
| W-5\$ | 1.73 | 1.75 | 0.02 | | | | | | |
| W-5R | 1.64 | 1.67 | 0.03 | | | | | | |
| W-6G | 13.29 | 13,29 | 0.00 | | | | | | |
| W-6S | 1.80 | 1.84 | 0.04 | | | | | | |
| W-6R | 2.04 | 2.06 | 0.02 | | | | | | |
| W-7S | 1.88 | 1.92 | 0.04 | | | | | | |
| W-7R | 2.00 | 2.04 | 0.04 | | | | | | |
| W-8S | 2.66 | 2.71 | 0.05 | | | | | | |
| W-8RR | 2.64 | 2.62 | 0.02 | | | | | | |
| W-9G | 7.38 | 7.40 | 0.02 | | | | | | |
| W-10G | 8.31 | 8.32 | 0.01 | | | | | | |
| W-13G | 6.70 | 6.69 | 0.01 | | | | | | |
| W-13S | 2.47 | 2.47 | 0.00 | | | | | | |
| W-15G | 1.49 | 1.49 | 0.00 | | | | | | |
| W-15S | 2.41 | 2.44 | 0.03 | | | | | | |

Table 3 Kin-Buc Landfill Leachate Cleanout Monitoring 2003

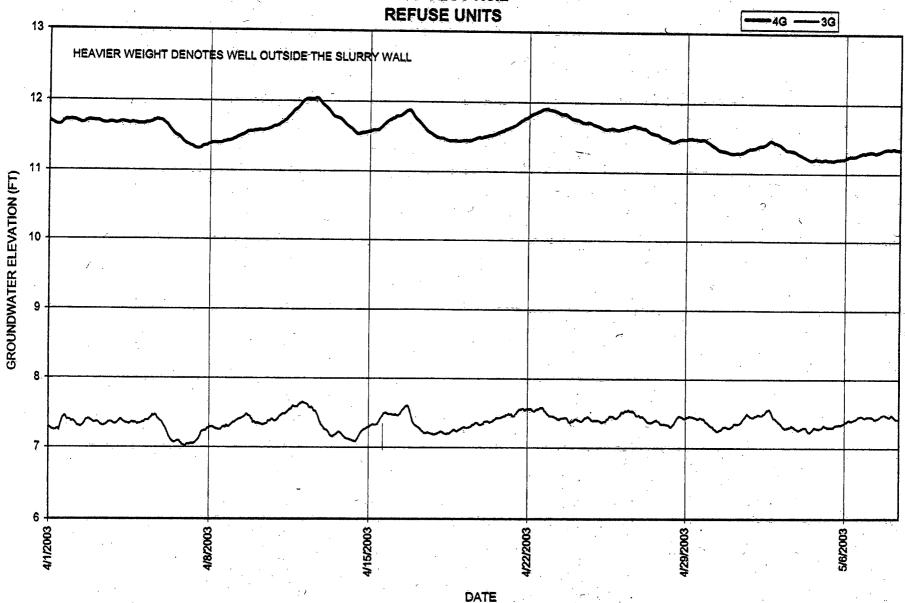
| Cleanout location | 14N 22.87 | | 1 | 14E | | 15N | | 15E | | 16N | | 105 | |
|--|----------------|--------------------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|---------------------|-----------|--|
| Elevation @ Sea Level Elevation Average | | | 22.77 | | 26.51 | | 26.51 | | 31.36 | | 16E 31.32 | | |
| | depth to water | | depth to | f . | depth to | | depth to | | depth to | | depth to | | |
| | water | elevation 10.09 | water | elevation | water | elevation | water | elevation | water | elevation | water | elevation | |
| | | 10.09 | | 10.06 | · · | 9.85 | | 9.93 | | na | , i | na | |
| DATE | | | | | | | | | | | | | |
| 12/10/2001 | 12.5 | 10.37 | 12.42 | 10.35 | 16.31 | 10.20 | 16.33 | 10.18 | dry | na | dry | na | |
| 1/3/2002 | 12.37 | 10.50 | 12.31 | 10.46 | 16.21 | 10.30 | 16.22 | 10.29 | dry | na | dry | na | |
| 2/13/2002 | 12.70 | 10.17 | 12.63 | 10.14 | 16.57 | 9.94 | 16.62 | 9.89 | dry | na | dry | na | |
| 3/27/2002 | 12.61 | 10.26 | 12.55 | 10.22 | 16.52 | 9.99 | 16,47 | 10.04 | dry | na | dry | na | |
| 4/19/2002 | 12.75 | 10.12 | 12.68 | 10.09 | 16.64 | 9.87 | 16.61 | 9.90 | dry | na | dry | na | |
| 5/3/2002 | 13.03 | 9.84 | 12.96 | 9.81 | 16.97 | 9.54 | 16,94 | 9.57 | dry | na | dry | na | |
| 6/5/2002 | 13.04 | 9.83 | 12.97 | 9.80 | 16.63 | 9.88 | 16.95 | 9.56 | dry | na | dry | na | |
| 7/8/2002 | 12.86 | 10.01 | 12.79 | 9.98 | 16.77 | 9.74 | 16.72 | 9.79 | dry | na | dry | na | |
| 8/2/2002 | 12.86 | 10.01 | 12.79 | 9.98 | 16.8 | 9.71 | 15.73 | 10.78 | dry | na | dry | na | |
| 9/5/2002 | 12.86 | 10.01 | 12.78 | 9.99 | 16.77 | 9.74 | 16.75 | 9.76 | dry | na | dry | na | |
| 9/26/2002 | 12.94 | 9,93 | 12.85 | 9.92 | 16.85 | 9.66 | 16.83 | 9.68 | dry | na | dry | | |
| 11/6/2002 | 12.64 | 10.23 | 12.58 | 10.19 | 16.59 | 9.92 | 16.48 | 10.03 | dry | na | dry | na | |
| 12/6/2002 | 13.02 | 9.85 | 12.94 | 9.83 | 16.97 | 9.54 | 16.95 | 9.56 | dry | na | | na | |
| 1/2/2003 | 13.07 | 9.80 | 13.00 | 9.77 | 17.03 | 9.48 | 17.01 | 9.50 | dry | | dry | na | |
| 2/12/2003 | 13.20 | 9.67 | 13.12 | 9.65 | 17.19 | 9.32 | 17.16 | 9.35 | dry | na | dry | na | |
| 3/4/2003 | 13.21 | 9.66 | 13.15 | 9.62 | 17.22 | 9.29 | 17.10 | 9.31 | dry | na | dry | na | |
| 4/1/2003 | 12.90 | 9.97 | 12.83 | 9.94 | 16.82 | 9.69 | 16.79 | 9.72 | | na | dry | na | |
| 5/8/2003 | 13.05 | 9.82 | 12.97 | 9.80 | 17.01 | 9.50 | 16.96 | 9.72 | dry | na | dry | na na | |
| 0,0,200 | 10.00 | U.UL | 12.31 | 9.00 | 17.01 | 9.00 | 10.90 | 9.55 | dry | na | dry | na | |

ATTACHMENT 1

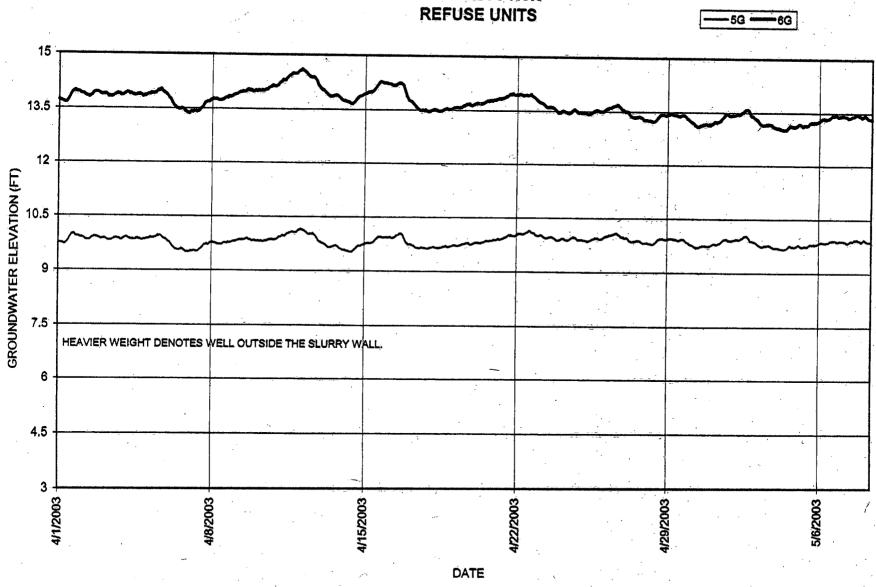
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #1 TRANSECT No. 1



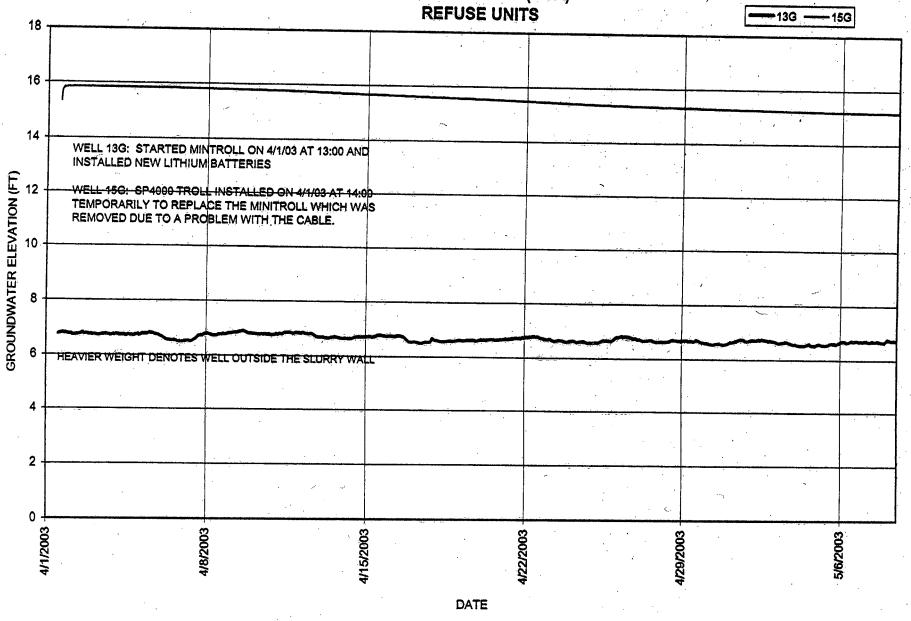
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #2 TRANSECT No.2



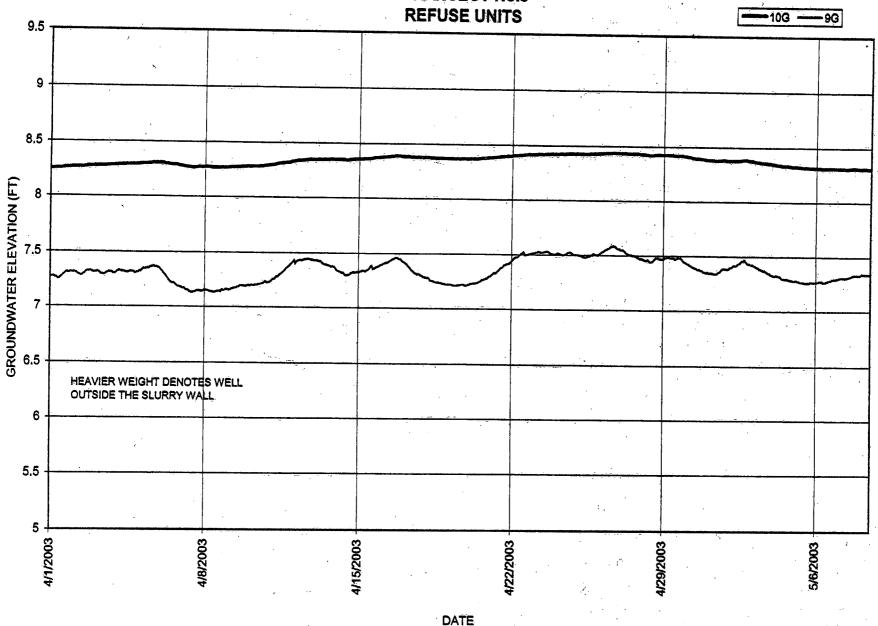
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH # 3 TRANSECT No.3

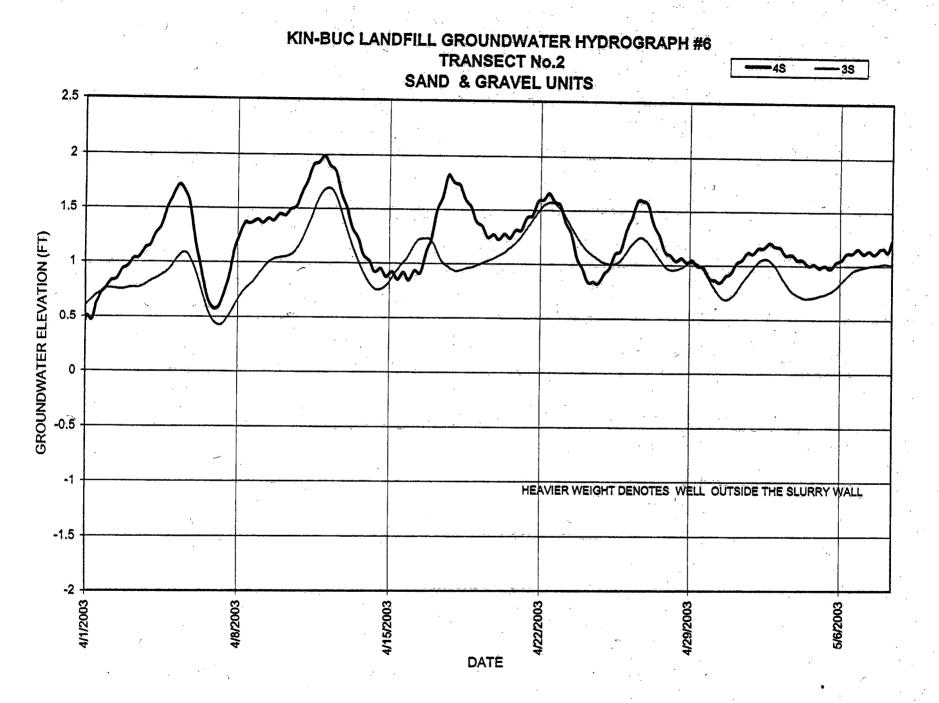


KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #4 TRANSECT No.4 (OSA)

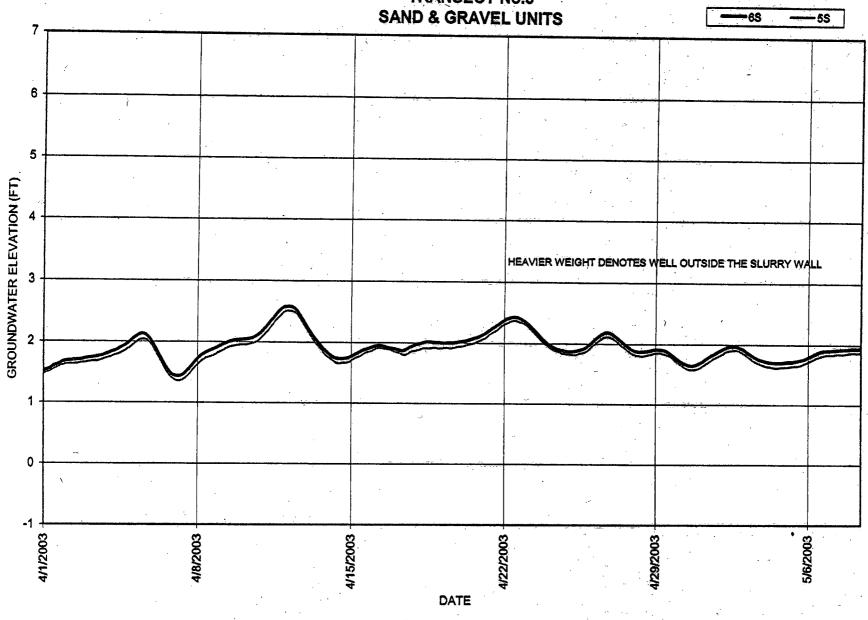


KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #5 TRANSECT No.5

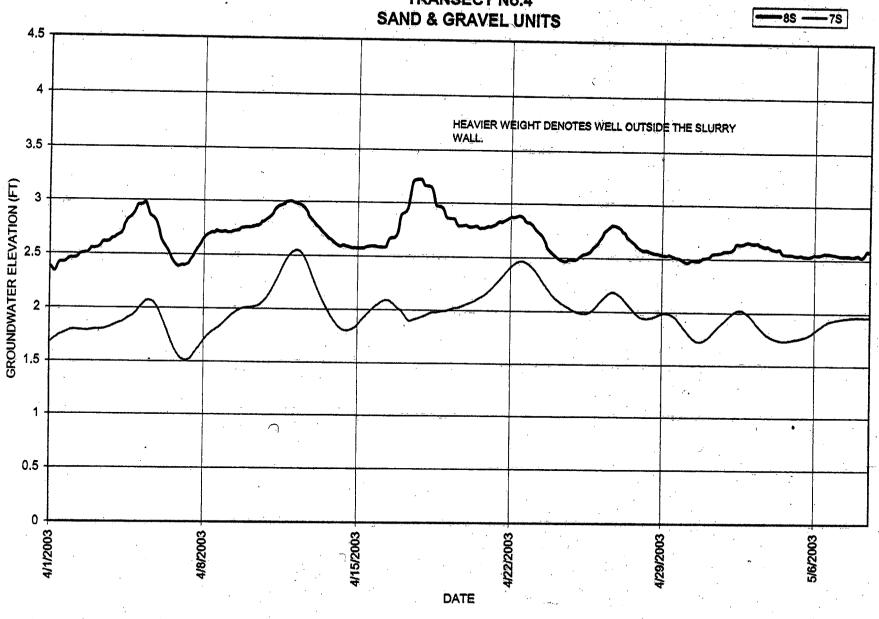




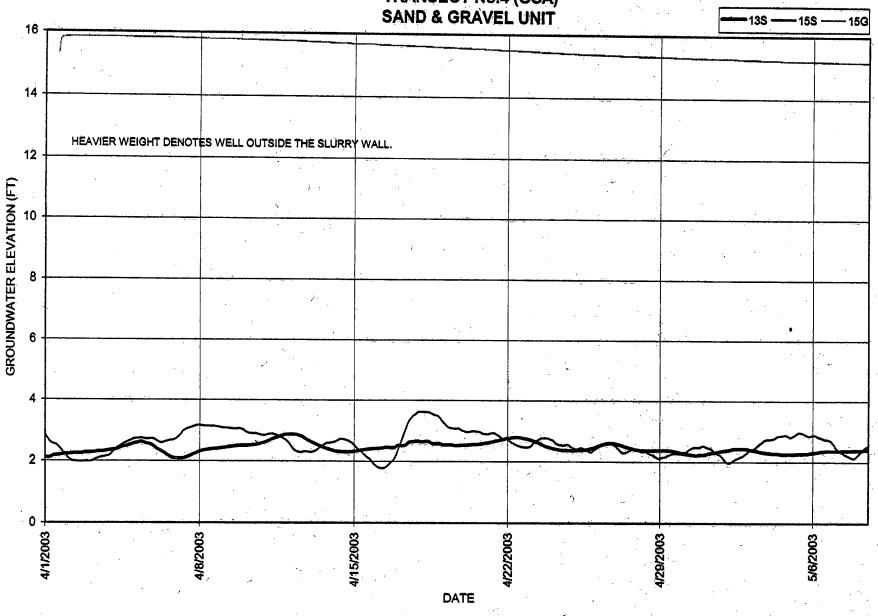
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #7 TRANSECT No.3



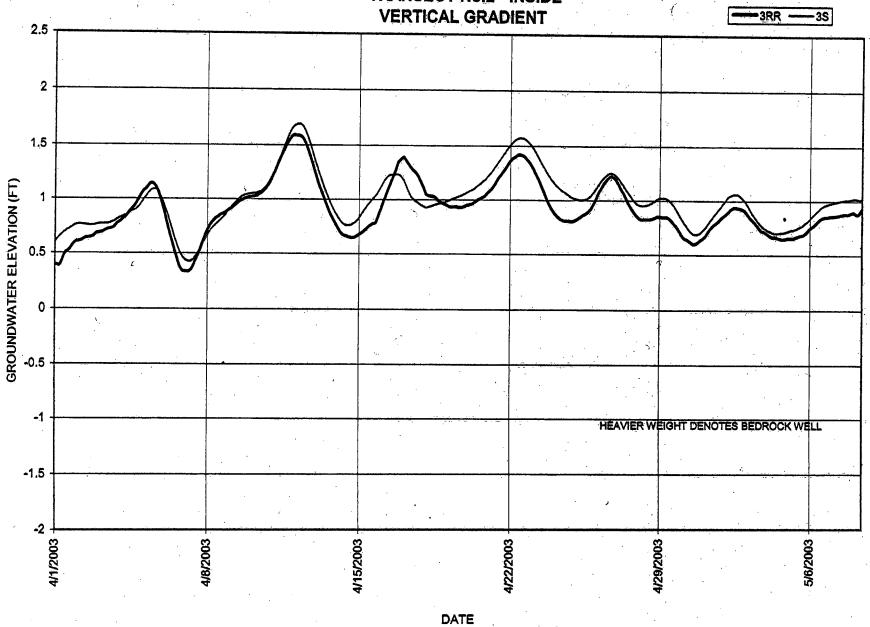
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #8 TRANSECT No.4



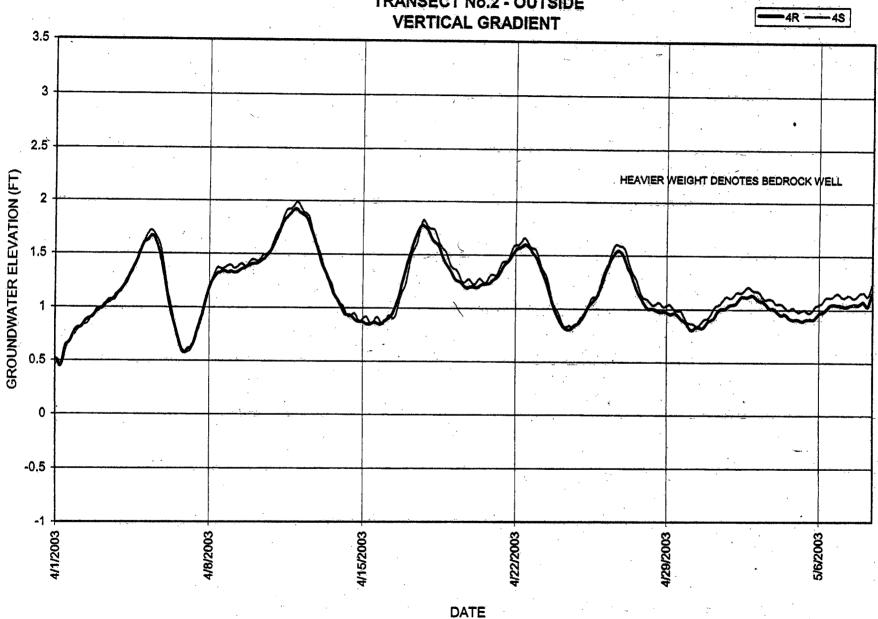
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #9 TRANSECT No.4 (OSA) SAND & GRAVEL UNIT



KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #10 TRANSECT No.2 - INSIDE



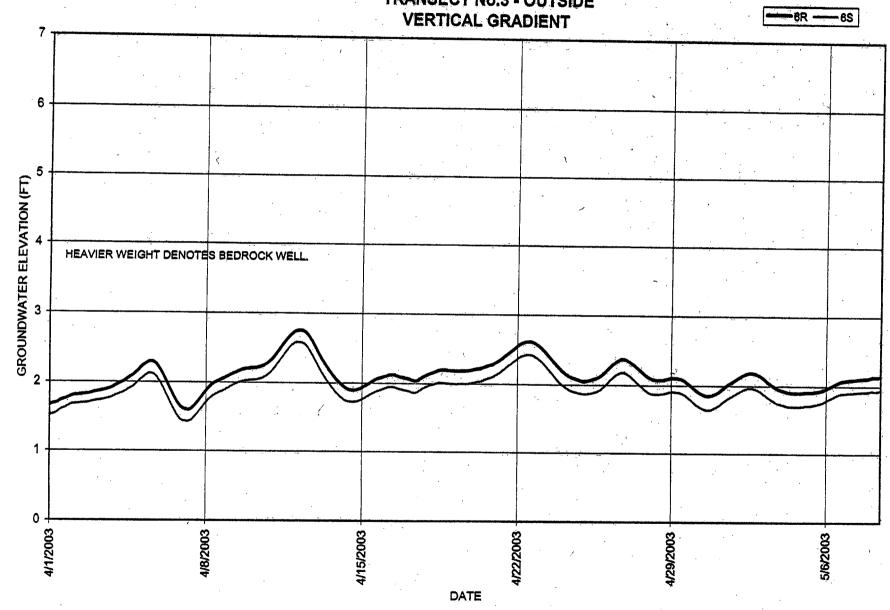
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #11 TRANSECT No.2 - OUTSIDE



KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #12 TRANSECT No.3 - INSIDE **VERTICAL GRADIENT** 3.5 3 2.5 GROUNDWATER ELEVATION (FT) -0.5 4/8/2003 4/1/2003 4/15/2003

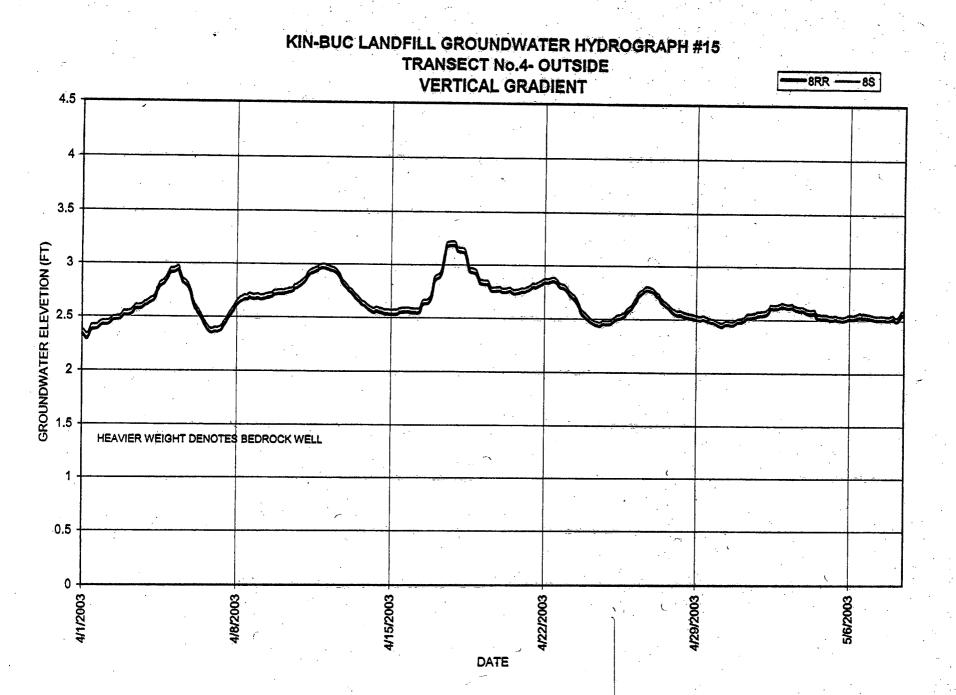
DATE

KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #13 TRANSECT No.3 - OUTSIDE



KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #14 TRANSECT No.4- INSIDE **VERTICAL GRADIENT** 3.5 3 2.5 GROUNDWATER ELEVATION (FT) HEAVIER WEIGHT DENOTES BEDROCK WELL 0 -0.5 4/8/2003 4/1/2003 4/15/2003

DATE



ATTACHMENT 2



IT Corporation

Crossroads Corporate Center
Oute International Boulevard, Suite 700
Mahvish, NJ 07495-0086
Tel. 201.512.5700
Fax. 201.512.5786

A Member of The IT Group

June 27, 2001 Project 796201

Carl Januszkiewicz
Waste Management, Inc
Kin-Buc Landfill Treatment Plant
383 Meadow Road
Bdison, NJ 08817

Re: Evaluation of Head Levels at Transcot 1

Doar Mr. Januszkiewicz:

We have completed an evaluation of the hydraulic characteristics at Transect I with specific focus on the lack of intragradient conditions associated with the high water levels in W-1G (inside of the slurry wall) relative to those levels in W-2G (outside of the wall).

While intragradient conditions were evident at the outset of the hydraulic monitoring program in April 1996, these conditions have generally not been maintained. Specifically, based on a review of historical hydrographs, intragradient conditions were evident initially from approximately April to July 1996, and April to June 1997. Thereafter, to more recent events, intragradient conditions have been observed intermittently and for shorter periods of time.

Attachment I presents a hydrograph at Transect I encompassing the period from September 1998 to December 2000. As seen on the hydrograph, there were periods of time when intragradient conditions were not being maintained.

As opposed to the other "G" series monitoring wells that are located in refuse, wells 1G and 2G at Transect 1 are actually located in a silt and clay deposit. Attachment 2 contains the boring logs for these 2 installations. In-situ hydraulic conductivity testing performed at Transect 1 indicated permeabilities of 10⁻⁷ cm/sec and 10⁻³ cm/sec in W-1G and W-2G, respectively. Accordingly, a source of recharge to the overburden soils in the area of W-1G would not readily drain away, and therefore, higher heads could result.

Well 1G sampling events (November 1998, October 1999, October 2000) can be seen on the hydrograph as sharp vertical drops in groundwater levels. Due to the low permeability of the surrounding materials, the groundwater levels required several months to recover. Since the final cover extends 10 feet past the slurry wall, the source of the groundwater that is recharging W-1G is unknown at present.

The hydraulic gradient between W-IG and W-IR is vertically downward which rules out the bedrock as being a source of groundwater recharge. Based on a recent visual inspection of the area around Transect I, the cap appears to be good condition and there were no signs that the cap integrity has been compromised.

Figure 1 depicts the conceptual model of the hydraulic interrelationship across Transect 1 showing water level measurements that depict the lack of intragradient conditions across the

Carl Januszkiewicz June 27, 2001 Page 2

Project 796201

slurty wall. The head levels in W-2G (outside the slurry wall) are generally at elevation 12 to 13 feet msl with periodic and short term increases to about 15 feet msl. The water level in the well sometimes falls below the level of the transducer. This is characterized by a flat straight line on the hydrographs as shown on Attachment 1. Head levels in W-1G (inside the slurry wall), on the other hand, are often greater with elevations as high as 15 to 16 feet msl being recorded.

It is evident from a review of Figure 1 that the drop in topography outside of the slurry wall toward Mill Brook, coupled with the higher permeability of W-2G relative to W-1G, would promote a more rapid decrease of head levels in the latter. This suggests that intragradient conditions may not be consistently attainable at this transect in any event. This notwithstanding however, and as depicted on Figure 1, it is important to note that the leachate collection system represents a hydraulic sink within the containment system. As such, groundwater in the vicinity of W-1G would drain toward the sink mitigating concerns of outward flow.

The leachate collection line runs parallel to the slurry wall and at its closest point is only about 20 feet away from Transect I. Several cleanouts are located along the collection line with the closest, Cleanout 16, only about 65 feet from Transect I. Leachate level measurements obtained from the cleanouts during December 2000 and June 2001 indicate a leachate level of 10 to 11 feet msl along the collection line as shown in Table 1. The leachate levels observed suggest that the leachate collection system is presently operating effectively.

Recommendations

Based on the above, it is recommended that during subsequent monitoring events at the site, measurements of leachate levels in Cleanouts 14 through 16 be recorded to verify that the leachate collection system is operating effectively. If liquid levels in the cleanouts increase above 12 to 13 feet msl, then maintenance of the collection line is recommended. Subsequent reports to EPA should include a discussion of the leachate collection system and its role as serving as a hydraulic sink within the containment system.

We trust you find this information useful. If you have any questions, please do not hesitate to

Sincerely,

IT Corporation

Steven Goldberg, Ph.D, CPG

Senior Hydrogeologist

Thomas M. Connors, P.E.

Project Manager

Attachments

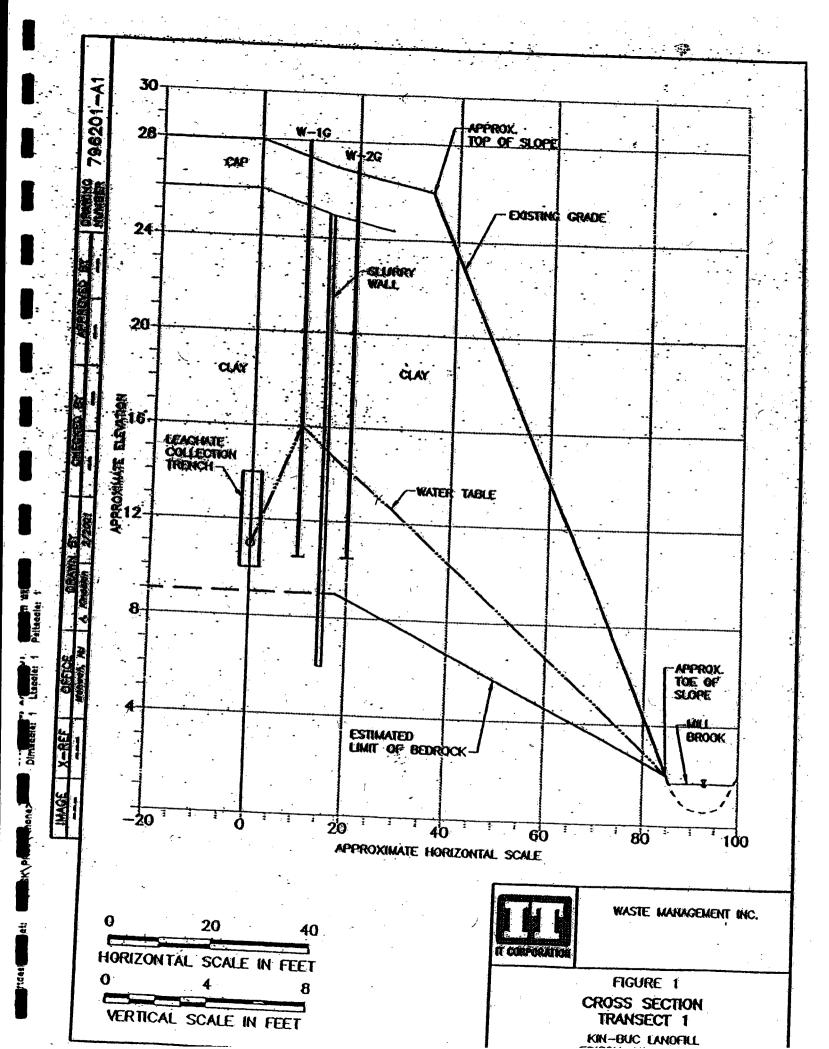
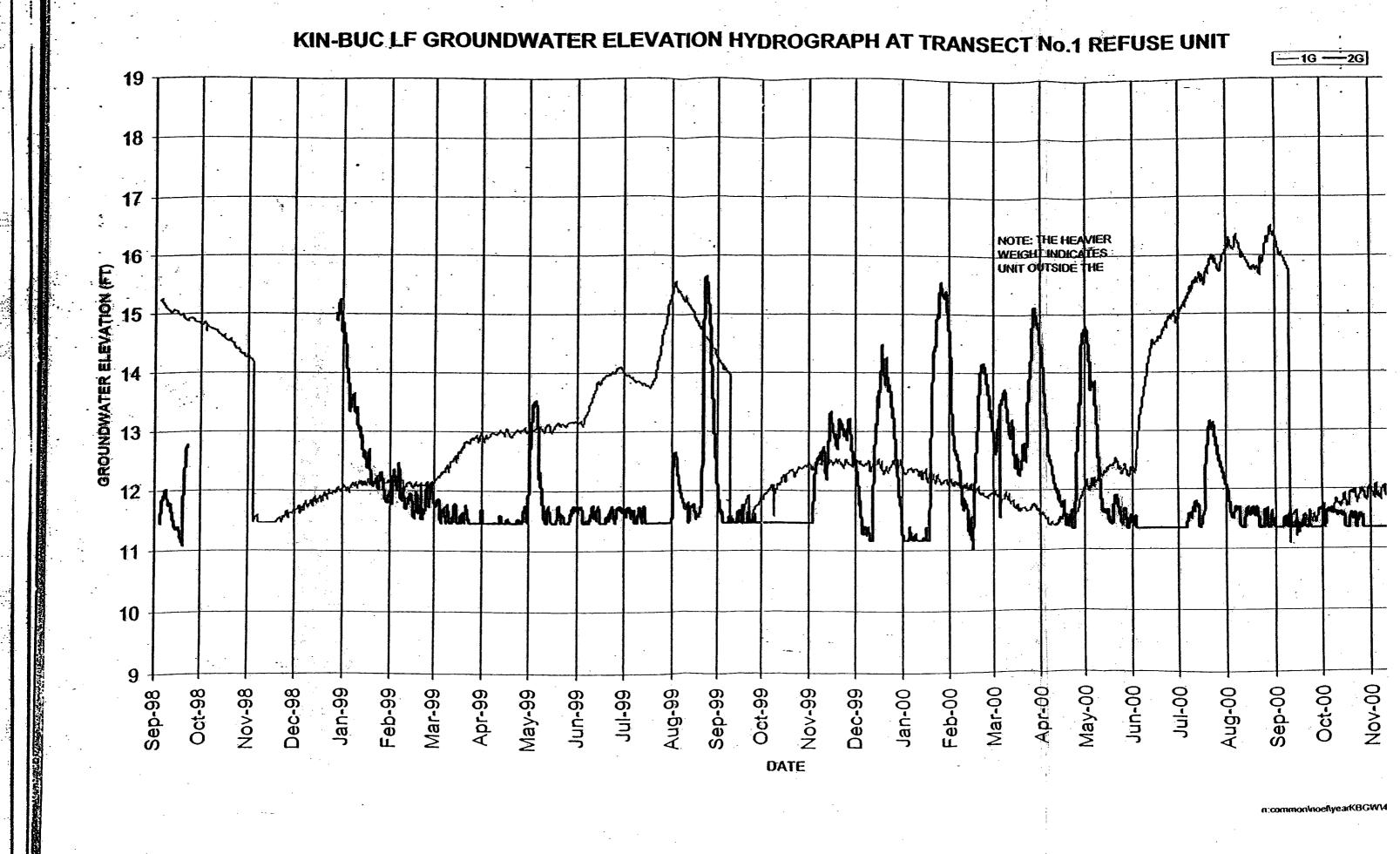


Table 1 Kin-Buc Landfill Leachate Cleanout Monitoring 2001

| leanout location levation @ Sea Level | 14N 22.87 | | 14E 22.77 | | 15N 26.51 | | 16E | | 169 | | 168 | |
|--|--------------------------|--------------------------|--------------------------|--------------------|--|-----------|-------------------------------------|----------------------|------------------------|--|------------------------------|---|
| | depth to water elevation | | depth to | | depth to | | depth to | 8.51. | depth to | 1.26 | | 1.32 |
| levation Average | | 10.80 | | elevation 10.74 | Water | elevation | Water | elevation | Water | elevation | | elevati |
| DATE | | MANAGE TO S | | 10,74 | Commission of the Commission o | 10.66 | Contraction of the process | 10.67 | • | | | 11.1 |
| | | The second second second | and the same of the same | | | 2014 | | | | ALCOHOLD BY THE PARTY OF THE PA | SOLVINOR VILLERY DESCRIPTION | |
| 6/7/01 | 11.98 | 10.89 | 12.02 | 40.26 | | | er | Contract of Contract | Management of the same | 1 | | |
| 5/16/01 | 12,25 | 10.62 | 12,23 | 10.75 | 15.86 | 10.65 | 15.87 | 10,64 | dry | na | dry | |
| 4/26/01 | 12.36 | 10.51 | 12.35 | 10.54 | 15,96 | 10,55 | 15,96 | 10.55 | dry | na | dry | na |
| 3/21/01 | 11.80 | 11.07 | 11.75 | 10.42 | 15.99 | 10.52 | 16.01 | 10.50 | dry | na | dry | na |
| 2/26/01 | 12.03 | 10.84 | 11.94 | 10.83 | 15.62 | 10.89 | 15.59 | 10.92 | dry | na | dry | na na |
| 1/29/01 | 12.08 | 10.79 | 11.98 | | 15.95 | 10.56 | 15.92 | 10.59 | dry | na | dry | na |
| 12/27/01 | 12.02 | 10.85 | 11.94 | 10.79 | 15.85 | 10.66 | 15.83 | 10.68 | · dry | na | 20,41 | 10.91 |
| | | | (1,94 | 10,83 | 15.72 | 10.79 | 15.68 | 10.83 | dry | na | 20.01 | |
| | | | | | | | | | | | 20.01 | 11.31 |
| | - | | | | | | | | 1 | - | | |
| | | | 197 | | | | | | | | | |
| | - | | | | | | | | | | | , |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | *************************************** |
| | | | | | - | | | | | | | · |
| | | | | | | | | | | | | |
| , | 1.7 | | | | | | | | | | | |
| | | | - | | | | | | | 10.00 | . 1 | |
| | | | | | | | | | | | | |
| | | | | | | | | | | • | | |
| | | | | | | | | Topological Company | | | | |
| | | - | | | | | м, | | | | | |



ATTACHMENT 2

MONITORING WELL RECORD

| OWNER IDENTIFICATION - Own | KIN DIC INC | | Alles Sheet Co | ordinates _ | 25 : 45 : 428 |
|--|--------------------------|-------------|---------------------------------------|-------------------|--|
| Nddress | 200 CONTINUAL | AVE | | | • |
| Xity | FIRSTANTA | | State | NY | · |
| | | | 36114 | - | Zip Code |
| VELL LOCATION - If not the same | as owner please give add | lress. | Owner's Well N | o, 20 | • |
| ddress 383 Headows Ro | Municipality 1309 | SON THE | | _ Lot No. | - son Block Ma |
| ounty HESPLESIEN ddress 383 Headows Ro YPE OF WELL (as per Well Pennit | antoon, ki | | · · · · · · · · · · · · · · · · · · · | | |
| (PE OF WELL (as per Well Pennik Igulatory Program Requiring Well | Calegories) Management | 9 | Date | Well comple | ted 2 , 15 , 95 |
| egulatory Program Requiring Well | CORTA | | Case | l.D. # | NJDØ49860836 |
| HSULTING FIRMFIELD SUPER | VISOR (il applicable) | • | | | Tala e |
| | | Depth to | | | |
| al depth drilled 15.6. ft. | | Top (fil) | Depth to Battom [ft.] | Olamete | |
| Il linished to 15 ft. | | from 1 | end surlace) | (inches) | Type and Material |
| ehole diameter: | Inner Casing | +4 | 5 | 2 | Sch 40 PVC |
| Top8in. | (Not Protective Cashig) | | - | | oen 40 LAP |
| lom <u>8</u> in. | Sotian | | 1 | | |
| was finished: Labove grade | (Note stor size) | .5 | 15. | 2 | Sch 40 PVC .010 |
| flush mounted | Tail Piece | | | | 10 110 .010 |
| shed above grade, casing a (slick up) above land | Gravel Pack | 3 | 1 | | |
| ce 4 fr | Annular Seal/Grout | | 15.6 | 8 | #00 Ricci |
| steal protective casing installed? | | 0 | 3 | 8 | Bentonite slurry |
| es Ano | Method of Grouting | tremi | e | | |
| water level after drilling | 4 | | | | |
| level was measured using - | | GEO | LOGIC LOG | geophys | of other geologic logs and/o ical logs should be attached |
| as developed for N/A hours | s at N/A gom | | 0 15 6 | | |
| of development N/A | Spm | | 0 - 15.6 | 1 | red dry stiff clay, |
| emanent pumping equipment inst | alled? Ve V | - | | | some silt |
| apacity N/A gpm | | 1 | | | |
| /pe: N/A | | | | | • |
| ARH botte | | | • | | |
| luid Type of | RigB-61 | | | | • |
| Draier Chad Chism | | - | | | |
| nd Safety Plan submitted? | Yes X No | | | | |
| Protection used on site (circle one) nse No. 0013753-001375 | None D C(B) A | | | | |
| nse No013753-001375 | · | - 1 | | • | • |
| 0.00 | DIN-HUBER, INC. | | | | |
| | | | | - | |
| | erenced wall in asset | | | | |
| | erenced well in accorda | nce with at | l well permit r | equiremen | its and all applicable |
| hal I have drilled the above-relies and regulations. | | nce with al | l well permit r | equiremen | its and all applicable |
| | | nce with al | l well permit r | equiremen Date | |

MONITORING WELL RECORD

| • | • | | Well Permit No. | | 46505 |
|---|--|---------------------------------------|------------------|---------------|--|
| | | • | Atlas Sheet Co | ordinales _ | 25 : 45 : 428 |
| OWNER IDENTIFICATION - Own | KIN-RIC INC | | | | |
| Vocasz | 200 CENTENTAL | AVE. | | | |
| City | PISCATAVAY | | State | NO | |
| 145711 4 000 | | | 3446 | | Zip Code |
| WELL LOCATION - If not the same | as owner please give add | iness. (| Owner's Well N | 0. 10 | |
| Address 183 Headows Ro | Municipality Example | | | Let No. | State Ass |
| Address | ad. Edison. NJ | SOLI THE | | | BIOCK NO |
| TYPE OF WELL (as per Well Pennil Regulatory Program Requiring Well | Calegories) | · · · · · · · · · · · · · · · · · · · | | | |
| Regulatory Program Requiring Well | HOUTTONIN | | Date | well comple | ted 2 / 15 / 95 |
| | The state of the s | • | Case | LD.# | MID049860836 |
| Signature series and the | VISOR (4 applicable) | | | | Tole. # |
| WELL CONSTRUCTION | | Do-Wa | | - | |
| Total depth drilled 15.6 ft. | | Depth to Top (ft.) | Depth to | Diamete | |
| Well linished to 15 ft. | | | Bottom (ff.) | (inches) | Type and Material |
| Borehole diameter: | Inner Casing | | | | |
| Too 8 in | Order Cara | | 5 | 2 | Sch 40 PVC |
| Bottom 8 in | (Not Protective Casing) | | | | |
| | Screen | · · · · · · · · · · · · · · · · · · · | | | |
| Vell was linished: Above grade | (Nace slot size) | 5 | 15 | 2 | Sch 40 PVC -020 |
| flush mounted | Tail Piece | . | | | |
| finished above grade, casing | Gravel Pack | 3 | 15.6 | 8 | 40.04 |
| eight (slick up) above land | Annular Seal/Grout | | 1 | • | #2 Ricci |
| | | . 0 | 5 | 8 | Bentonite slurry |
| as steel protective casing installed? | Method of Grouting | tremi | .e | · · · · | |
| Yes W No | | | | | |
| alic water level after drilling | ft. | GE | DLOGIC LOG | (Copies | of other geologic logs and/ |
| ater level was measured using | - | | | geophy | sical logs should be attache |
| ell was developed for N/A hou | s at N/A gom | | | | |
| thod of developmentN/A | Misself Misself | | 0 - 15.6 | | red gray dry stiff |
| s permanent pumping equipment ins | 1010-42 Dv D | | | | clay, some silt |
| rp capacity N/A gpm | ranaga [] Aes [X] No | • | | | |
| op type: N/A | | | | | |
| ing Method HSA | | | | | e de la companya del companya de la companya de la companya del companya de la co |
| on Class | | | | | |
| | 1 RigB-61 | | | • | |
| | | | | | |
| th and Salety Plan submitted? | Yes X No | | | | |
| of Protection used on site (circle one | None D CBA | 1 | | | |
| License No | | | - | | |
| of Drilling Company HA | RDIN-HUBER, INC. | - 1 | | | |
| | | | | - | |
| lify that I have drilled the above-re e rules and regulations. | terenced well in accord | ance with a | all well permit | requireme | nis and all annimates |
| - Samonia. | | | • | - 7 | and an approache |
| Driller's Signatur | 1/1/ | 2, | _ | ٠ | ų |
| Sime a Signatur | · Wach | 211 | ` | Date | 2/15/05 |

Canary - Driller

Pink - Owner

Goldenrod - Health Dept.

COPIES: White - DEP



One International Boulevard, Suite 700 Mahwah, NJ 07495-0086 201:512.5700 Fax 201:512.5786

July 1, 2003 Project 791186

Mr. Carl Januszkiewicz Waste Management, Inc. Kin-Buc Landfill Treatment Plant 383 Meadow Road Edison, NJ 08817

Re: Hydraulic Monitoring for May 2003

Dear Mr. Januszkiewicz:

A site visit was completed on June 3, 2003 to download the May water level recorder data and obtain manual water level measurements. The following is an update of the hydraulic monitoring for the month of May 2003 at the Kin-Buc Landfill. This information is to be included in the quarterly report, which is to be submitted to the EPA by mid-August 2003.

The minimum, maximum, and average water elevations recorded at each well are included in Table 1. Table 2 shows the troll water elevations versus the manual water elevations. The continuous water level elevation data when compared with manual readings indicated that the miniTrolls are functioning properly and are recording accurate data. The SP4000 Troll is still recording continuous hydraulic data in Well 15G.

Also, the data supplied for wells SG-1 and SG-3 showed the same water level for the entire period. These water levels should be fluctuating. The automated water level recording device in these wells need to be checked so that accurate readings can be obtained in the future.

Hydrographs have been prepared for each of the transect locations and are enclosed for your reference as Attachment No. 1. The water levels in wells on the outside of the slurry wall vary over the course of the day due to the tidal influence at the site. For clarity, Hydrograph Nos. 6 through 15 show the average water level in the well over a 24-hour period (12 hours before, and 12 hours after).

Refuse

As defined in the Record of Decision (ROD) for OU-1, the performance objective for the refuse unit calls for the pumping of leachate to establish inward gradients across the slurry wall with the additional benefit of reducing downward flow into the underlying sand and gravel unit. Based on the hydrographs the following is presented.

Transect 1-Refuse (1G/2G)/Hydrograph No. 1 - Intragradient conditions were observed during the entire month of May. The average monthly water elevation for May at Well 1G (inside) and Well 2G (outside) was 11.24 and 11.68 feet msl, respectively. Water level elevation measurements taken from Leachate Collection Cleanouts Nos. 14 through 16 are included in Table 3, and indicate that the leachate collection system is functioning properly. The fact that the leachate collection system is functioning properly suggests significant capture of leachate. The evaluation of the hydraulic conditions in the refuse at Transect 1 is provided in Attachment No.2.

Transect 2-Refuse (3G/4G)/Hydrograph No. 2 — Intragradient conditions were maintained throughout the month of May. The average monthly water elevation for the month at Well 3G (inside) and Well 4G (outside) was 7.32 and 11.17 feet msl, respectively

Transect 3-Refuse (5G/6G)/Hydrograph No. 3 — Intragradient conditions were maintained throughout the month of May. The average monthly water elevation for the month of May at Well 5G (inside) and Well 6G (outside) was 9.82 and 13.22 feet msl, respectively.

Transect 4-Refuse Oil Seeps Area (13G/15G)/Hydrograph No. 4 — Intragradient conditions were maintained throughout the month of May. The average monthly water elevation for the month of May at Well 15G (inside) and Well 13G (outside) was 1.53 and 6.69 feet msl, respectively.

Transect 5-Refuse (9G/10G)/Hydrograph No. 5 — Intragradient conditions were maintained throughout the month of May. The average monthly water elevation for the month of May at Well 9G (inside) and Well 10G (outside) was 7.31 and 8.28 feet msl, respectively.

Sand and Gravel/Bedrock

For the sand and gravel unit, the performance objectives call for pumping of sand and gravel groundwater to prevent flow toward the slurry wall and to impose upward hydraulic gradients from the bedrock to the sand and gravel. An additional benefit would be the establishment of inward gradients across the slurry wall within the sand and gravel unit. The following is a description of the flow characteristics based on visual observation of the hydrographs.

Horizontal Flow

Transect 2-Sand and Gravel (3S/4S)/Hydrograph No. 6 — Although intragradient conditions were not consistently maintained throughout the month of May, intragradient conditions were evident most of the month. Containment is being maintained by pumping

wells (see discussion in Conclusion). The average monthly water elevations for the month of May at Well 3S (inside) and Well 4S (outside) was 0.97 and 1.17 feet msl, respectively.

Transect 3-Sand and Gravel (5S/6S)/Hydrograph No. 7 — Slight intragradient conditions were maintained throughout the month of May. The average monthly water elevation for Well 5S (inside) and Well 6S (outside) was 1.81 and 1.86 feet msl, respectively.

Transect 4-Sand and Gravel (7S/8S)/Hydrograph No. 8- Intragradient conditions were maintained throughout the month of May. The average monthly water elevation for the month of May at Well 7S (inside) and Well 8S (outside) was 1.92 and 2.64 feet msl, respectively.

Transect 4 Sand and Gravel Oil Seeps Area (13S/15S)/Hydrograph No. 9 – Intragradient conditions were not evident during most of the month of May. The average monthly water elevation for the month of May at Well 15S (inside) and Well 13S (outside) was 2.64 and 2.39 feet msl, respectively. Water levels from Well 15G in the refuse unit are included on the hydrograph for comparison.

Vertical Flow-Inside Slurry Wall

Transect 2-Vertical Gradient (3S/3RR)-Inside/Hydrograph No.10 — Upward gradient conditions were not observed between the bedrock and overlying sand & gravel units inside the slurry wall for most of the month of May. The average monthly water elevation for the month of May at Well 3S (sand & gravel) and Well 3RR (bedrock) was 0.97 and 0.89 feet msl, respectively.

Transect 3-Vertical Gradient (5R/5S)-Inside/Hydrograph No. 12 — Upward gradient conditions were observed between the bedrock and overlying sand & gravel units inside the slurry wall for the month of May. The average monthly water elevation for the month of May at Well 5S (sand & gravel) and Well 5R (bedrock) was 1.81 and 1.93 feet msl, respectively.

Transect 4-Vertical Gradient (7R/7S)-Inside/Hydrograph No. 14 — Upward gradient conditions were observed between the bedrock and overlying sand & gravel units inside the slurry wall throughout the month of May. The average monthly water elevation for the month of May at Well 7S (sand & gravel) and Well 7R (bedrock) was 1.92 and 2.01 feet msl, respectively.

Page 4

Vertical Flow-Outside Slurry Wall

Transect 2-Vertical Gradient (4S/4R)-Outside/Hydrograph No. 11 — Upward gradient conditions were not observed between the bedrock and overlying sand & gravel units outside the slurry wall for the month of May. The average monthly water elevation for the month of May at Well 4S (sand & gravel) and Well 4R (bedrock) was 1.17 and 1.04 feet msl, respectively.

Transect 3-Vertical Gradient (6R/6S)-Outside/Hydrograph No. 13 — Upward gradient conditions were observed between the bedrock and overlying sand & gravel units outside the slurry wall for the month of May. The average monthly water elevation for the month of May at Well 6S (sand & gravel) and Well 6R (bedrock) was 1.86 and 2.03 feet msl, respectively.

Transect 4-Vertical Gradient (8RR/8S)-Outside/Hydrograph No. 15 — Upward gradient conditions were not observed between the bedrock and overlying sand & gravel units outside the slurry wall throughout the month of May. The average monthly water elevation for the month of May at both Well 8S (sand & gravel) and Well 8RR (bedrock) was 2.64 and 2.60 feet msl, respectively. The difference in average monthly water elevations for April was 0.04 feet.

An initial review of the hydrographs indicates that certain performance objectives associated with the sand and gravel and bedrock units may not be met, specifically associated with the uniform achievement of upward gradients from the bedrock to the overlying sand and gravel inside the wall (e.g. Hydrograph 10), and inward gradients across the slurry wall within the sand and gravel (Hydrographs 6 and 9). However previous investigations performed at the site would indicate that complete control of OU-1 groundwater can be achieved notwithstanding indications of downward flow from the sand and gravel to the bedrock, or outward flow across the slurry wall within the sand and gravel unit. This is based on the findings of the considerable pumping influence of the sand and gravel pumping wells, in particular S&G#2, in achieving hydraulic control at the site (see Groundwater Pumping Well Performance Evaluation Report, July 2000).

The influence of the pumping well can be demonstrated by review of a plan view groundwater contour map of the sand and gravel (Figure 1) and equipotential profiles and vector diagrams (Figures 1, 2, 3, and 4) that have been prepared for a period of time when the vertical gradient between the sand and gravel and the bedrock was downward at Transect 2. For this evaluation, a snapshot of groundwater elevations from the monitoring wells and pumping wells was obtained for May 20, 2003. At this time, S&G#2 was pumping at a rate of about 9.2 gallons per minute (gpm), while S&G#4 was pumping at a rate of 1.6 gpm. This resulted in a total of approximately 10.8 gpm or about 15,561 gallons per day. There was a downward vertical gradient observed the majority of the

time between the sand and gravel and the bedrock inside and outside the slurry wall at Transect No.2 in May as evidenced by higher heads in the sand and gravel wells relative to bedrock wells. Occasionally, there was also a higher head within the sand and gravel inside the slurry wall relative to the sand and gravel outside the slurry wall at Transect No. 2 in May.

Figures 1-4 incorporate the heads induced by pumping and show the considerable pumping influence of S&G#2. Specifically, groundwater flowing downward from the sand and gravel into the bedrock subsequently flows toward the pumping well. This occurs both inside and outside of the slurry wall. Also, groundwater within the sand and gravel unit flows toward the pumping well. The considerable pumping influence demonstrated at S&G#2, in conjunction with the fact that natural groundwater gradients in both the sand & gravel and bedrock flow predominantly towards the area of S&G#2, result in the complete capture of OU-1 groundwater at these pumping rates.

Groundwater and Leachate Collection

Based on data provided by U.S. Filter, the following volumes of groundwater and leachate were extracted from the sand & gravel wells and leachate collection system for the period from May 1 to May 31, 2003:

| S&G No. 1 Groundwater | S&G No. 2 Groundwater | S&G No. 3 Groundwater | S&G No. 4 Groundwater | Leachate |
|--------------------------|--------------------------|--------------------------|--------------------------|-------------|
| 0 gal. | 398,760 gal. | 51,233 gal. | 28,251 gal. | 43,717 gal. |
| 0 gpd | 12,863 gpd | 1,652 gpd | 911 gpd | 1,410 gpd |

For the month of May, a total of 478,244 gallons of groundwater was collected. The average daily groundwater extraction rate for all of the wells was 15,427 gpd. The extraction rate from S&G No. 2 was 12,863 gpd, 1,652 gpd for S&G No. 3, and the extraction rate from S&G No. 4 was 911 gpd. The leachate extraction rate was 1,410 gpd for the month of May.

CONCLUSIONS

Intragradient conditions were maintained in the refuse unit at Transects 1, 2, 3, 4, and 5.

Intragradient conditions are not usually maintained by the monitoring wells at Transect 1 (although they were for the month of May), although each month levels in the leachate collection system indicate intragradient conditions are present at this location.

Transducers in S&G#1 and S&G#3 need to be checked. The data for May 20, 2003 showed no change in water level throughout the day, suggesting that the transducers are not functioning properly.

Hydraulic control was maintained within OU-1 based on the analysis of the significant influence of S&G#2 in acting as a hydraulic sink for sand and gravel and bedrock groundwater. Groundwater flow in the sand and gravel and bedrock is ultimately captured by the pumping wells (S&G#2 and S&G#3 or 4) resulting in overall containment of groundwater in OU-1.

In view of the analysis presented herein, it is recommended that the combined groundwater pumping rates in the sand and gravel be maintained at 15,000 gpd with S&G#2 and S&G#3 pumping at 10,000 gpd and 5,000 gpd, respectively. These lower pumping rates will be evaluated to confirm continued hydraulic control of OU-1 groundwater.

We trust you find this information useful. If you have any questions, please do not hesitate to contact us.

EMCON/OWT, INC.

Tim Pagano, CPG

Senior Hydrogeologist

Laura Kisala

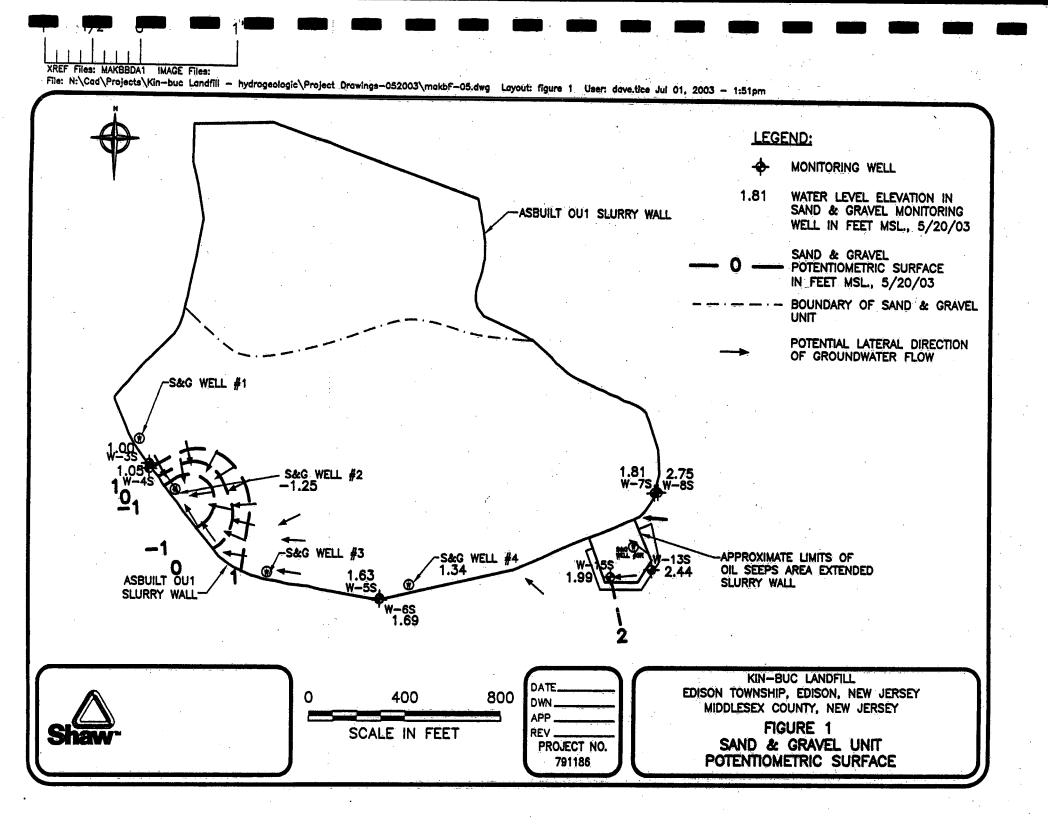
Environmental Scientist

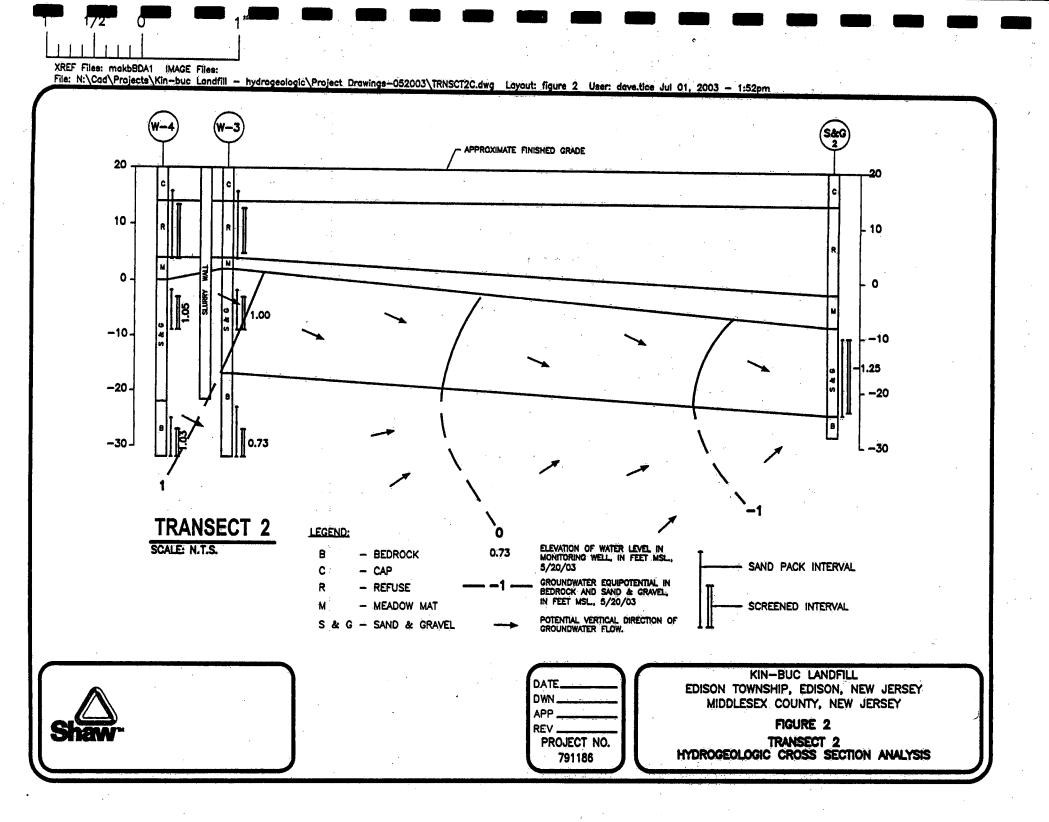
Attachments

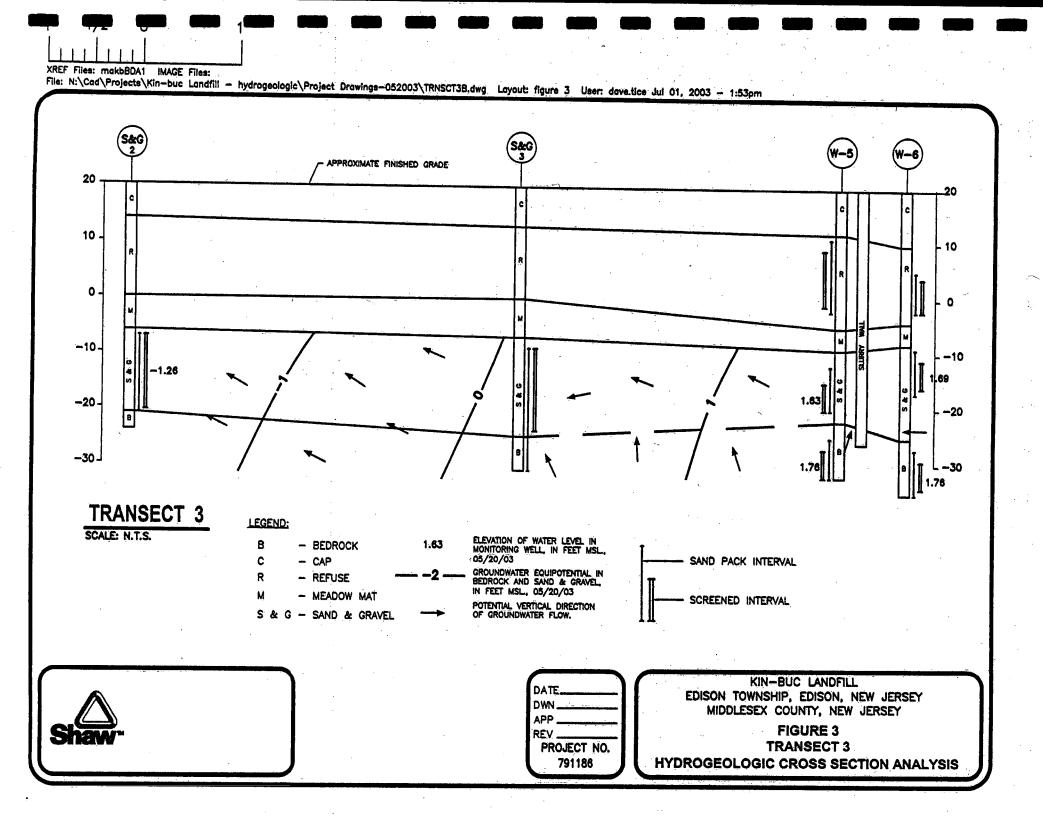
cc: Glenn Grieb, US Filter

Steve Golberg, EMCON/OWT, Inc.

Jeff Shanks, WM, Inc.







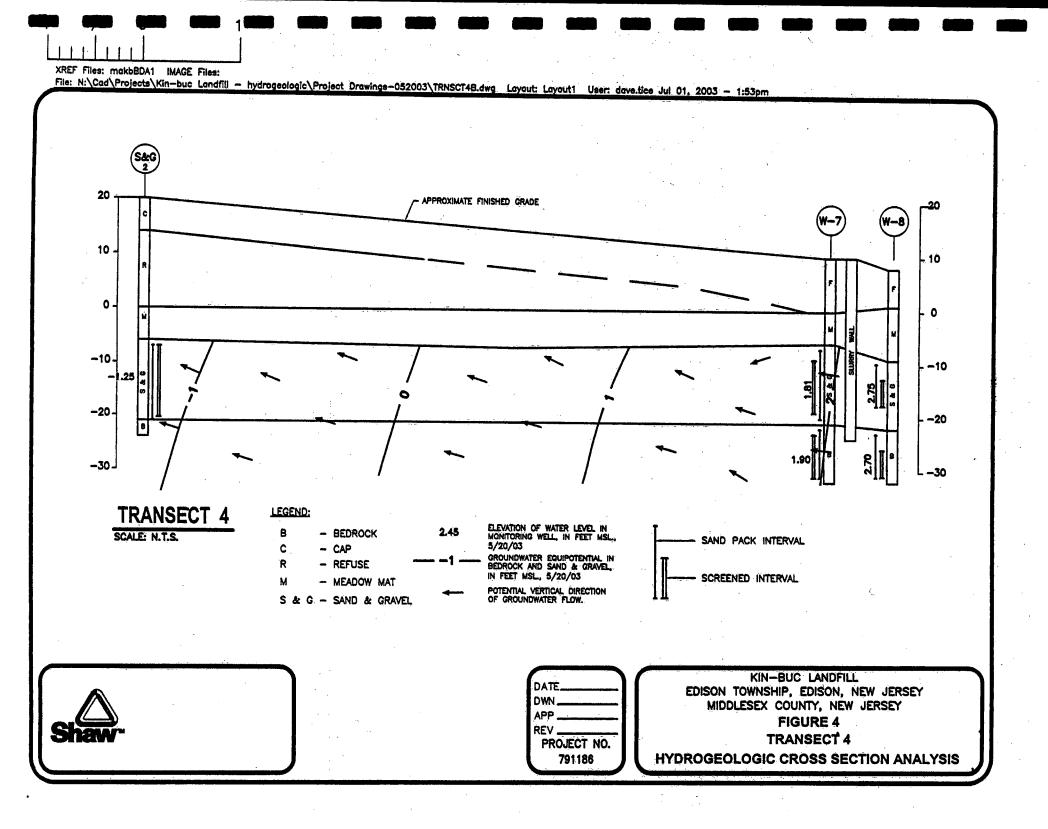


Table 1
KinBuc Landfill Operable Units 1 and 2
Continuous Hydraulic Monitoring Results
2003
Minimum/Maximum/Average Water Elevations

| | | Inside Sturry Wall | | | | | Outside Slurry Wall | | |
|---------|----------------------|--|--|---------------------------------|---------|----------------------|--|--|---------------------------------|
| Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) | Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) |
| W-1G | Aprii May | 11.25 11.23 | 11.27 11.25 | 11.25 11,24 | W-2G | April May | 11.79 11.47 | 12.16 11.93 | 12.00 11.68 |
| W-3G | April May | 7.02 6.84 | 7.65 7.58 | 7.36 7.32 | W-4G | April May | 11.29 10.80 | 12.04 11.48 | 11.63 11.17 |
| V-3S | April May | 0.31 0.43 | 1.83 1.53 | 1.02 0.97 | W-4S | April May | -0,19 0.00 | 2.78 2.46 | 1.23 1.17 |
| W-5G | April Mãy | 9.50 9.59 | 10.14 10.07 | 9.84 9.82 | W-6G | April May | 13.09 12.76 | 14.60 13.74 | 13.75 13.22 |
| V-5S | April May | 1.21 1.13 | 2.68 2.50 | 1.89 1.81 | W-6S | April May | 1.27 1.21 | 2,77 2.57 | 1.96 1.86 |
| V-7S | April May | 1.42 1.49 | 2.69 2.52 | 2.00 1.92 | W-8S | April May | 2.10 2.12 | 5.27 5.02 | 2.70 2.64 |
| V-15S | April May | 1.10 1.38 | 4.35 4.05 | 2.62 2.64 | W-13S | April May | 1.90 1.89 | 3.73 3.52 | 2.45 2.39 |
| V-15G | April May | 1.22 1.28 | 1.71 1.69 | 1.50 1.53 | W-13G | April May | 6.48 6.47 | 6.91 7.00 | 6.70 6.69 |
| V-9G | April May | 7.13 7.06 | 7.60 7.65 | 7.35 7.31 | W-10G | April May | 8.25 8.18 | 8.44 8.38 | 8.35 8.28 |
| V-3RR | April May | 0.03 -0.10 | 1.94 1.91 | 0.94 0.89 | W-4R | April May | -0.27 -0.25 | 2.85 2.36 | 1.20 1.04 |
| /-5R | April May | 1.38 1.24 | 2.84 2.61 | 2.05 1.93 | W-6R | April May | 1.47 1.47 | 2.91 2.66 | 2.13 2.03 |
| /-7R | April May | 1.51 1.59 | 2.77 2.62 | 2.09 2.01 | W-8RR | April May | 2.05 2.09 | 5.21 4.97 | 2.66 2.60 |

Table 2
KinBuc Landfill Operable Unit 1
May 2003
Troll Water Elevations vs. Manual Water Elevations

| QU 1 | | June 3, 2003 | | | | | | | | | |
|---------|-------|--------------|------------|--|--|--|--|--|--|--|--|
| Well ID | Troll | Manual | Difference | | | | | | | | |
| W-1G | 11.25 | 11.26 | 0.01 | | | | | | | | |
| W-2G | 11.60 | 11.62 | 0.02 | | | | | | | | |
| W-3G | 7.21 | 7.69 | 0.48 | | | | | | | | |
| W-3S | 0.67 | 0.75 | 0.08 | | | | | | | | |
| W-3RR | 0.55 | 0.57 | 0.02 | | | | | | | | |
| W-4G | 11.10 | 11.11 | 0.01 | | | | | | | | |
| W-4S | 0.78 | 0.78 | 0.00 | | | | | | | | |
| W-4R | 0.71 | 0.80 | 0.09 | | | | | | | | |
| W-5G | 9.68 | 9.75 | 0.07 | | | | | | | | |
| W-5S | 1.57 | 1.59 | 0.02 | | | | | | | | |
| W-5R | 1.44 | 1.48 | 0.04 | | | | | | | | |
| W-6G | 13.24 | 13.27 | 0.03 | | | | | | | | |
| W-6S | 1.62 | 1.66 | 0.04 | | | | | | | | |
| , W-6R | 1.73 | 1.79 | 0.06 | | | | | | | | |
| W-7S | 1.75 | 1.78 | 0.03 | | | | | | | | |

1.91

2.70

2.67

7.59

8.41

6.77

2.39

1.48

2.37

0.03

0.01

0.00

0.04

0.01

0.07

0.01

0.01

0.05

W-7R

W-8S

W-8RR

W-9G

W-10G

W-13G

W-13S

W-15G

W-15S

1.88

2.69

2.67

7.55

8.42

6.70

2.38

1.47

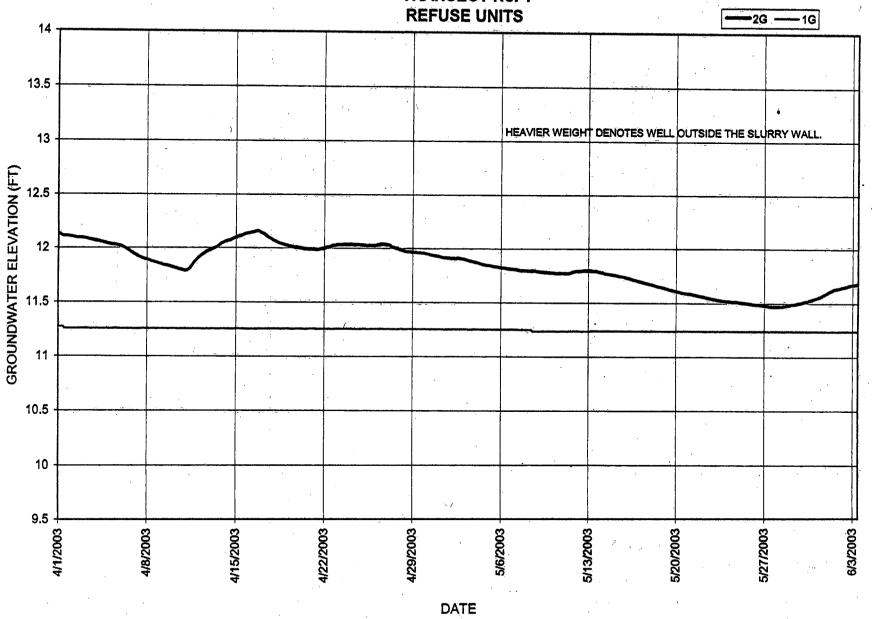
2.32

Table 3 Kin-Buc Landfill Leachate Cleanout Monitoring 2003

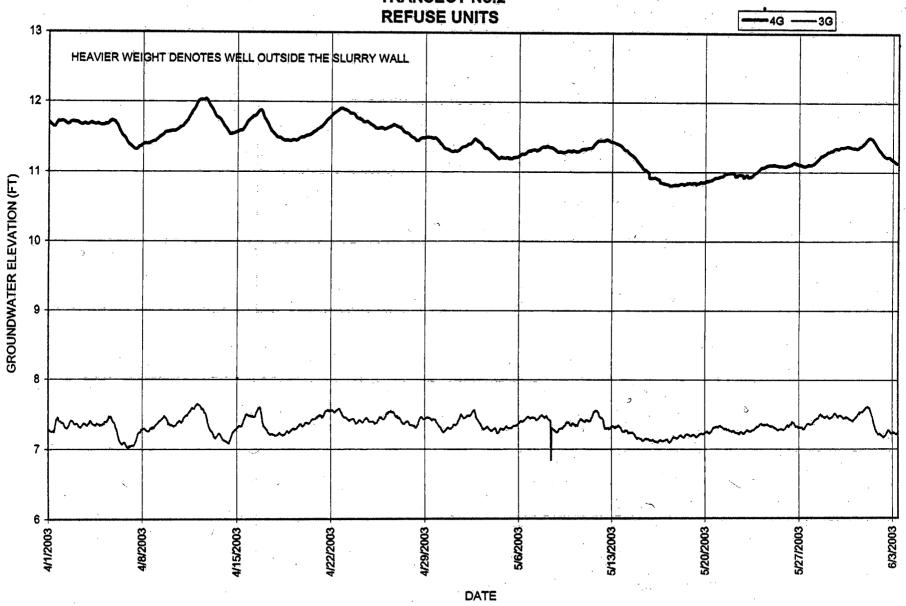
| Cleanout location | 1 | 4N | 1 | 4E | 1 | 5N | 1 | 15E | | 6N | 16E | |
|--|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------------|-----------|----------|-----------|
| Elevation @ Sea Level | 22,87 | | 22.77 | | 26.51 | | 26.51 | | 31,36 | | 31.32 | |
| | depth to | | depth to | | depth to | | depth to | depth to | | | depth to | |
| | water | elevation | water | elevation | | elevation | | elevation | depth to water | elevation | | elevation |
| Elevation Average | | 10.09 | | 10.06 | | 9.85 | | 9.93 | | na | | na |
| DATE | | 7 P. C. | | No. | | | | | | | | |
| 12/10/2001 | 12.5 | 10.37 | 12.42 | 10.35 | 16,31 | 10.20 | 16.33 | 10.18 | dry | na | dry | na |
| 1/3/2002 | 12.37 | 10.50 | 12.31 | 10.46 | 16.21 | 10.30 | 16.22 | 10.29 | dry | na | dry | na |
| 2/13/2002 | 12.70 | 10.17 | 12.63 | 10.14 | 16.57 | 9.94 | 16.62 | 9.89 | dry | na | dry | na |
| 3/27/2002 | 12.61 | 10.26 | 12.55 | 10.22 | 16.52 | 9.99 | 16.47 | 10.04 | dry | na | dry | na |
| 4/19/2002 | 12.75 | 10.12 | 12.68 | 10.09 | 16.64 | 9.87 | 16.61 | 9.90 | dry | na | dry | na |
| 5/3/2002 | 13.03 | 9.84 | 12.96 | 9.81 | 16.97 | 9.54 | 16.94 | 9.57 | dry | na | dry | na |
| 6/5/2002 | 13.04 | 9.83 | 12.97 | 9.80 | 16.63 | 9.88 | 16.95 | 9.56 | dry | na | dry | na |
| 7/8/2002 | 12.86 | 10.01 | 12.79 | 9.98 | 16.77 | 9.74 | 16.72 | 9.79 | dry | na | dry | na |
| 8/2/2002 | 12.86 | 10.01 | 12.79 | 9.98 | 16.8 | 9.71 | 15.73 | 10.78 | dry | na | dry | na |
| 9/5/2002 | 12.86 | 10.01 | 12.78 | 9.99 | 16.77 | 9.74 | 16.75 | 9.76 | dry | na | dry | na |
| 9/26/2002 | 12.94 | 9.93 | 12.85 | 9.92 | 16.85 | 9,66 | 16,83 | 9.68 | dry | na | dry | na |
| 11/6/2002 | 12.64 | 10.23 | 12.58 | 10.19 | 16.59 | 9.92 | 16.48 | 10.03 | dry | na | dry | na |
| 12/6/2002 | 13.02 | 9.85 | 12,94 | 9.83 | 16.97 | 9.54 | 16.95 | 9.56 | dry | na | dry | na |
| 1/2/2003 | 13.07 | 9.80 | 13.00 | 9.77 | 17.03 | 9.48 | 17.01 | 9.50 | dry | na | dry | na |
| 2/12/2003 | 13.20 | 9.67 | 13.12 | 9.65 | 17.19 | 9.32 | 17.16 | 9.35 | dry | na | dry | na |
| 3/4/2003 | 13.21 | 9.66 | 13.15 | 9.62 | 17.22 | 9.29 | 17.20 | 9,31 | dry | na | dry | na |
| 4/1/2003 | 12.90 | 9.97 | 12.83 | 9.94 | 16.82 | 9.69 | 16.79 | 9.72 | dry | na | dry | na |
| 5/8/2003 | 13.05 | 9.82 | 12.97 | 9.80 | 17.01 | 9.50 | 16.96 | 9.55 | dry | na | dry | na |
| 6/3/2003 | 13.11 | 9.76 | 13,14 | 9.63 | 17.09 | 9.42 | 17.04 | 9,47 | dry | na | dry | na |
| A CONTRACTOR OF THE CONTRACTOR | | | | ····· | *** | | | | | , | | |

ATTACHMENT 1

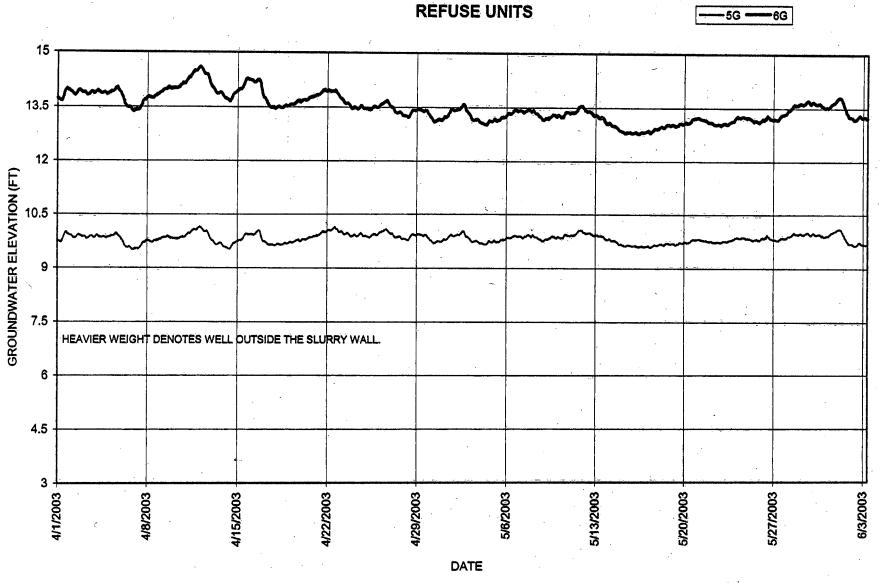
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #1 TRANSECT No. 1



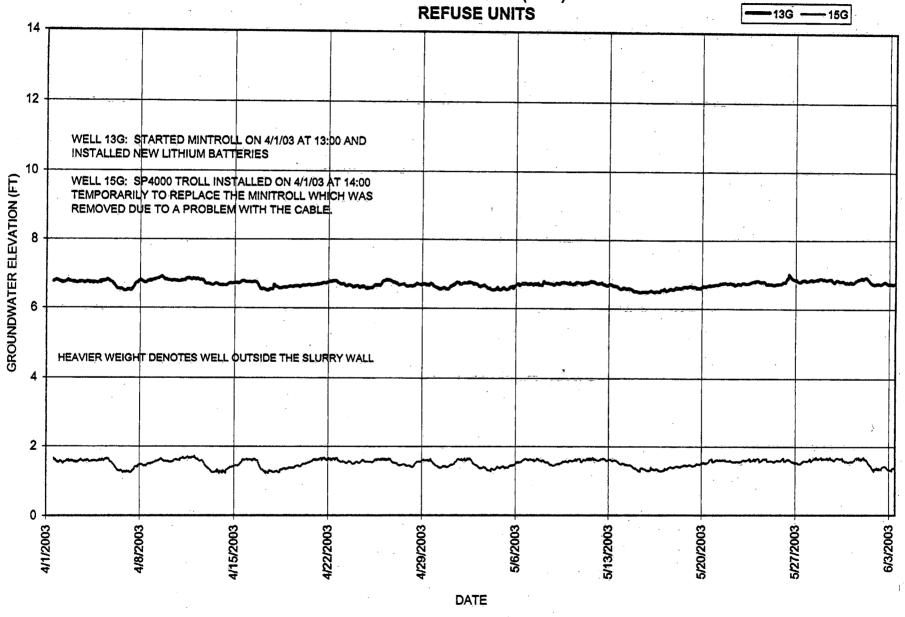
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #2 TRANSECT No.2



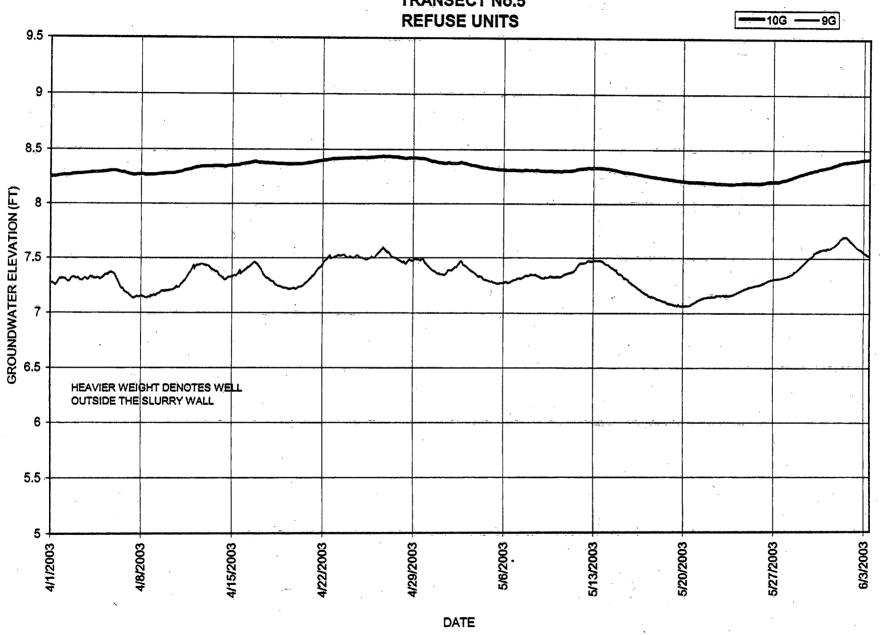
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH # 3 TRANSECT No.3



KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #4 TRANSECT No.4 (OSA)



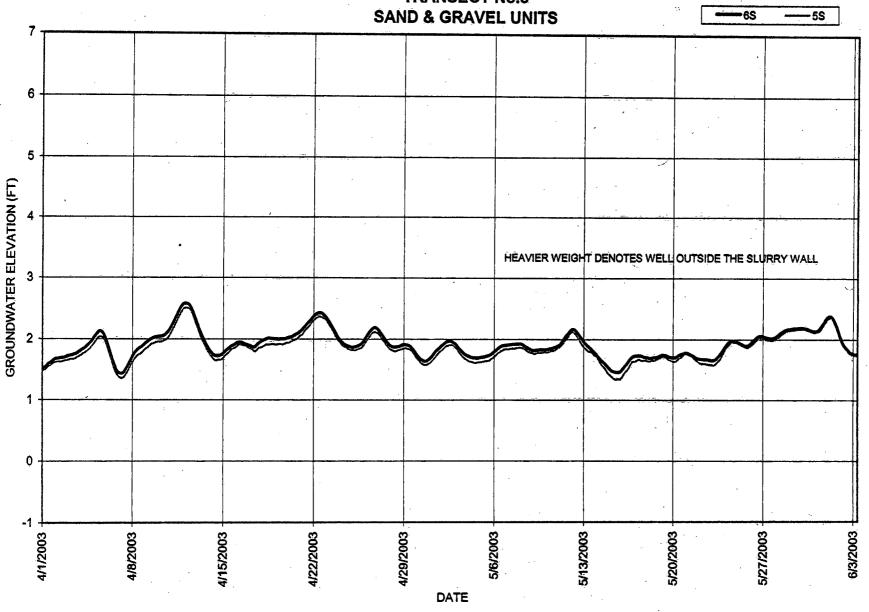
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #5 TRANSECT No.5



KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #6 **TRANSECT No.2** -48 **SAND & GRAVEL UNITS** 2.5 2 1.5 GROUNDWATER ELEVATION (FT) -1 HEAVIER WEIGHT DENOTES WELL OUTSIDE THE STURRY WALL -1.5 -2 4/1/2003 4/8/2003 5/6/2003 4/15/2003 4/29/2003 5/13/2003 5/20/2003 5/27/2003 4/22/2003

DATE

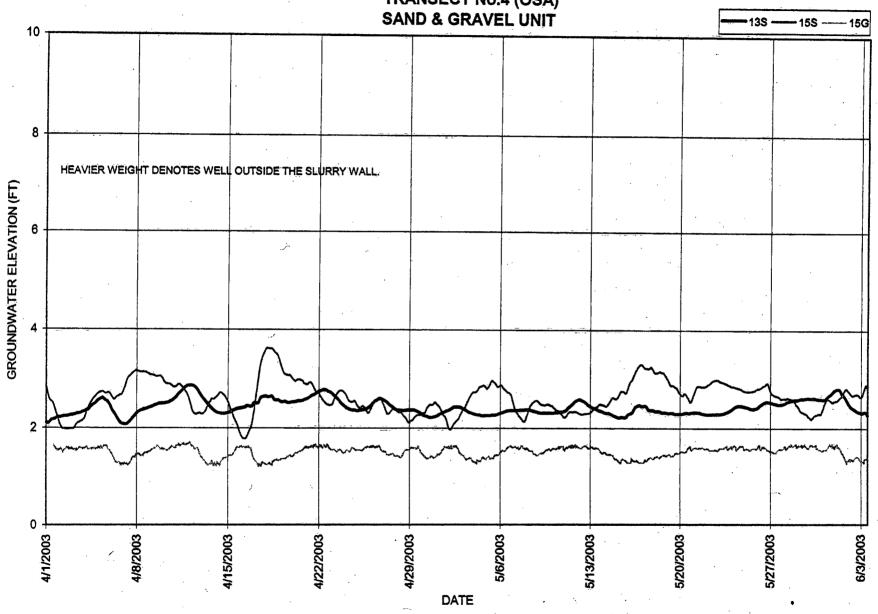
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #7 TRANSECT No.3



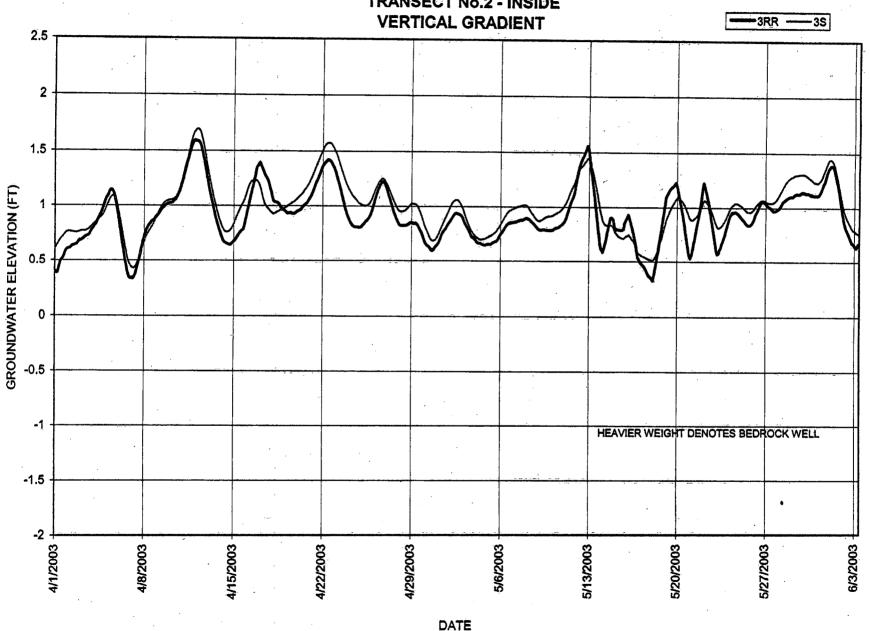
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #8 **TRANSECT No.4 SAND & GRAVEL UNITS** -85 4.5 HEAVIER WEIGHT DENOTES WELL OUTSIDE THE SLURRY WALL. 3.5 GROUNDWATER ELEVATION (FT) 3 0.5 0 5/6/2003 6/3/2003 4/1/2003 4/29/2003 5/20/2003 4/8/2003 4/15/2003 5/13/2003 5/27/2003 4/22/2003

DATE

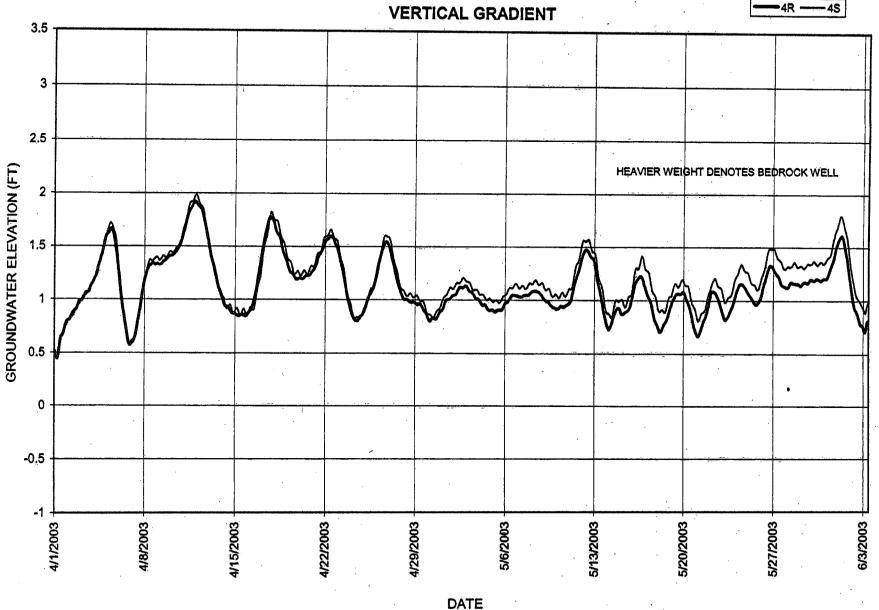
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #9 TRANSECT No.4 (OSA)



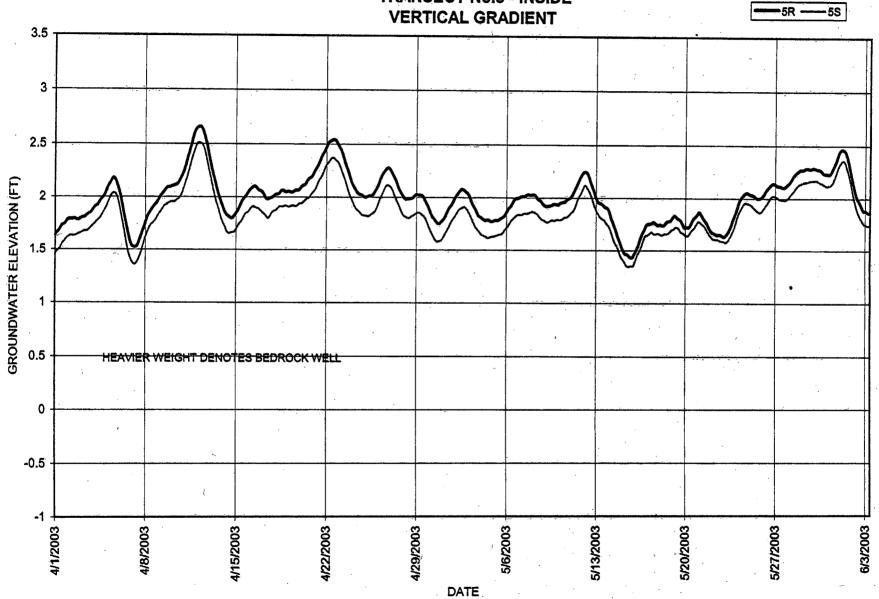
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #10 TRANSECT No.2 - INSIDE



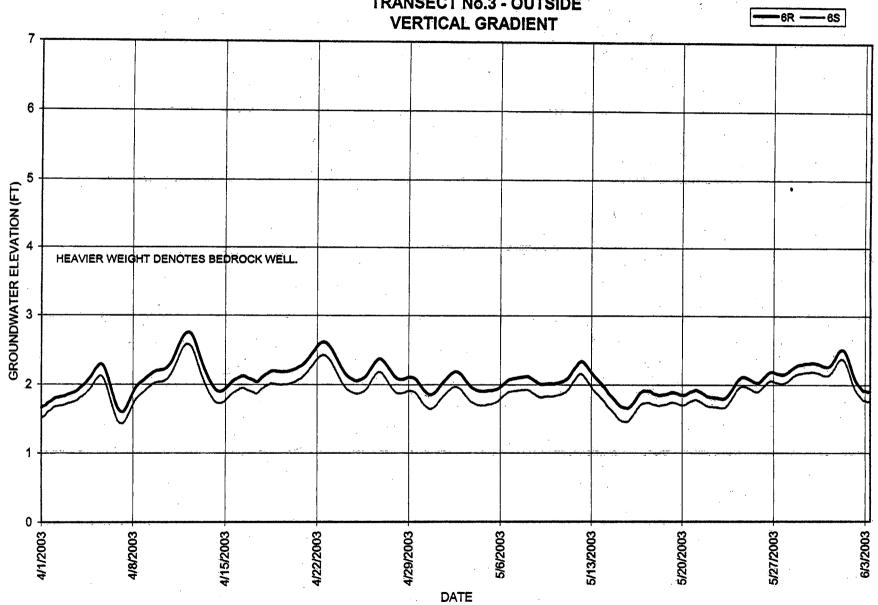
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #11 TRANSECT No.2 - OUTSIDE



KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #12 TRANSECT No.3 - INSIDE VERTICAL GRADIENT



KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #13 TRANSECT No.3 - OUTSIDE



KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #14 TRANSECT No.4- INSIDE 7R -**VERTICAL GRADIENT** 3.5 3 GROUNDWATER ELEVATION (FT) HEAVIER WEIGHT DENOTES BEDROCK WELL 0.5 0 -6/3/2003 5/6/2003 4/8/2003 4/1/2003 5/13/2003 4/15/2003 4/22/2003 4/29/2003 5/20/2003 5/27/2003

DATE

KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #15 **TRANSECT No.4- OUTSIDE** BRR . **VERTICAL GRADIENT** 4.5 3.5 GROUNDWATER ELEVETION (FT) HEAVIER WEIGHT DENOTES BEDROCK WELL 1 0.5 6/3/2003 4/1/2003 4/8/2003 5/6/2003 5/27/2003 4/22/2003 4/15/2003 4/29/2003 5/20/2003 5/13/2003

DATE

the Figroup

IT Corporation

Crossroads Corporate Center
One International Boulevard, Suite 700
Mahwah, NJ 07495-0086
Tel. 201.512.5700
Fax. 201.512.5786

A Member of The IT Group

June 27, 2001 Project 796201

Carl Januszkiewicz
Waste Management, Inc
Kin-Buc Landfill Treatment Plant
383 Meadow Road
Bdison, NJ 08817

Re: Evaluation of Head Levels at Transect 1

Dear Mr. Januszkiewicz:

We have completed an evaluation of the hydraulic characteristics at Transect 1 with specific focus on the lack of intragradient conditions associated with the high water levels in W-IG (inside of the slurry wall) relative to those levels in W-2G (outside of the wall).

While intragradient conditions were evident at the outset of the hydraulic monitoring program in April 1996, these conditions have generally not been maintained. Specifically, based on a review of historical hydrographs, intragradient conditions were evident initially from approximately April to July 1996, and April to June 1997. Thereafter, to more recent events, intragradient conditions have been observed intermittently and for shorter periods of time.

Attachment 1 presents a hydrograph at Transect 1 encompassing the period from September 1998 to December 2000. As seen on the hydrograph, there were periods of time when intragradient conditions were not being maintained.

As opposed to the other "G" series monitoring wells that are located in refuse, wells 1G and 2G at Transect 1 are actually located in a silt and clay deposit. Attachment 2 contains the boring logs for these 2 installations. In-situ hydraulic conductivity testing performed at Transect 1 indicated permeabilities of 10^{-7} cm/sec and 10^{-5} cm/sec in W-1G and W-2G, respectively. Accordingly, a source of recharge to the overburden soils in the area of W-1G would not readily drain away, and therefore, higher heads could result.

Well 1G sampling events (November 1998, October 1999, October 2000) can be seen on the hydrograph as sharp vertical drops in groundwater levels. Due to the low permeability of the surrounding materials, the groundwater levels required several months to recover. Since the final cover extends 10 feet past the slurry wall, the source of the groundwater that is recharging W-1G is unknown at present.

The hydraulic gradient between W-1G and W-1R is vertically downward which rules out the bedrock as being a source of groundwater recharge. Based on a recent visual inspection of the area around Transect 1, the cap appears to be good condition and there were no signs that the cap integrity has been compromised.

Figure 1 depicts the conceptual model of the hydraulic interrelationship across Transect 1 showing water level measurements that depict the lack of intragradient conditions across the

Carl Januszkiewicz June 27, 2001 Page 2

Project 796201

slurry wall. The head levels in W-2G (outside the slurry wall) are generally at elevation 12 to 13 feet msl with periodic and short term increases to about 15 feet msl. The water level in the well sometimes falls below the level of the transducer. This is characterized by a flat straight line on the hydrographs as shown on Attachment 1. Head levels in W-1G (inside the slurry wall), on the other hand, are often greater with elevations as high as 15 to 16 feet msl being recorded.

It is evident from a review of Figure 1 that the drop in topography outside of the slurry wall toward Mill Brook, coupled with the higher permeability of W-2G relative to W-1G, would promote a more rapid decrease of head levels in the latter. This suggests that intragradient conditions may not be consistently attainable at this transect in any event. notwithstanding however, and as depicted on Figure 1, it is important to note that the leachate collection system represents a hydraulic sink within the containment system. As such, groundwater in the vicinity of W-1G would drain toward the sink mitigating concerns of

The leachate collection line runs parallel to the slurry wall and at its closest point is only about 20 feet away from Transect 1. Several cleanouts are located along the collection line with the closest, Cleanout 16, only about 65 feet from Transect 1. Leachate level measurements obtained from the cleanouts during December 2000 and June 2001 indicate a leachate level of 10 to 11 feet msl along the collection line as shown in Table 1. The leachate levels observed suggest that the leachate collection system is presently operating effectively.

Recommendations

Based on the above, it is recommended that during subsequent monitoring events at the site, measurements of leachate levels in Cleanouts 14 through 16 be recorded to verify that the leachate collection system is operating effectively. If liquid levels in the cleanouts increase above 12 to 13 feet msl, then maintenance of the collection line is recommended. Subsequent reports to EPA should include a discussion of the leachate collection system and its role as serving as a hydraulic sink within the containment system.

We trust you find this information useful. If you have any questions, please do not hesitate to

Sincerely,

IT Corporation

Steven Goldberg, Ph.D, C

Senior Hydrogeologist

Thomas M. Connors, P.E. Project Manager

Attachments

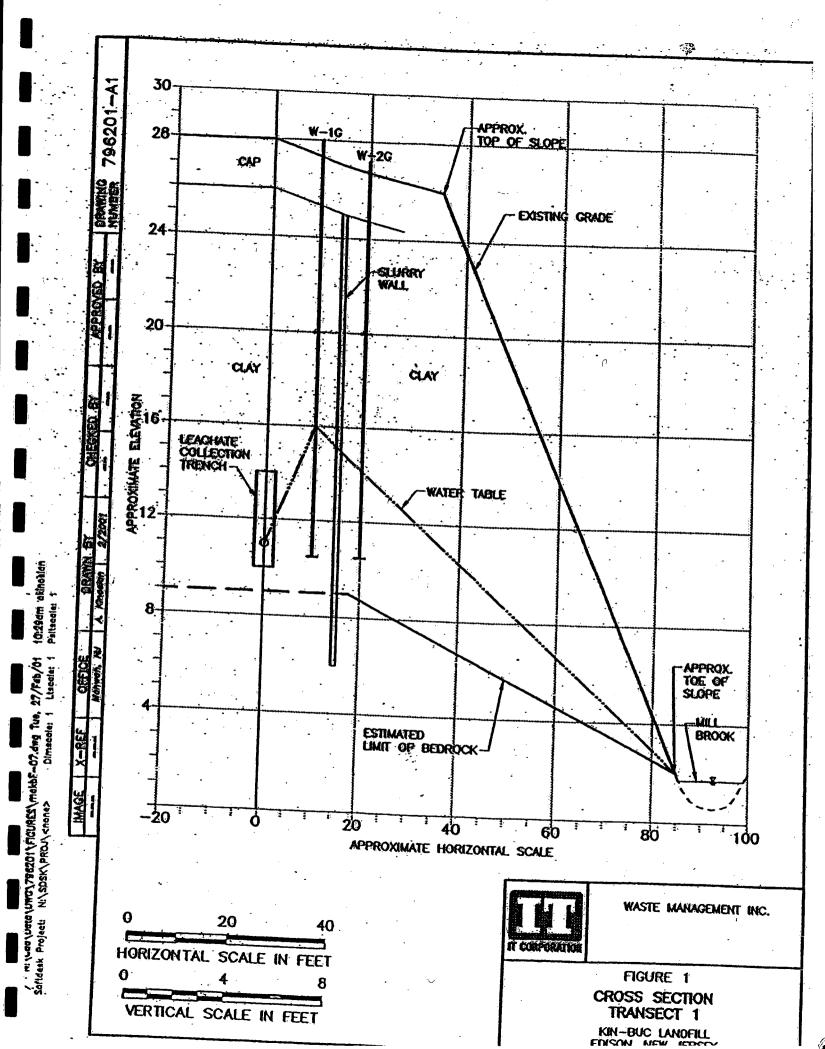
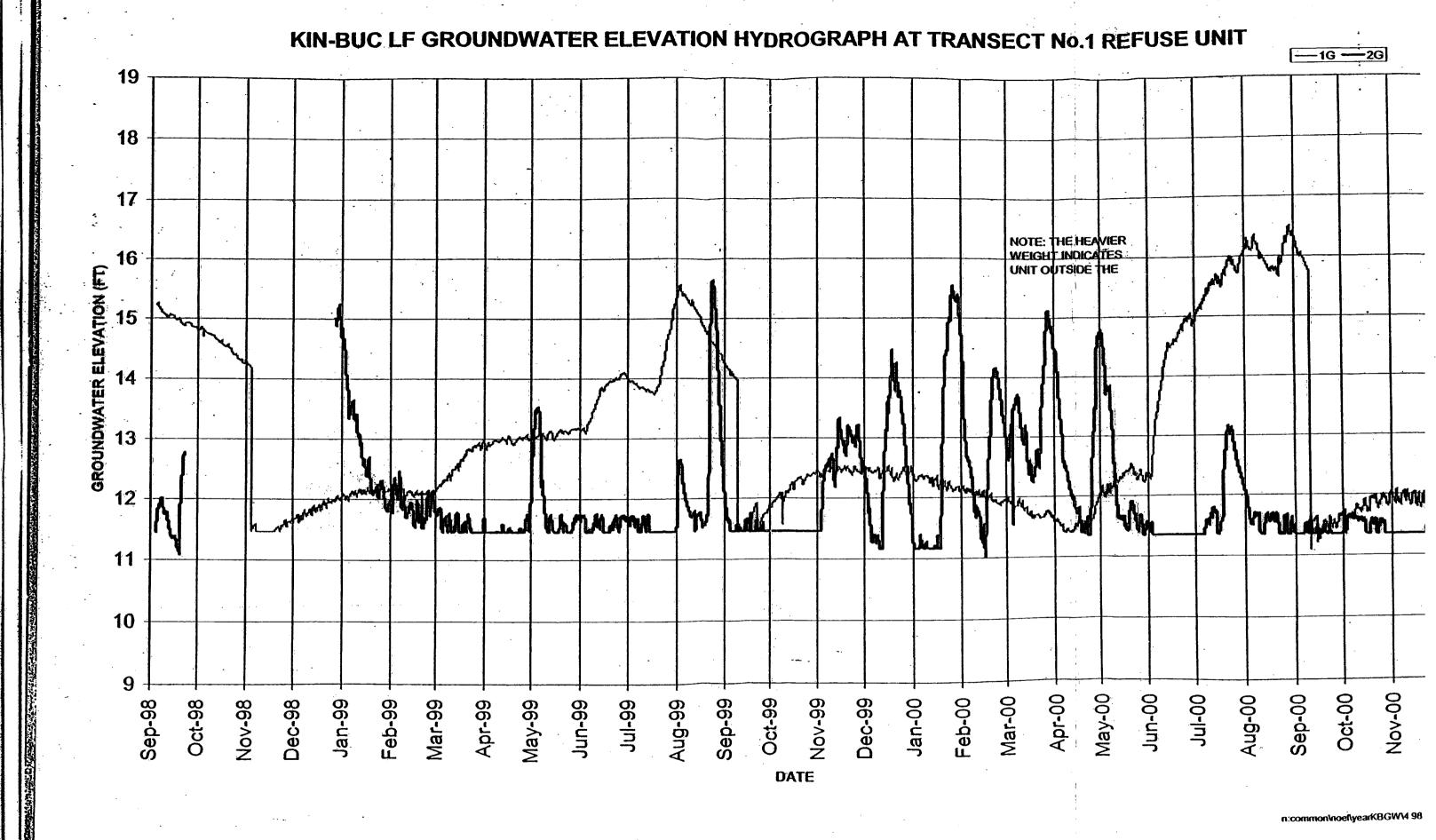


Table 1 Kin-Buc Landfill Leachate Cleanout Monitoring 2001

| Cleanout location Elevation @ Sea Level | 14N | | | 4E | | 15N | | 6E | | | | |
|--|---|------------------------------|--|-----------|-------------|--------------|------------------|-----------|-------------------|----------------------|-------------------------|-------|
| TOTAL CONTRACTOR | | 2.87 | 2 | 2.7.7 | | 6.51 | | | | 6N | | 16E |
| | depth to | | depth to | | depth to | V V | - Z | 3.51 | | 1.36 | . 3 | 1.32 |
| Elevation Average | water | elevation 10.80 | | elevation | water | elevation | depth to water | elevation | depth to water | elevation | depth to | |
| DATE | HARRING THE PARTY OF THE PARTY | Process in the second second | D CAMPASARA AND AND AND AND AND AND AND AND AND AN | 10.74 | | 10.66 | | 10.67 | | | | 11.11 |
| | | | | | | 排除推销额 | | | 1200000000000 | Beer Bronner Bronner | Grade viction represent | 11,11 |
| 6/7/01 | 44.00 | 4 | | | | | Anna Caran Caran | | MERCEN COM | | | |
| 5/16/01 | 11.98 | 10.89 | 12.02 | 10.75 | 15.86 | 10.65 | 15.87 | 10.64 | dry | | | |
| 4/26/01 | 12.25 | 10.62 | 12.23 | 10.54 | 15,96 | 10.55 | 15.96 | 10.55 | | na . | dry | na |
| 3/21/01 | 12.36 | 10.51 | 12.35 | 10.42 | 15.99 | 10.52 | 16.01 | 10.50 | dry | na | dry | na |
| 2/26/01 | 11.80 | 11.07 | 11.75 | 11.02 | 15.62 | 10.89 | 15.59 | 10.92 | dry | na | dry | na |
| 1/29/01 | 12.03 | 10.84 | 11.94 | 10.83 | 15.95 | 10.56 | 15:92 | 10.59 | dry | na | dry | na |
| | 12.08 | 10.79 | 11.98 | 10.79 | 15.85 | 10.66 | 15.83 | 10.68 | diy | na | dry | na |
| 12/27/01 | 12.02 | 10.85 | 11.94 | 10.83 | 15.72 | 10.79 | 15.68 | | dry | na i | 20.41 | 10.91 |
| | | | | | | | 10.00 | 10.83 | dry | na | 20.01 | 11.31 |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | 1 |
| | | | | | | | -, | | · | | | |
| | | | | | | | | | | | | |
| | | | | | | - | | | | | | |
| | | | | - | | | | | | | | |
| | | | - | - | | | | | | | | |
| | | | | | | | | | | | | |
| 10 | | | - | | | | | | | | | |
| | | - | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | - | | | | <u> </u> | | | | | | | |
| | | | | · | | | | | 1. | | | |

ATTACHMENT 1



ATTACHMENT 2

MONITORING WELL RECORD

| OWNER IDENTIFICATION - Own Address | 200 CENTENTAL | • | | | 25 : 45 : 428 |
|---|----------------------------|-----------------------|---|----------------|-------------------------------|
| City | FISCATAVAY | | State | NJ | 7-0 |
| WELL LOCATION - If not the same | e as owner please give add | Isasa | | | Zip Code |
| Address Address | Municipality | FOOT | Owners Well V | lo, <u>2</u> (| 3 |
| Address 383 Headows Ro | oad, Edison, NJ | THE WAY | · ···································· | Lot No. | Block No |
| TYPE OF WELL (as per Wall Permi Regulatory Program Requiring Well | (Categories) | | | - | |
| Regulatory Program Requiring Well CONSULTING FIRM/FIELD SUPER | CTOTA | | - Date | well comple | ted 2 , 15 , 95 |
| CONSULTING FIRMFIELD SUPER | NVISOR (if applicable) | | C456 | 1.0.# | NJD049860836 |
| THE TAXABLE FOR | | | | | Tele. # |
| Total depth drilled 15.6 ft. | • • • • | Depth to Top (ft.) | | Diameter | |
| Well finished to15ft. | | (From 1 | Battom (ft. | (inches) | Type and Material |
| Porehole diameter: | Inner Casing | +4 | | 2 | Sch 40 PVC |
| Top 8 in. | (Not Protective Casing) | | | - | 40 EAC |
| ell was finished: Above grade | Same | | | | |
| above grade | (Note sigt size) | | 15. | 2 | Sch 40 PVC .010 |
| inished above grade, casing | | | | | |
| and (allow up) above land | Gravel Pack | 3 | 15.6 | 8 | #00 Ricci |
| face 4 ft. | Annular Seal/Grout | 0 | 3 | | |
| s steel protective casing installed? | Method of Grouting | tremi | 2 | | Bentonite slurry |
| lic water level after drilling | | | | · · · | |
| U MVO Was managed | | GEO | LOGIC LOG | (Copies | of other geologic logs and/or |
| was developed for N/A hour | s at N/A gpm | | 0 | goping | ical logs should be attached. |
| N/A | | 1 | 0 - 15.6 | .1 | ed dry stiff clay, |
| permanent pumping equipment inst | alled? Yes X No | - ∤ | | | ome silt |
| gpm | | . | | | |
| | | : 1. | | - | |
| n Fluid | | 1 | 5 | | |
| of Driller Chad Chism | RigB-61 | _ | | | |
| and Safety Plan submitted? | Yes X No | _ | | | . (|
| Protection used on site (circle one) | None D C/D | | | | · |
| | · - | | | • | • |
| Drilling Company HAR | DIN-HUBER, INC. | .1 | | | - |
| that I have drilled the above-ref | erenced well in accordance | | | | |
| HOC and comments | according | ice with all | well permit re | equirement | s and all applicable |
| vies and regulations. | • | - | | | |
| that I have drilled the above-refules and regulations. Driller's Signature | | · Dj· | | | |

COPIES:

White - DEP

Canary - Driller

Pink - Owner

Goldenrod - Health Dept.

MONITORING WELL RECORD

| | | | Vell Permit No. Viles Sheet Cod | | . 465 <i>0</i> 5 25 : 45 · 428 |
|--|---|-----------------------------------|--|--------------------------|---|
| OWNER IDENTIFICATION - Owner Address | KIN-BIC INC | · · · · . | | | |
| Address | PISCATAWAY | AVE. | State | N | |
| WELL LOCATION - If not the same | as owner please mine sale | 2000 | 449.000 | | Zip Code |
| Address 383 Headows Ro | Municipality EDE | SON THE | owner's Well No | - <u>IG</u> _ Lot No. | _483 Block No |
| TYPE OF WELL (as per Well Permit Flegulatory Program Requiring Well CONSTITUTE FROM SEC. | | | | well comple | ted 2 / 15 / 95 |
| CONSULTING FIRMFIELD SUPER | VISOR (if applicable) | | | | NJD249962836 |
| WELL CONSTRUCTION | | - | | | Tele.# |
| Total depth drilled 15.6 tt. Well linished to 15 tt. | | Depth to Top (ft.) (From la | Depth to Bottom (ft.) ind surface) | Diameter (inches) | |
| Borehole diameter: | Inner Casing | +4 | 5 | 2 | Sch 40 PVC |
| Top 8 in. Bottom 8 in. | Outer Casing (Not Protective Casing) | | | | |
| Well was finished: X above grade | (Note slot size) | 5 | 15 | 2 | Sch 40 PVC .020 |
| L flush mounted | | <u> </u> | | ` | 10 10 1020 |
| linished above grade, casing eight (stick up) above land | Gravel Pack | 3 | 15.6 | 8 | #2 Ricci |
| unace,ft. | Annular Seal/Grout | 0 | 5 | 8 | Bentonite slurry |
| vas steel protective casing installed? Yes TX No | Method of Grouting | tremi | 2 | | |
| ater level was measured using | <u>. </u> | GEO | LOGIC LOG | (Copies geophy: | of other geologic logs and/cical logs should be attache |
| ell was developed for N/A hour | N/A | | | | • |
| s permanent pumping equipment ins | plas Dy D. | _ | 0 - 15.6 | | red gray dry stiff clay, some silt |
| mp capacity N/A gpm | Tes LY No | | • | | |
| mp type:N/A | | | | | • |
| ing Fluid Type o | — 1 Rig B-61 | | | | |
| ne of Driller Chad Chism | | | | | |
| Ith and Salety Plan submitted? If of Protection used on site (circle one License No. 0013753-001375 | Yes X No None D C(B) A | | | | |
| | RDIN-HUBER, INC. | | - | | |
| lify that I have drilled the above-re rules and regulations. | | ance with a | ll well permit : | requiremen | nts and all applicable |
| Driller's Signatur | | Bui | . | Date | |



One International Boulevard, Suite 700 Mahwah, NJ 07495-0086 201.512.5700 Fax 201.512.5786

July 30, 2003 Project 791186

Mr. Carl Januszkiewicz
Waste Management, Inc.
Kin-Buc Landfill Treatment Plant
383 Meadow Road
Edison, NJ 08817

Re: Hydraulic Monitoring for June 2003

Dear Mr. Januszkiewicz:

A site visit was completed on June 30, 2003 to download the June water level recorder data and obtain manual water level measurements. The following is an update of the hydraulic monitoring for the month of June 2003 at the Kin-Buc Landfill. This information is to be included in the quarterly report, which is to be submitted to the EPA by mid-August 2003.

The minimum, maximum, and average water elevations recorded at each well are included in Table 1. Table 2 shows the troll water elevations versus the manual water elevations. The continuous water level elevation data when compared with manual readings indicated that the miniTrolls are functioning properly and are recording accurate data. The SP4000 Troll is still recording continuous hydraulic data in Well 15G.

Also, the data supplied for well SG-3 showed the same water level for the entire period. These water levels should be fluctuating. The automated water level recording device in this well needs to be checked so that accurate readings can be obtained in the future.

Hydrographs have been prepared for each of the transect locations and are enclosed for your reference as Attachment No. 1. The water levels in wells on the outside of the slurry wall vary over the course of the day due to the tidal influence at the site. For clarity, Hydrograph Nos. 6 through 15 show the average water level in the well over a 24-hour period (12 hours before, and 12 hours after).

Refuse

As defined in the Record of Decision (ROD) for OU-1, the performance objective for the refuse unit calls for the pumping of leachate to establish inward gradients across the slurry wall with the additional benefit of reducing downward flow into the underlying sand and gravel unit. Based on the hydrographs the following is presented.

Transect 1-Refuse (1G/2G)/Hydrograph No. 1 - Intragradient conditions were observed during the entire month of June. The average monthly water elevation for June at Well 1G (inside) and Well 2G (outside) was 11.28 and 12.71 feet msl, respectively. Water level elevation measurements taken from Leachate Collection Cleanouts Nos. 14 through 16 are included in Table 3, and indicate that the leachate collection system is functioning properly. The fact that the leachate collection system is functioning properly suggests significant capture of leachate. The evaluation of the hydraulic conditions in the refuse at Transect 1 is provided in Attachment No.2.

Transect 2-Refuse (3G/4G)/Hydrograph No. 2 — Intragradient conditions were maintained throughout the month of June. The average monthly water elevation for the month at Well 3G (inside) and Well 4G (outside) was 7.41 and 11.57 feet msl, respectively

Transect 3-Refuse (5G/6G)/Hydrograph No. 3 — Intragradient conditions were maintained throughout the month of June. The average monthly water elevation for the month of June at Well 5G (inside) and Well 6G (outside) was 9.85 and 13.77 feet msl, respectively.

Transect 4-Refuse Oil Seeps Area (13G/15G)/Hydrograph No. 4 — Intragradient conditions were maintained throughout the month of June. The average monthly water elevation for the month of June at Well 15G (inside) and Well 13G (outside) was 1.54 and 6.79 feet msl, respectively.

Transect 5-Refuse (9G/10G)/Hydrograph No. 5 — Intragradient conditions were maintained throughout the month of June. The average monthly water elevation for the month of June at Well 9G (inside) and Well 10G (outside) was 7.74 and 8.80 feet msl, respectively.

Sand and Gravel/Bedrock

For the sand and gravel unit, the performance objectives call for pumping of sand and gravel groundwater to prevent flow toward the slurry wall and to impose upward hydraulic gradients from the bedrock to the sand and gravel. An additional benefit would be the establishment of inward gradients across the slurry wall within the sand and gravel unit. The following is a description of the flow characteristics based on visual observation of the hydrographs.

Horizontal Flow

Transect 2-Sand and Gravel (3S/4S)/Hydrograph No. 6 – Although intragradient conditions were not consistently maintained throughout the enitre month of June, intragradient conditions were evident most of the month. Containment is being

maintained by the pumping wells (see discussion in Conclusion). The average monthly water elevations for the month of June at Well 3S (inside) and Well 4S (outside) was 1.11 and 1.36 feet msl, respectively.

Transect 3-Sand and Gravel (5S/6S)/Hydrograph No. 7 — Slight intragradient conditions were maintained throughout the month of June. The average monthly water elevation for Well 5S (inside) and Well 6S (outside) was 1.93 and 2.01 feet msl, respectively.

Transect 4-Sand and Gravel (7S/8S)/Hydrograph No. 8- Intragradient conditions were maintained throughout the month of June. The average monthly water elevation for the month of June at Well 7S (inside) and Well 8S (outside) was 2.06 and 2.77 feet msl, respectively.

Transect 4 Sand and Gravel Oil Seeps Area (13S/15S)/Hydrograph No. 9 – Intragradient conditions were not evident during most of the month of June. The average monthly water elevation for the month of June at Well 15S (inside) and Well 13S (outside) was 2.77 and 2.54 feet msl, respectively. Water levels from Well 15G in the refuse unit are included on the hydrograph for comparison.

Vertical Flow-Inside Slurry Wall

Transect 2-Vertical Gradient (3S/3RR)-Inside/Hydrograph No.10 – Upward gradient conditions were not observed between the bedrock and overlying sand & gravel units inside the slurry wall for most of the month of June. The average monthly water elevation for the month of June at Well 3S (sand & gravel) and Well 3RR (bedrock) was 1.11 and 1.04 feet msl, respectively.

Transect 3-Vertical Gradient (5R/5S)-Inside/Hydrograph No. 12 – Upward gradient conditions were observed between the bedrock and overlying sand & gravel units inside the slurry wall for the month of June. The average monthly water elevation for the month of June at Well 5S (sand & gravel) and Well 5R (bedrock) was 1.93 and 2.07 feet msl, respectively.

Transect 4-Vertical Gradient (7R/7S)-Inside/Hydrograph No. 14 – Upward gradient conditions were observed between the bedrock and overlying sand & gravel units inside the slurry wall throughout the month of June. The average monthly water elevation for the month of June at Well 7S (sand & gravel) and Well 7R (bedrock) was 2.06 and 2.16 feet msl, respectively.

Vertical Flow-Outside Slurry Wall

Transect 2-Vertical Gradient (4S/4R)-Outside/Hydrograph No. 11 — Upward gradient conditions were not observed between the bedrock and overlying sand & gravel units outside the slurry wall for the month of June. The average monthly water elevation for the month of June at Well 4S (sand & gravel) and Well 4R (bedrock) was 1.36 and 1.17 feet msl, respectively.

Transect 3-Vertical Gradient (6R/6S)-Outside/Hydrograph No. 13 – Upward gradient conditions were observed between the bedrock and overlying sand & gravel units outside the slurry wall for the month of June. The average monthly water elevation for the month of June at Well 6S (sand & gravel) and Well 6R (bedrock) was 2.01 and 2.16 feet msl, respectively.

Transect 4-Vertical Gradient (8RR/8S)-Outside/Hydrograph No. 15 — Upward gradient conditions were not observed between the bedrock and overlying sand & gravel units outside the slurry wall throughout the month of June. The average monthly water elevation for the month of June at both Well 8S (sand & gravel) and Well 8RR (bedrock) was 2.77 and 2.73 feet msl, respectively. The difference in average monthly water elevations for June was 0.04 feet.

An initial review of the hydrographs indicates that certain performance objectives associated with the sand and gravel and bedrock units may not be met, specifically associated with the uniform achievement of upward gradients from the bedrock to the overlying sand and gravel inside the wall (e.g. Hydrograph 10), and inward gradients across the slurry wall within the sand and gravel (Hydrographs 6 and 9). However previous investigations performed at the site would indicate that complete control of OU-1 groundwater can be achieved notwithstanding indications of downward flow from the sand and gravel to the bedrock, or outward flow across the slurry wall within the sand and gravel unit. This is based on the findings of the considerable pumping influence of the sand and gravel pumping wells, in particular S&G#2, in achieving hydraulic control at the site (see Groundwater Pumping Well Performance Evaluation Report, July 2000).

The influence of the pumping well can be demonstrated by review of a plan view groundwater contour map of the sand and gravel (Figure 1) and equipotential profiles and vector diagrams (Figures 1, 2, 3, and 4) that have been prepared for a period of time when the vertical gradient between the sand and gravel and the bedrock was downward at Transect 2. For this evaluation, a snapshot of groundwater elevations from the monitoring wells and pumping wells was obtained for June 26, 2003. At this time, S&G#2 was pumping at a rate of about 12 gallons per minute (gpm), S&G#1 was pumping at a rate of 1.25 gpm, and S&G#4 was pumping at a rate of 3.7 gpm. This resulted in a total of approximately 17 gpm or about 24,473 gallons per day. There was a downward vertical

gradient observed the much of the time between the sand and gravel and the bedrock inside and outside the slurry wall at Transect No.2 in June as evidenced by higher heads in the sand and gravel wells relative to bedrock wells. For a brief period, there was also a higher head within the sand and gravel inside the slurry wall relative to the sand and gravel outside the slurry wall at Transect No. 2 in June.

Figures 1-4 incorporate the heads induced by pumping and show the considerable pumping influence of S&G#2. Specifically, groundwater flowing downward from the sand and gravel into the bedrock subsequently flows toward the pumping well. This occurs both inside and outside of the slurry wall. Also, groundwater within the sand and gravel unit flows toward the pumping well. The considerable pumping influence demonstrated at S&G#2, in conjunction with the fact that natural groundwater gradients in both the sand & gravel and bedrock flow predominantly towards the area of S&G#2, result in the complete capture of OU-1 groundwater at these pumping rates.

Groundwater and Leachate Collection

Based on data provided by U.S. Filter, the following volumes of groundwater and leachate were extracted from the sand & gravel wells and leachate collection system for the period from June 1 to June 30, 2003:

| S&G No. 1 Groundwater | S&G No. 2 Groundwater | S&G No. 3 Groundwater | S&G No. 4 Groundwater | Leachate |
|--------------------------|--------------------------|--------------------------|--------------------------|-------------|
| 2,160 gal. | 466,095 gal. | 38,124 gal. | 20,401 gal. | 54,990 gal. |
| 72 gpd | 15,537 gpd | 1,271 gpd | 680 gpd | 1,833 gpd |

For the month of June, a total of 526,780 gallons of groundwater was collected. The average daily groundwater extraction rate for all of the wells was 17,559 gpd. The extraction rate from S&G No. 1 was 72 gpd, 15,537 gpd for S&G No. 2, 1,271 gpd for S&G No. 3, and the extraction rate from S&G No. 4 was 680 gpd. The leachate extraction rate was 1,833 gpd for the month of June.

CONCLUSIONS

Intragradient conditions were maintained in the refuse unit at Transects 1, 2, 3, 4, and 5.

Intragradient conditions are not usually maintained by the monitoring wells at Transect 1 (although they were for the month of June), although each month levels in the leachate collection system indicate intragradient conditions are present at this location.

The transducer in S&G#3 needs to be checked. The data for June 26, 2003 showed no change in water level throughout the day, suggesting that the transducers are not functioning properly.

Hydraulic control was maintained within OU-1 based on the analysis of the significant influence of S&G#2 in acting as a hydraulic sink for sand and gravel and bedrock groundwater. Groundwater flow in the sand and gravel and bedrock is ultimately captured by the pumping wells (S&G#2 and S&G#1, 3, or 4) resulting in overall containment of groundwater in OU-1.

In view of the analysis presented herein, it is recommended that the combined groundwater pumping rates in the sand and gravel be maintained at 15,000 gpd with S&G#2 and S&G#3 pumping at 10,000 gpd and 5,000 gpd, respectively. These lower pumping rates will be evaluated to confirm continued hydraulic control of OU-1 groundwater.

We trust you find this information useful. If you have any questions, please do not hesitate to contact us.

EMCON/OWT, INC.

Tim Pagano, CPG

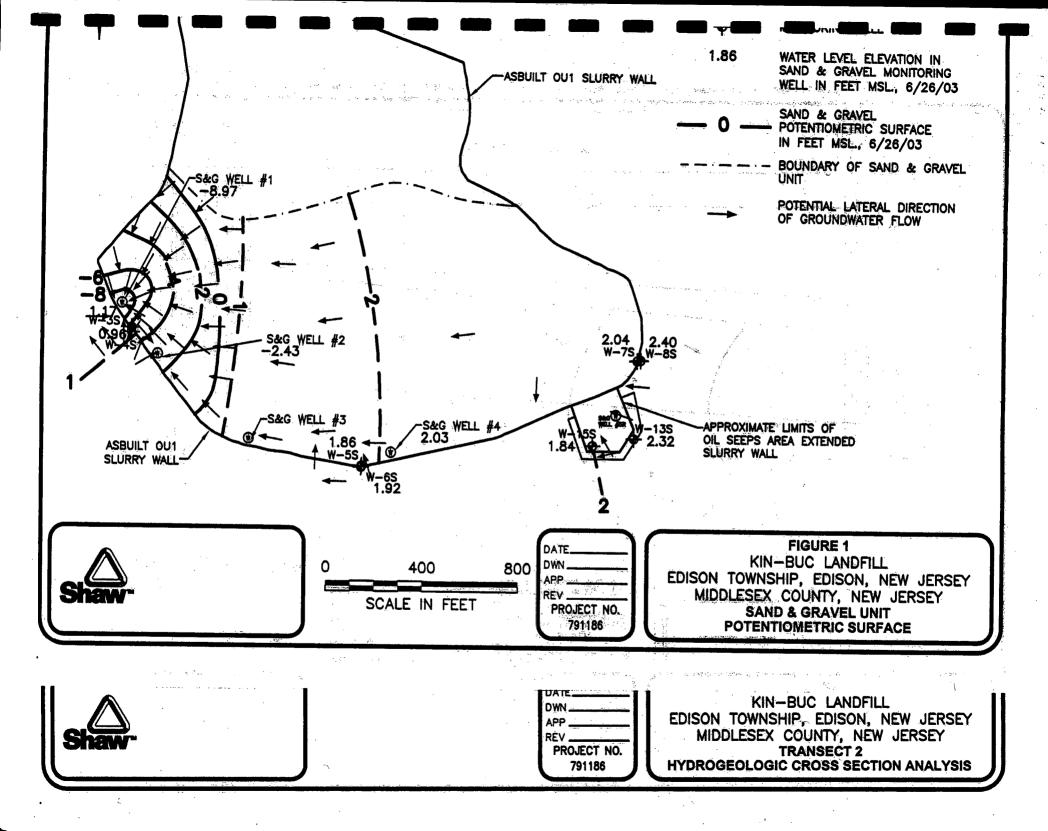
Senior Hydrogeologist

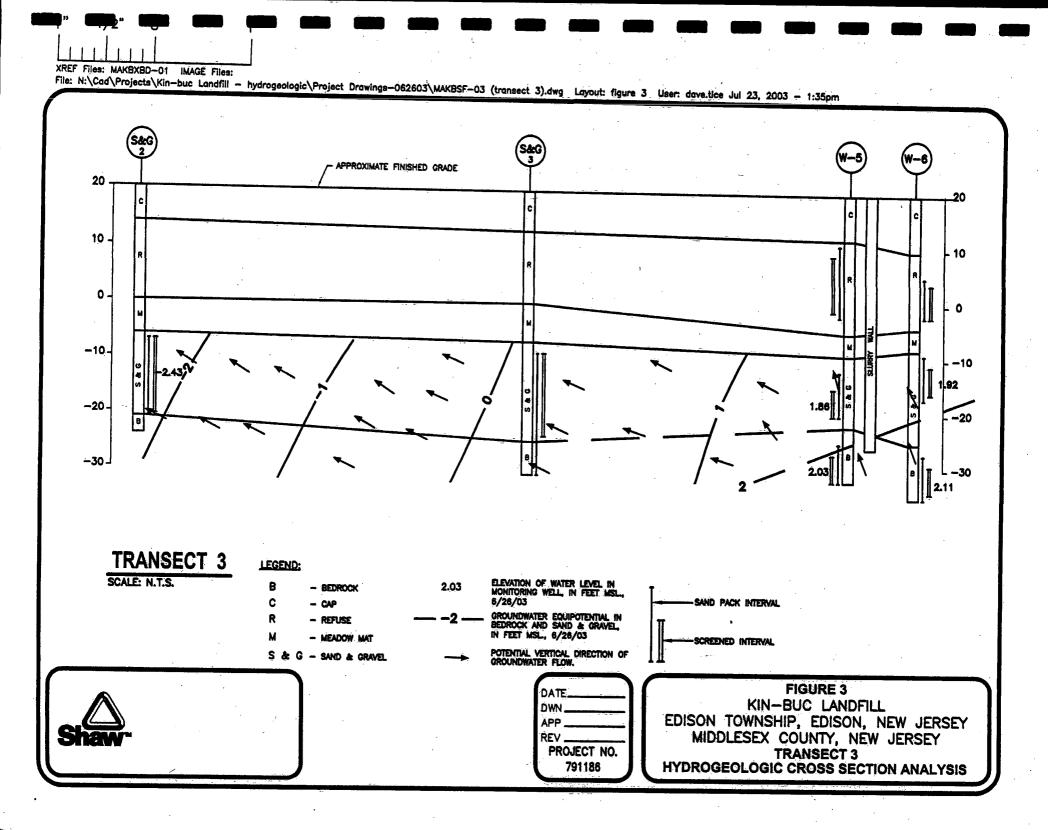
Laura Kisala

Environmental Scientist

Attachments

cc: Glenn Grieb, US Filter Steve Golberg, EMCON/OWT, Inc. Jeff Shanks, WM, Inc.





XREF Files: MAKBXBD-01 IMAGE Files: File: N:\Cad\Projects\Kin-buc Landfill - hydrogeologic\Project Drawings-082603\MAKBSF-04 (transect 4).dwg Layout: Layout1 User: dave.tice Jul 23, 2003 - 1:57pm 20 APPROXIMATE FINISHED GRADE 10 10 0 -10--10 -20 ~20 -30 TRANSECT 4 LEGEND: SCALE: N.T.S. ELEVATION OF WATER LEVEL IN MONITORING WELL, IN FEET MSL. 2.16 - BEDROCK 6/26/03 SAND PACK INTERVAL GROUNDWATER EQUIPOTENTIAL IN BEDROCK AND SAND & GRAVEL, IN FEET MSL., 8/28/03 MEADOW MAT SCREENED INTERVAL POTENTIAL VERTICAL DIRECTION OF GROUNDWATER FLOW. - SAND & CRAVEL FIGURE 4 KIN-BUC LANDFILL DWN. EDISON TOWNSHIP, EDISON, NEW JERSEY APP __ MIDDLESEX COUNTY, NEW JERSEY REV . PROJECT NO. **TRANSECT 4** HYDROGEOLOGIC CROSS SECTION ANALYSIS 791186

Table 1
KinBuc Landfill Operable Units 1 and 2
Continuous Hydraulic Monitoring Results
Second Quarter 2003
Minimum/Maximum/Average Water Elevations

| | | inside Slurry Wall | | | | • . | Outside Slurry Wall | • | |
|---------|----------------------|---------------------------------------|--|---------------------------------|----------|----------------------|--|---------------------------------------|---------------------------------|
| Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) | Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) |
| 11-10 | April | 11.25 | 11.27 | 11.25 | W-2G | April | 11.79 | 12.16 | 12.00 |
| | May | 11.23 | 11.25 | 11.24 | 1 | May | 11.47 | 11.93 | |
| | June | 11.12 | . 11.78 | 11.28 | | June | 11,60 | 13.34 | 11.68 |
| V-3G | 2nd Quarter | 11.12 | 11.78 | 11.26 | | 2nd Quarter | 11.47 | 13.34 | 12.71 |
| Y-3G | April | 7.02 | 7.65 | 7.36 | W-4G | April | 11,29 | 12.04 | 12.12 |
| | May | 6:84 | 7.58 | 7.32 | | May | 10.80 | 11.48 | 11.63 |
| | June | 7.17 | 7 <u>.</u> 61 | 7.41 | 1 1 | June | 11.10 | | 11.17 |
| | 2nd Quarter | 6.84 | 7.65 | 7.36 | 1 1 | 2nd Quarter | 10.80 | 11.84 12.04 | 11.57 |
| V-3S | April | 0.31 | 1.83 | 1.02 | W-4S | April | -0.19 | | 11.45 |
| | May | 0.43 | 1.53 | 0.97 | | May | 0.00 | 2.78 | 1.23 |
| | June | 0.63 | 1.58 | 1.11 | 1 1 | June | 0.26 | 2.46 | 1.17 |
| | 2nd Quarter | 0.31 | 1.83 | 1.03 | 1 1 | 2nd Quarter | -0.19 | 2.83 | 1.36 |
| V-5G | April | 9.50 | 10.14 | 9.84 | W-6G | April | 13.09 | 2.83 | 1.25 |
| 1 | May | 9.59 | 10.07 | 9.82 | | May | 12.76 | 14.60 | 13.75 |
| | June | 9.64 | 10.10 | 9.85 | 1 1 | June | 1 | 13.74 | 13.22 |
| | 2nd Quarter | 9.50 | 10.14 | 9.84 | | 2nd Quarter | 13.17 | 14.10 | 13.77 |
| V-5S | April | 1.21 | 2.68 | 1.89 | W-6S | April | 12.76 | 14.60 | 13,58 |
| | May | 1,13 | 2.50 | 1.81 | 111-03 | | 1.27 | 2.77 | 1.96 |
| 1 | June | 1.35 | 2.50 | 1.93 | 1 1 | May June | 1.21 | 2.57 | 1.86 |
| | 2nd Quarter | 1.13 | 2.68 | 1.88 | 1 1 | | 1.45 | 2.57 | 2.01 |
| V-7S | April | 1.42 | 2.69 | 2.00 | W-8S | 2nd Quarter | 1.21 | 2.77 | 1.94 |
| ľ | May | 1.49 | 2.52 | 1.92 | 144-02 | April | 2.10 | 5.27 | 2.70 |
| 1 | June | 1.66 | 2.48 | 2.06 | 1 | May | 2.12 | 5.02 | 2.64 |
| | 2nd Quarter | 1.42 | 2.69 | 1.99 | 1 1 | June | 2.21 | 4.92 | 2.77 |
| V-15S | April | 1.10 | 4.35 | 2.62 | W-13S | 2nd Quarter | 2.10 | 5,27 | 2.70 |
| | May | 1.38 | 4.05 | 2.64 | VV-135 | April | 1.90 | 3.73 | 2.45 |
| ł | June | 1.66 | 4.11 | 2. 04 2.77 | 1 1 | May | 1.89 | 3.52 | 2.39 |
| ļ | 2nd Quarter | 1,10 | 4.35 | | 1 1 | June | 2.06 | 3.72 | 2.54 |
| /-15G | April | 1.22 | 1,71 | 2.68 1.50 | 144.400 | 2nd Quarter | 1.89 | 3.73 | 2.46 |
| · 1 | May | 1.28 | 1.69 | | W-13G | April | 6.48 | 6.91 | 6.70 |
| 1 | June | 1.28 | 1.69 | 1.53 | 1 1 | May | 6.47 | 7.00 | 6.69 |
| | 2nd Quarter | 1.22 | 1.71 | 1,54 | 1 | June | 6.47 | 7.05 | 6.79 |
| -9G | April | 7.13 | 7.60 | 1.52 | | 2nd Quarter | 6.47 | 7.05 | 6.73 |
| - | May | 7.06 | | 7.35 | W-10G | April | 8.25 | 8.44 | 8.35 |
| | June | 7.51 | 7.65 | 7.31 | | May | 8.18 | 8.38 | 8.28 |
| 1 | 2nd Quarter | 7.06 | 7.96 | 7.74 | | June | 8.37 | 9.18 | 8.80 |
| -3RR | April | 0.03 | 7.96 | 7.46_ | | 2nd Quarter | 8.18 | 9.18 | 8.47 |
| -UNN | May | | 1.94 | 0.94 | W-4R | April | -0.27 | 2.85 | 1.20 |
| i | | -0.10 | 1.91 | 0.89 | | May | -0.25 | 2.36 | 1,04 |
| | June | 0.23 | 2.18 | 1.04 | ! | June | -0.05 | 2.81 | 1.17 |
| | 2nd Quarter | -0.10 | 2.18 | 0.96 | 1 | 2nd Quarter | -0.27 | 2.85 | 1.14 |

Table 1

KinBuc Landfill Operable Units 1 and 2 Continuous Hydraulic Monitoring Results Second Quarter 2003 Minimum/Maximum/Average Water Floration

| | Inside Sturry Wall | | | | | 100 Sec. 150 Sec. 100 | Outside Slurry Wall | | |
|-----------------|----------------------|--|--|---------------------------------|---------|-----------------------|---------------------------------------|---------------------------------------|----------------|
| Well ID V-5R | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water Elevation (ft) | Well ID | Monitoring Period | Minimum Recorded Water Elevation (ft) | Maximum Recorded Water Elevation (ft) | Average Water |
| 4-5K | April | 1.38 | 2.84 | 2.05 | W-6R | April | 1,47 | | Elevation (ft) |
| - 1 | May | 1.24 | 2.61 | 1.93 | | May | | 2.91 | 2.13 |
| | June | 1.47 | 2.62 | 2.07 | | | 1.47 | .2.66 | 2.03 |
| | 2nd Quarter | 1.24 | 2.84 | 2.01 | 1 | June | 1.64 | 2.69 | 2.16 |
| -7R | April | 1.51 | 2.77 | | - | 2nd Quarter | 1.47 | 2.91 | 2.11 |
| i | May | 1.59 | | 2.09 | W-8RR | April | 2.05 | 5.21 | 2.66 |
| ľ | June | 1.77 | 2.62 | 2.01 | 1 1 | May | 2.09 | 4.97 | 2.60 |
| i i | | | 2.58 | 2.16 | 1. [| June | 2.17 | 4.89 | |
| | 2nd Quarter | 1.51 | 2.77 | 2.09 | 1 . 1 | 2nd Quarter | 2.05 | 5.21 | 2.73 2.66 |

Table 2
KinBuc Landfill Operable Unit 1
June 2003
Troll Water Elevations vs. Manual Water Elevations

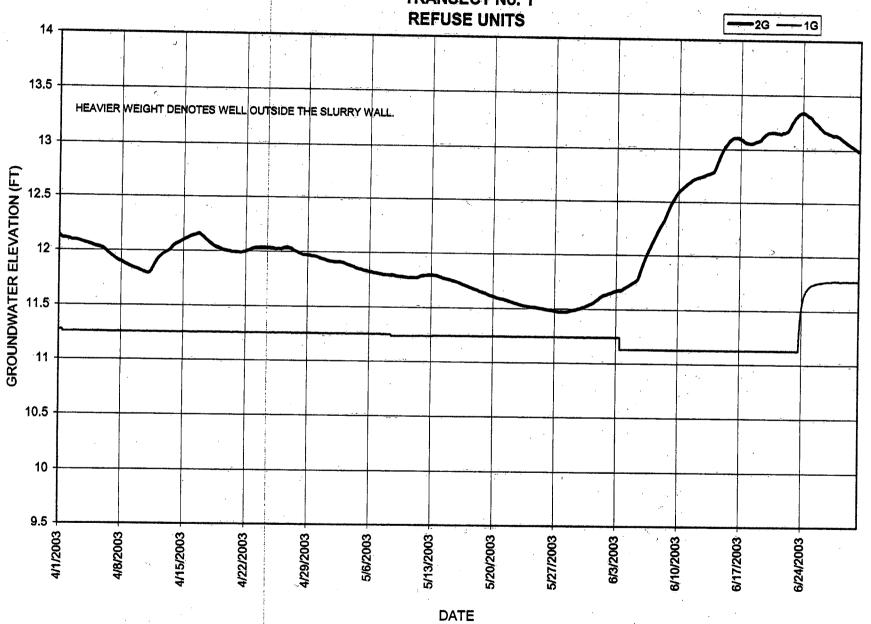
| OU 1 | | June 30, 2 | 2003 |
|---------|-------|------------|------------|
| Well ID | Troll | Manual | Difference |
| W-1G | 11.89 | 11.86 | 0.03 |
| W-2G | 12.92 | 12.91 | 0.01 |
| W-3G | 7.39 | 7.85 | 0.46 |
| W-3S | 0.70 | 0.73 | 0.03 |
| W-3RR | 0.66 | 0.63 | 0.03 |
| W-4G | 11.53 | 11.53 | 0.00 |
| W-4S | 1.18 | 1.18 | 0.00 |
| W-4R | 0.98 | 1.12 | 0.14 |
| W-5G | 9.84 | 9.90 | 0.06 |
| W-5S | 1.51 | 1.51 | 0.01 |
| W-5R | 1.39 | 1.43 | 0.04 |
| W-6G | 13.38 | 13.38 | 0.00 |
| W-6S | 1.65 | 1.68 | 0.03 |
| W-6R | 1.76 | 1.80 | 0.04 |
| W-7S | 1.67 | 1.72 | 0.05 |
| W-7R | 1.82 | 1.87 | 0.05 |
| W-8S | 2.36 | 2.37 | 0.01 |
| W-8RR | 2.35 | 2.31 | 0.04 |
| W-9G | 7.78 | 7.82 | 0.04 |
| W-10G | 9.12 | 9.12 | 0.00 |
| W-13G | 6.60 | 6.62 | 0.02 |
| W-13S | 2.14 | 2.15 | 0.01 |
| W-15G | 1.54 | 1.19 | 0.35 |
| W-15S | 2.20 | 2.24 | 0.04 |

Table 3
Kin-Buc Landfill
Leachate Cleanout Monitoring
2003

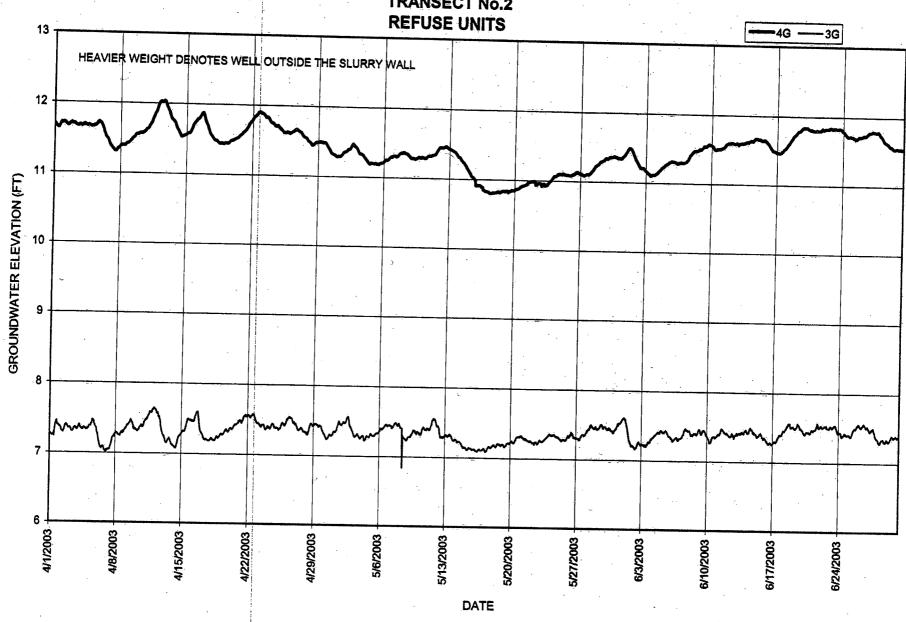
| Cleanout location | 1 | 4N | 1 | 4E | 1 | 5N | | 5E | 4 | 6N | · | 6E |
|-----------------------|----------|-----------|----------|-----------|-------|-----------|---------------|-----------|-------------|--|------------|----------|
| Elevation @ Sea Level | 22 | 2.87 | 22 | 2.77 | | 3.51 | | 3.51 | | 1.36 | | 1.32 |
| | depth to | | depth to | | | | depth to | | depth to | | depth to | |
| | water | elevation | _ | elevation | water | elevation | 1 7 | elevation | | elevation | | elevatio |
| Elevation Average | | 10.09 | | 10.06 | | 9.85 | - | 9.93 | water | na | Water | na |
| DATE | | | | | | | Mil. Letteriy | | | | | |
| 12/10/2001 | 12.5 | 10.37 | 12.42 | 10.35 | 16.31 | 10.20 | 16.33 | 10.18 | dry | SOFTIAL PRODUCTION OF THE PRODUCTION OF THE PROPERTY OF THE PR | | |
| 1/3/2002 | 12.37 | 10.50 | 12.31 | 10.46 | 16.21 | 10.30 | 16.22 | 10.19 | dry | na | dry | na |
| 2/13/2002 | 12.70 | 10.17 | 12.63 | 10.14 | 16.57 | 9.94 | 16.62 | 9.89 | dry | na na | dry dry | na |
| 3/27/2002 | 12.61 | 10.26 | 12.55 | 10.22 | 16.52 | 9.99 | 16.47 | 10.04 | dry | na | dry | na na |
| 4/19/2002 | 12.75 | 10.12 | 12.68 | 10.09 | 16.64 | 9.87 | 16.61 | 9.90 | dry | na | dry | |
| 5/3/2002 | 13.03 | 9.84 | 12.96 | 9.81 | 16.97 | 9.54 | 16.94 | 9.57 | dry | na | dry | na na |
| 6/5/2002 | 13.04 | 9.83 | 12.97 | 9.80 | 16.63 | 9.88 | 16.95 | 9.56 | dry | na | dry | na |
| 7/8/2002 | 12.86 | 10.01 | 12.79 | 9.98 | 16.77 | 9.74 | 16.72 | 9.79 | dry | na | dry | na |
| 8/2/2002 | 12.86 | 10.01 | 12.79 | 9.98 | 16.8 | 9.71 | 15.73 | 10.78 | dry | na | dry | na |
| 9/5/2002 | 12.86 | 10.01 | 12.78 | 9.99 | 16.77 | 9.74 | 16.75 | 9.76 | dry | na | dry | na |
| 9/26/2002 | 12.94 | 9.93 | 12.85 | 9.92 | 16.85 | 9.66 | 16.83 | 9.68 | dry | na | dry | na |
| 11/6/2002 | 12.64 | 10.23 | 12.58 | 10.19 | 16.59 | 9.92 | 16.48 | 10.03 | dry | na | dry | na |
| 12/6/2002 | 13.02 | 9.85 | 12.94 | 9.83 | 16.97 | 9.54 | 16.95 | 9.56 | dry | na | dry | na |
| 1/2/2003 | 13.07 | 9.80 | 13.00 | 9.77 | 17.03 | 9.48 | 17.01 | 9.50 | dry | na | dry | na |
| 2/12/2003 | 13.20 | 9.67 | 13.12 | 9.65 | 17.19 | 9.32 | 17.16 | 9.35 | dry | na | dry | na |
| 3/4/2003 | 13.21 | 9.66 | 13.15 | 9.62 | 17.22 | 9.29 | 17.20 | 9.31 | dry | na | dry | na |
| 4/1/2003 | 12.90 | 9.97 | 12.83 | 9.94 | 16.82 | 9.69 | 16.79 | 9.72 | dry | na | dry | na |
| 5/8/2003 | 13.05 | 9.82 | 12.97 | 9.80 | 17.01 | 9.50 | 16.96 | 9.55 | dry | na | dry | na |
| 6/3/2003 | 13.11 | 9.76 | 13.14 | 9.63 | 17.09 | 9.42 | 17.04 | 9.47 | dry | na | dry | na |
| 6/30/2003 | 12.92 | 9.95 | 12.85 | 9.92 | 16.83 | 9.68 | 16.79 | 9.72 | dry | na | dry | na |
| | | | | | | | 7507 | | | 1104 | , | 1164 |

ATTACHMENT 1.

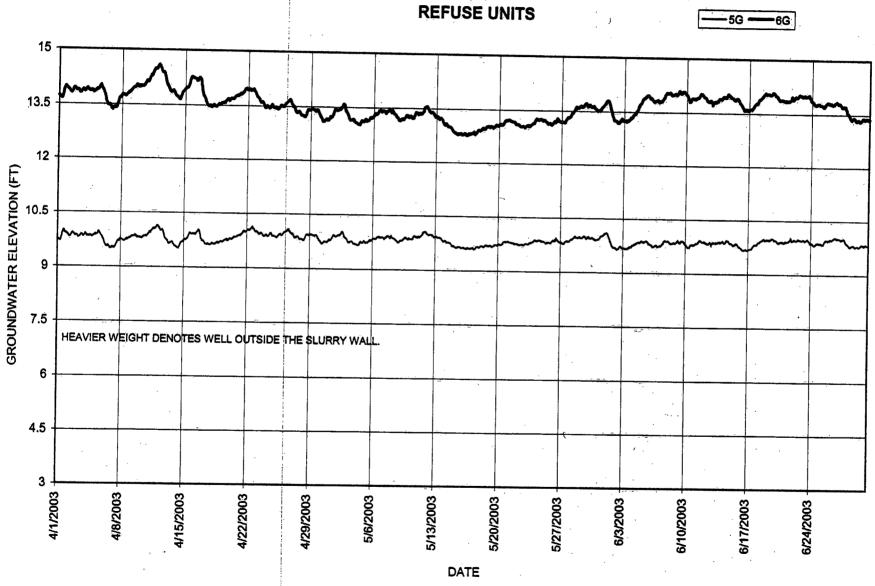
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #1 TRANSECT No. 1

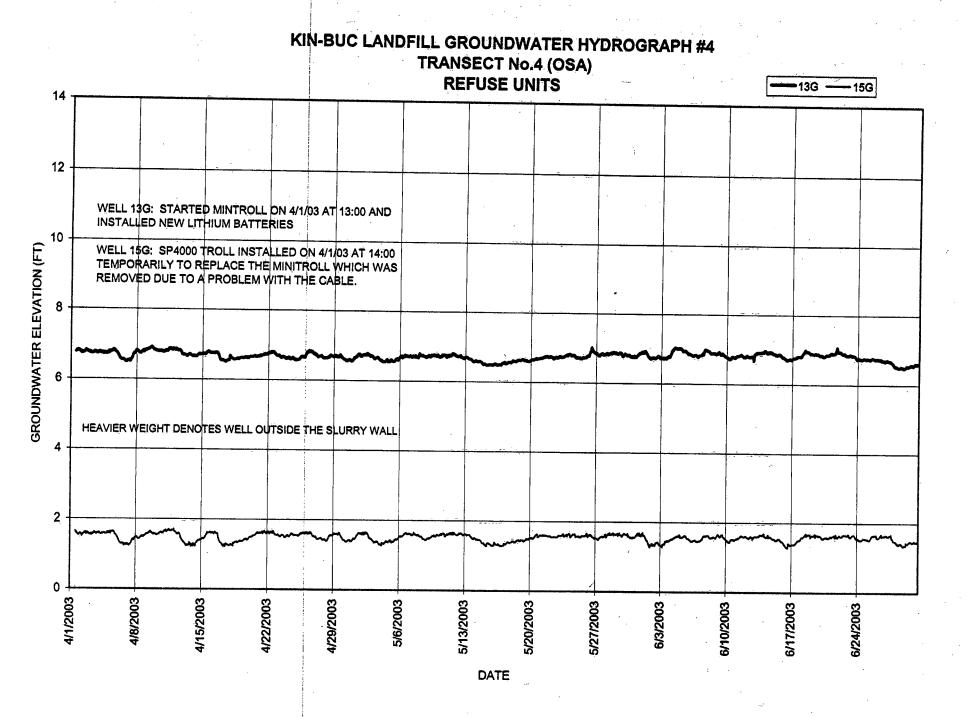


KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #2 TRANSECT No.2

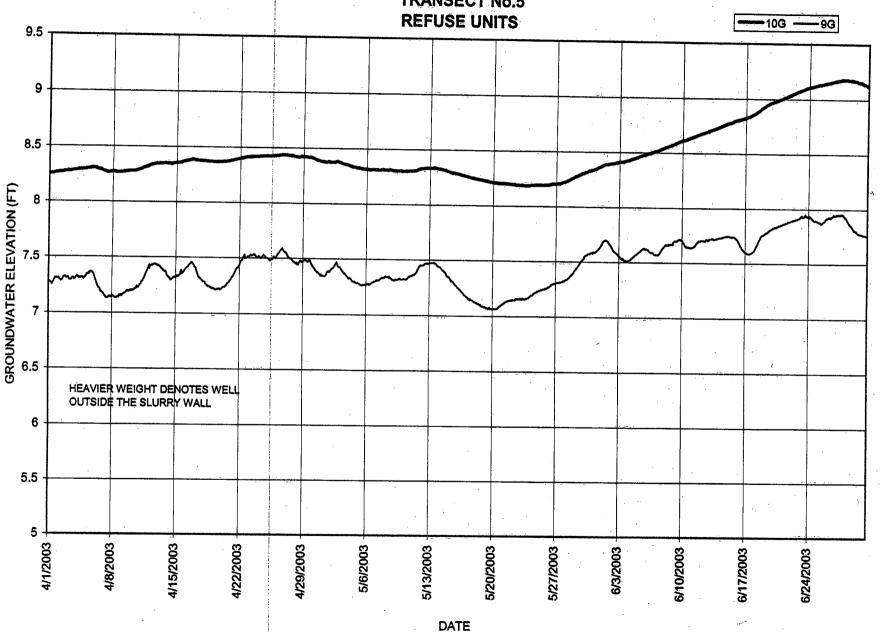


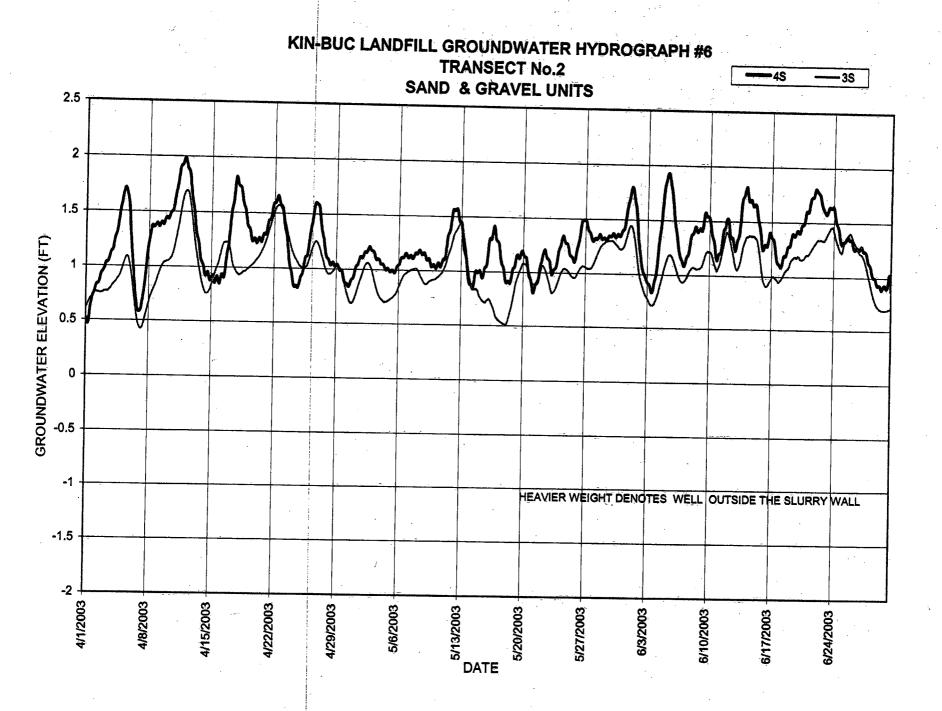
KIN BUC LANDFILL GROUNDWATER HYDROGRAPH # 3 TRANSECT No.3



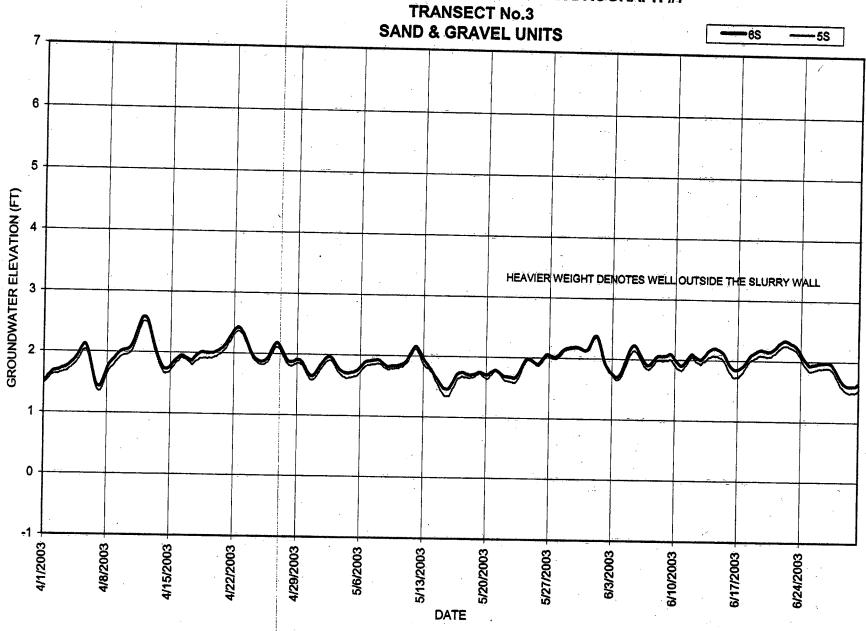


KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #5 TRANSECT No.5 REFUSE UNITS

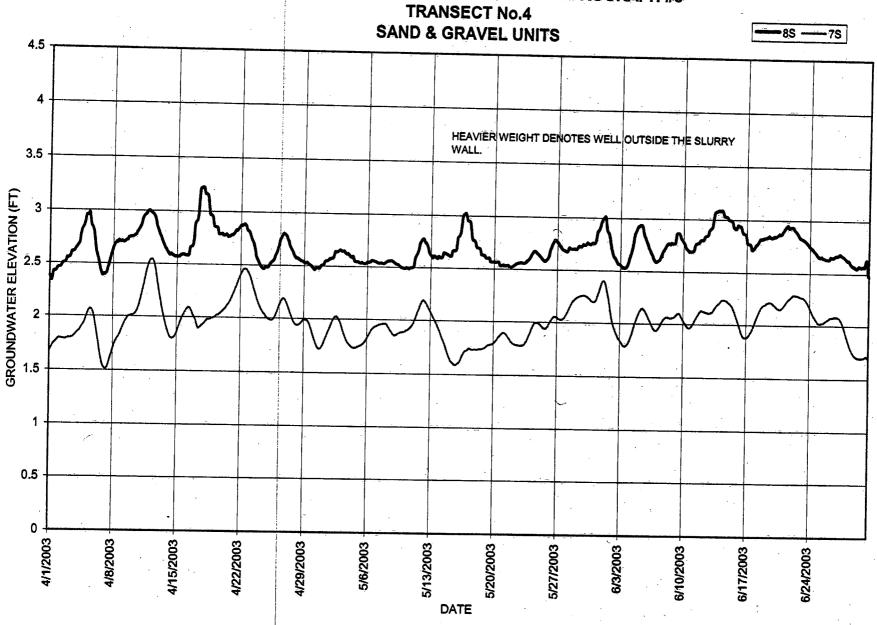




KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #7

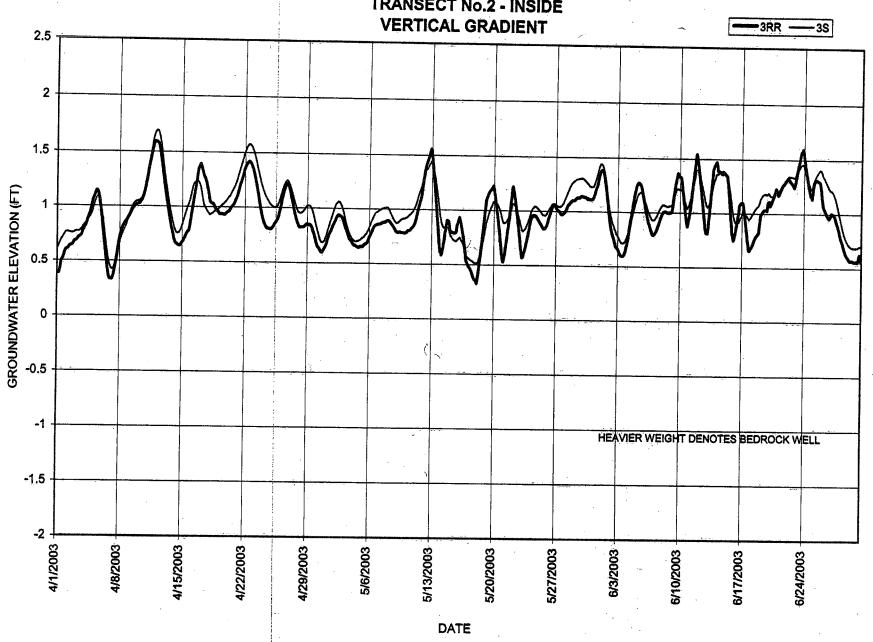


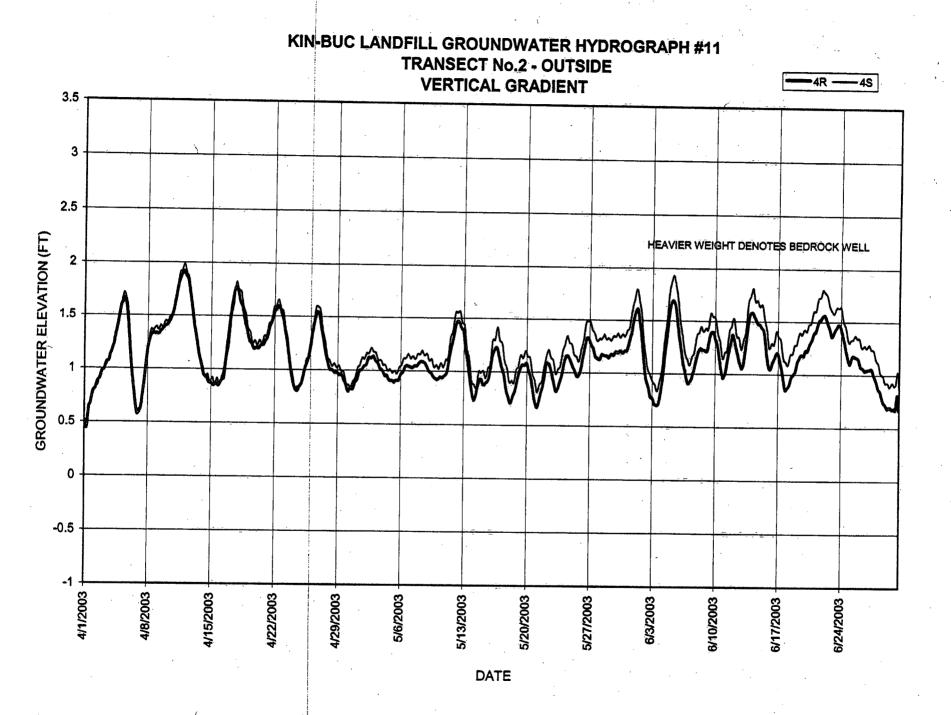
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #8



KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #9 TRANSECT No.4 (OSA) SAND & GRAVEL UNIT 10 13S --15S 15G 8 HEAVIER WEIGHT DENOTES WELL OUTSIDE THE SLURRY WALL. GROUNDWATER ELEVATION (FT) 4/1/2003 4/8/2003 4/15/2003 5/6/2003 4/22/2003 4/29/2003 5/13/2003 5/27/2003 6/3/2003 6/10/2003 6/17/2003 6/24/2003 DATE

KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #10 TRANSECT No.2 - INSIDE





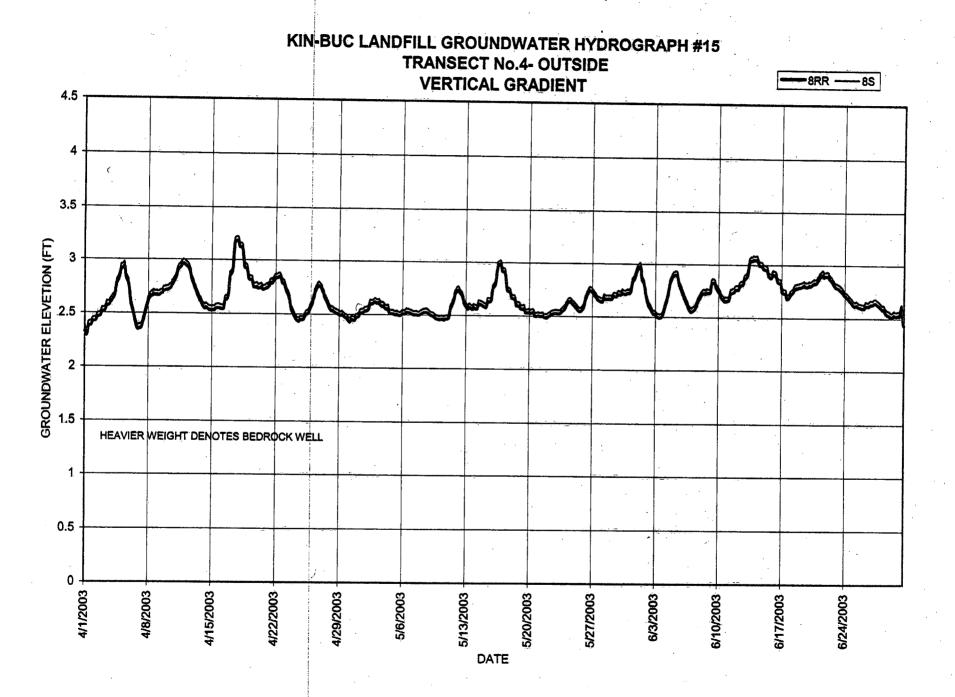
KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #12 TRANSECT No.3 - INSIDE **VERTICAL GRADIENT** SR · -58 3.5 3 2.5 GROUNDWATER ELEVATION (FT) HEAVIER WEIGHT DENOTES BEDROCK WELL 0 -0.5 4/1/2003 4/8/2003 4/15/2003 4/22/2003 5/6/2003 4/29/2003 5/13/2003 5/20/2003 5/27/2003 6/3/2003 6/10/2003 6/17/2003 6/24/2003

DATE

KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #13 TRANSECT No.3 - OUTSIDE **VERTICAL GRADIENT** -6R -65 6 GROUNDWATER ELEVATION (FT) HEAVIER WEIGHT DENOTES BEDROCK WELL 4/1/2003 4/8/2003 5/6/2003 4/15/2003 4/22/2003 4/29/2003 5/13/2003 6/3/2003 5/20/2003 5/27/2003 6/10/2003 6/17/2003 6/24/2003 DATE

KIN-BUC LANDFILL GROUNDWATER HYDROGRAPH #14 TRANSECT No.4- INSIDE **VERTICAL GRADIENT** -7R --78 3.5 3 GROUNDWATER ELEVATION (FT) HEAVIER WEIGHT DENOTES BEDROCK WELL 0.5 0 -4/1/2003 | 4/8/2003 4/29/2003 5/6/2003 4/15/2003 6/3/2003 4/22/2003 5/13/2003 5/27/2003 6/10/2003 6/17/2003 6/24/2003

DATE



ATTACHMENT 2



IT Corporation

Crossroads Corporate Center One International Boulevard, Suite 700 Mahwah, NJ 07495-0086 Tel. 201.512.5700 Fax. 201.512.5786

A Member of The IT Group

June 27, 2001 Project 796201

Carl Januszkiewicz
Waste Management, Inc
Kin-Buc Landfill Treatment Plant
383 Meadow Road
Bdison, NJ 08817

Re: Evaluation of Head Levels at Transect 1

Dear Mr. Januszkiewicz:

We have completed an evaluation of the hydraulic characteristics at Transect 1 with specific focus on the lack of intragradient conditions associated with the high water levels in W-1G (inside of the slurry wall) relative to those levels in W-2G (outside of the wall).

While intragradient conditions were evident at the outset of the hydraulic monitoring program in April 1996, these conditions have generally not been maintained. Specifically, based on a review of historical hydrographs, intragradient conditions were evident initially from approximately April to July 1996, and April to June 1997. Thereafter, to more recent events, intragradient conditions have been observed intermittently and for shorter periods of time.

Attachment 1 presents a hydrograph at Transect 1 encompassing the period from September 1998 to December 2000. As seen on the hydrograph, there were periods of time when intragradient conditions were not being maintained.

As opposed to the other "G" series monitoring wells that are located in refuse, wells 1G and 2G at Transect 1 are actually located in a silt and clay deposit. Attachment 2 contains the boring logs for these 2 installations. In-situ hydraulic conductivity testing performed at Transect 1 indicated permeabilities of 10⁻⁷ cm/sec and 10⁻⁵ cm/sec in W-1G and W-2G, respectively. Accordingly, a source of recharge to the overburden soils in the area of W-1G would not readily drain away, and therefore, higher heads could result.

Well 1G sampling events (November 1998, October 1999, October 2000) can be seen on the hydrograph as sharp vertical drops in groundwater levels. Due to the low permeability of the surrounding materials, the groundwater levels required several months to recover. Since the final cover extends 10 feet past the slurry wall, the source of the groundwater that is recharging W-1G is unknown at present.

The hydraulic gradient between W-1G and W-1R is vertically downward which rules out the bedrock as being a source of groundwater recharge. Based on a recent visual inspection of the area around Transect 1, the cap appears to be good condition and there were no signs that the cap integrity has been compromised.

Figure 1 depicts the conceptual model of the hydraulic interrelationship across Transect 1 showing water level measurements that depict the lack of intragradient conditions across the

Carl Januszkiewicz June 27, 2001. Page 2

Project 796201

slurry wall. The head levels in W-2G (outside the slurry wall) are generally at elevation 12 to 13 feet msl with periodic and short term increases to about 15 feet msl. The water level in the well sometimes falls below the level of the transducer. This is characterized by a flat straight line on the hydrographs as shown on Attachment 1. Head levels in W-IG (inside the slurry wall), on the other hand, are often greater with elevations as high as 15 to 16 feet msl being

It is evident from a review of Pigure 1 that the drop in topography outside of the slurry wall toward Mill Brook, coupled with the higher permeability of W-2G relative to W-1G, would promote a more rapid decrease of head levels in the latter. This suggests that intragradient conditions may not be consistently attainable at this transect in any event. notwithstanding however, and as depicted on Figure 1, it is important to note that the leachate collection system represents a hydraulic sink within the containment system. As such, groundwater in the vicinity of W-1G would drain toward the sink mitigating concerns of

The leachate collection line runs parallel to the slurry wall and at its closest point is only about 20 feet away from Transect 1. Several cleanouts are located along the collection line with the closest, Cleanout 16, only about 65 feet from Transect 1. Leachate level measurements obtained from the cleanouts during December 2000 and June 2001 indicate a leachate level of 10 to 11 feet msl along the collection line as shown in Table 1. The leachate levels observed suggest that the leachate collection system is presently operating effectively.

Recommendations

Based on the above, it is recommended that during subsequent monitoring events at the site, measurements of leachate levels in Cleanouts 14 through 16 be recorded to verify that the leachate collection system is operating effectively. If liquid levels in the cleanouts increase above 12 to 13 feet msl, then maintenance of the collection line is recommended. Subsequent reports to EPA should include a discussion of the leachate collection system and its role as serving as a hydraulic sink within the containment system.

We trust you find this information useful. If you have any questions, please do not hesitate to

Sincerely,

IT Corporation

Steven Goldberg, Ph.D, CPG

Senior Hydrogeologist

Thomas M. Connors, P.E.

Project Manager

Attachments

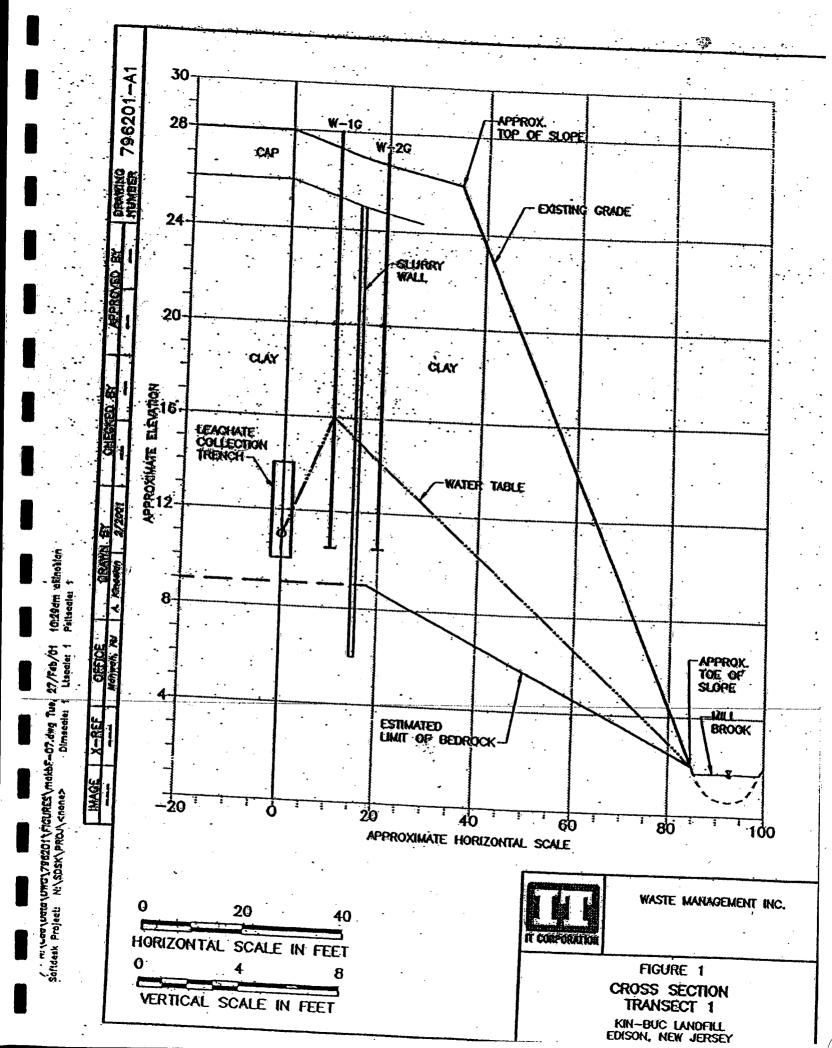
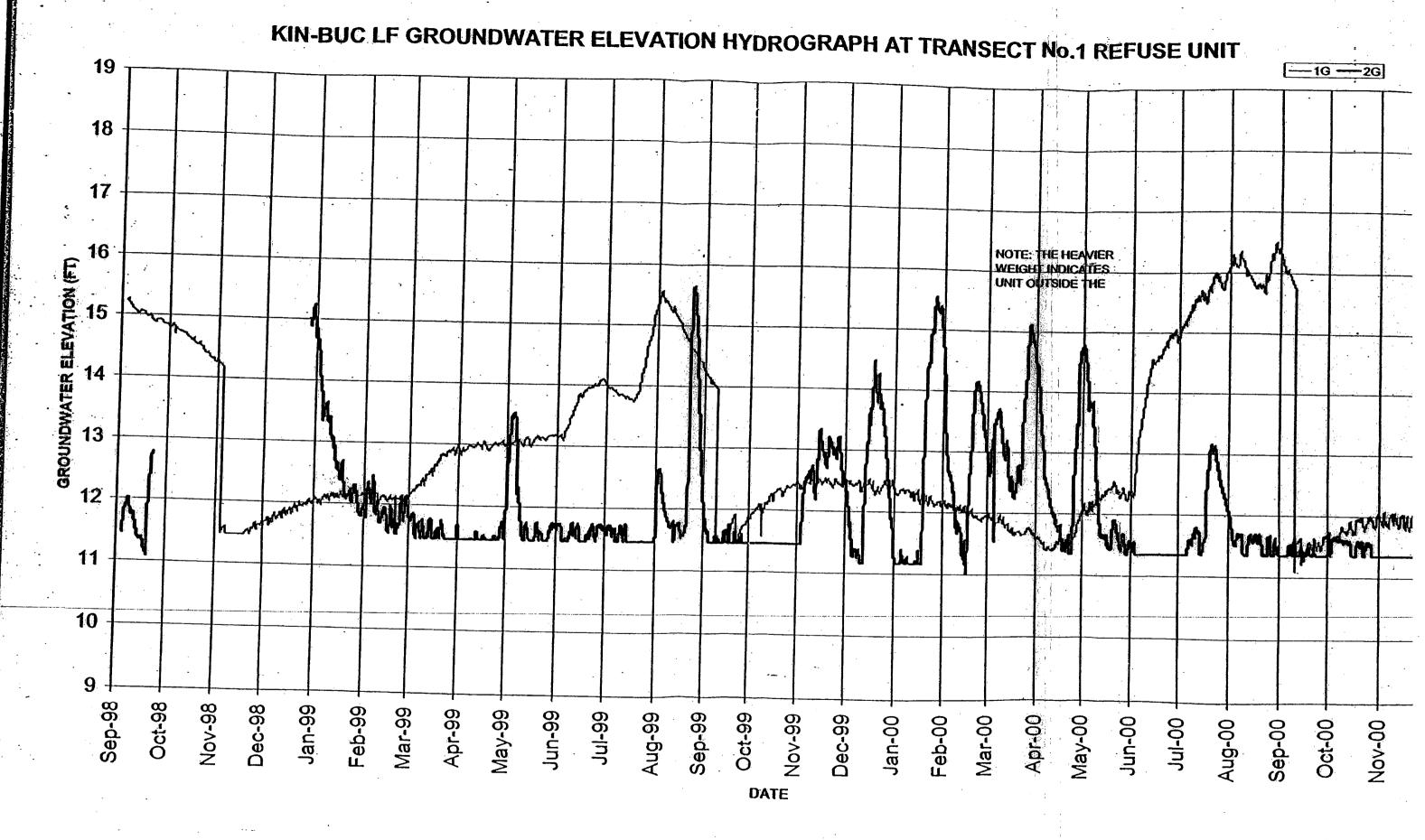


Table 1 Kin-Buc Landfill Leachate Cleanout Monitoring 2001

| leanout location levation @ Sea Level | | 14N | | 4E | | SN | | 100 | | | * • | • |
|--|----------|------------|---------------------------|--------------------|------------------|----------------|----------|-------------|-------------------|-----------|--------------------------------|-------------------|
| | depth to | 2.87 | . 22 | 2.7.7 | | 6.51 | | 16E 6.51 | | 16N | | IEE |
| | Water | 1 | depth to | ľ | depth to | | depth to | | 3 | 1.36 | 3 | 1.32 |
| evation Average | 174401 | elevation. | water | elevation 10.74 | Water | elevation | water | elevation | depth to water | elevation | depth to water | |
| DATE | How May | | | | | 10.66 | | 10,67 | | | | elevation 11.11 |
| 0/2/04 | | | and the same and the same | Resident Const. | | | | | | | | |
| 6/7/01 | 11.98 | 10,89 | 12.02 | 10.75 | 15.86 | 40.05 | | | | | tion and all the second second | ki Nisa Mahiki ka |
| 5/16/01 | 12.25 | 10.62 | 12,23 | 10.54 | 15.96 | 10.65 | 15.87 | 10.64 | dry: | na | dry | na |
| 4/26/01 | 12.36 | 10.51 | 12,35 | 10.42 | 15.99 | 10.55 | 15.96 | 10.55 | dry | na | dry | na |
| 3/21/01 | 11.80 | 11.07 | 11.75 | 11.02 | 15.62 | 10.52 10.89 | 16.01 | 10.50 | dry | na | dry | na |
| 2/26/01 1/29/01 | 12.03 | 10.84 | 11.94 | 10.83 | 15,95 | 10.89 | 15.59 | 10,92 | dry | na | dry | na |
| | 12.08 | 10.79 | 11.98 | 10.79 | 15.85 | 10.66 | 15,92 | 10.59 | dry | na | dry | na |
| 12/27/01 | 12.02 | 10.85 | 11.94 | 10.83 | 15.72 | 10.79 | 15.83 | 10.68 | dry | na i | 20.41 | 10.91 |
| | | | | | 10.12 | 10.79 | 15.68 | 10.83 | dry | na | 20.01 | 11.31 |
| | | | • | | | | | | | | | |
| | • | | | | | | | | | | | |
| | | | · · · · | | - - | - | | | | | | <u></u> |
| | | | | | | | | | | | | |
| | | | | | · | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | • |
| | | | | | | | | | | | | |
| | | | | | | | | <u> </u> | | | | |
| | | | | | | | - | | | | | |
| | | | | | | | | | | | | |
| | | . | | | | - | | | - | | | |
| | | | | | | | | | | | | |
| | | | | | | | - | | | | • | |

ATTACHMENT 1



ATTACHMENT 2

MONITORING WELL RECORD

| OWNER IDENTIFICATION - Owner | | • | Well Permit No Atlas Sheet Co | pordinates | 25 : <u>45</u> : 428 |
|---|--------------------------------|--------------|----------------------------------|--------------------|--|
| Address. | "_KIN_BIC_INC | | <u> </u> | | |
| City | 200 CENTRALAL | AVE. | | | · · · · · · · · · · · · · · · · · · · |
| City | PISCATAVAY | | State | NJ | |
| WELL LOCATION - If not the same | | | - · · | | Zip Code |
| County | as owner please give add | ress. (| Dwner's Well N | lo. 20 | ; |
| Address 383 Meadows Ro | ad Edding ED | SOU-THP | | Lot No. | Direct M |
| Address 383 Headows Ro TYPE OF WELL (as per Well Permit | - s carson, NJ | | A | | -499 - DOCK NO |
| TYPE OF WELL (as per Well Permit Regulatory Program Requiring Well | Categories) Masselbonson | | 0.4 | | |
| Requiring Well | CERCIA | | _ Uake | well comple | ted 2 , 15 , 95 |
| Regulatory Program Requiring Well CONSULTING FIRMFIELD SUPER | /ISOR (if soplicable) | | Case | LD.# | NJDØ4996Ø836 |
| WELL CONSTRUCTION | | | ·: | | Tele. # |
| Total depth drilled 15.6. II. | | Depth to | Depth to | | |
| Wolf 6224 4 | | Top (ft.) | Bettomte | Diamete | Tama and as |
| Well finished to 15 ft. | | from to | nd sudace | (sucites) | Type and Material |
| orehole diameter: | Inner Casing | +4 | 5 | 2 | Sch 40 PVC |
| Top 8 in. | Alor Duter Casing | - | | | sea do Pac |
| Sottem 8 in. | (Not Protective Casing) Screen | | | | |
| ell was finished: Above grade | (Note slot size) | .5 | 15 | 2 | |
| flush mounted | Tail Piece | | | | Sch 40 PVC .010 |
| inished above grade casion | | | | | · |
| gni (Stick up) above land | Gravel Pack | 3 | 15.6 | 8 | 400 m |
| lace 4 fi. | Annular Seal/Grout | 0 | 3 | | #00 Ricci |
| s steel protective casing installed | Method of Growing | tremie | | 8 | Bentonite slurry |
| res FRINO | | cremie | | | |
| ic water level after drilling | • | · . | | /D : | |
| er level was more and | • | GEO | LOGIC LOG | (Copies geophys | of other geologic logs and/ ical logs should be attache |
| was developed for N/A hours | at N/A gpm | 1 | | | ALPRINE BO CHOOL SECTION |
| rod of development N/A | Spm | | 0 - 15.6 | 1 | ed dry stiff clay |
| permanent pumping equipment insta | | <u> </u> | | | ome silt |
| capacity N/A gom | Med? Yes X No | 1 | | | |
| type:N/A | · • · | • | | | • |
| g MethodHSA | | | | | |
| a Elvid | <u>-</u> | 1 | • • | | |
| of Driller Chad Chism | RigB-61 | | | | |
| and Salaty Blooms | | | | | . (|
| of Protection was a submitted? | es X No | | , | | • |
| of Protection used on site (circle one) cense No. 0013753-001375 | None D C(B) A | | | | • |
| | | 1 | | • | • |
| of Oniting Company HARI |)IN-HUBER, INC. | . | | • | |
| that I have drilled the above-rele ules and regulations. | renced | | | | |
| ules and regulations. | renced well in accorda | nce with all | well permit a | equiremen | Is and all annihing to |
| | | • | | 4 | - and an abhicable |
| Driller's Signature | 0/ /0 | 21: | • | | |
| ormer a signature | | 24 | | | |
| COPIES: White | - Sedly | Elsa | 6 | Date | 2/15/95 |

MONITORING WELL RECORD

| | | - 1 | Well Permit Ho Atlas Sheet Co | 25 | 771 |
|--|--------------------------------------|---|----------------------------------|-------------------|--|
| OWNER IDENTIFICATION - Own | INTER THE THE THE | • • | | CONTRACTOR _ | 25 : 45 : 428 |
| Address | 200 COMPONIAL | 4200 | | | |
| City | PISCATAVAY | AVB. | | | |
| | | | _ State _ | NU | Zip Code |
| WELL LOCATION - If not the same | e as owner please give add | mee . | Brown and a Martinet as | | |
| County | Municipality | | Owner's Well N | 10. <u>IG</u> | |
| Address 383 Headows R | oad Edison, NJ | SON THE | | Lot No | _423 Block No |
| THE OF WELL (as per Well Permi | Colomatics | | | | |
| Regulatory Program Requiring Well | MONITORIN | | _ Date | well comple | ted 2 / 15 / 95 |
| CONSULTING FIRM FIRM OF STREET | - CERCIA | | Case | LD.# | N.110049860836 |
| CONSULTING FIRMFIELD SUPER | (VISOR (il applicable) | , , , , , , , , , , , , , , , , , , , | | | Tole # |
| MELL LONSTHUCTION | | | / | | Total |
| Total depth drilled 15.6 t. | | Depth to Top (ft.) | | Diamete | |
| Well finished to | | from k | Bottom (it. | (inches) | Type and Material |
| Borehole diameter: | Inner Casing | +6 | | | |
| Top8in. | Outer Circina | | 5 | 2 | Sch 40 PVC |
| Bottom 8 in | Outer Casing (Not Protective Casing) | |] | | |
| Well was finished: 🗓 above grade | (Note slot size) | | 1 | | |
| I flush mounted | | _5 | 15 | 2 | Sch 40 PVC .020 |
| finished where we to | | | | | |
| f finished above grade, casing leight (stick up) above land | Gravel Pack | 3 | 15.6 | 8 | #2 Ricci |
| urlaceft. | Annular Seal/Grout | | | | N.S. WTGGT |
| as steel protective casing installed | | 0 | 5 | 8 | Bentonite slurry |
| Yes KX No | Method of Grouting | tremi | e . | • • | |
| tatic water level after drilling | | | | | |
| ater level was measured using | n. | GEO | LOGIC LOG | (Copies Geophy | of other geologic logs and/o ical logs should be attached |
| ell was developed for N/A hour | N/A | | • | | A SUGGIO DA SUSCIONA |
| thod of development N/A | rs at N/A gom | | 0 - 15.6 | | · |
| as permanent purpose as | | | U - 13.6 | . ; | red gray dry stiff |
| is permanent pumping equipment ins mp capacityN/A _ com | talled? Yes Y No | ·· | | | clay, some silt |
| Mo to a second | | | | | |
| | · · | 1 | | | |
| ing Child | | | | | |
| Type c | 1 Rig B-61 | _ | | | |
| | | | | | |
| hith and Salety Plan submitted? | Yes X No | -1: | | • | . ` |
| el of Protection used on site (circle one | None D CBA | ı | | | |
| | | | | | |
| e of Drilling Company HA | RDIN-HUBER, INC. | 1 | | | • |
| ify that I have drilled the above-re rules and regulations. | lerenced well in accorda | nce with al | l well permit : | requiremer | ils and all apate. |
| | | | | - dan oueg | and an applicable |
| Driller's Signatur | | 2, ·. | | | |
| - 3;14(0) | - wind | Zasa | | Date | 2/15/95 |
| COPIES: White | | | | | |

Ly Cramsin

Date: 4-7-03

| , <u> </u> | START Prior to Well Field Adjust | END Affortation Finish Annual |
|-----------------|----------------------------------|----------------------------------|
| FLARE TEMP | 1508 | After Well Field Adjust |
| FLOW(CAL) | 120 | /5-/0 |
| CHy CO2 O2 | 42.6cm, 28.6cm, 4.10. | 114 44.044, 28.8co, 3.60, |
| Pressure n | 1.0 | 1, 13 |
| Vacuum I | -7.60 | - 7.50 |
| NET CH TEMP | 40 | 40 |
| | | 70 |
| | | |
| | | |
| | | |
| 6 | | |
| mp | 42 | |
| | | 38 |
| me varoury | 16 apl | |
| NO DECOM | .58 | 16 m/L |
| Limerer | 28.9 | 5.5 |
| OVENU CONDITION | Wer/Snaw | 28.9 |
| | WEI / SNEW | Wor/swow |
| | | |
| | | |
| | | |

No : Loy Commence.

Date: 4-21-03

| | START Prior to Well Field Adjust | END After Well Field Adjust |
|---------------|----------------------------------|---------------------------------------|
| FL. | 1214 | 15-18 |
| FL . (C | 142 | 147 |
| वः वट | 45.4 cm 31800 2.100 | 46.8 ay 32.5 con 2.002 |
| Pre une in. | 10 | 1.0 |
| Va | 7.5 | 7.5 |
| in. C | 54 % | 56 °F |
| BC JE | | |
| 1 | | |
| Ei | | · · · · · · · · · · · · · · · · · · · |
| T W | | |
| N: in | | |
| E | 65 % | 68.4 |
| T | | |
| v : . | 8 4 | 8 mgL |
| v i is | 58 | 25 |
| F . ER | 30./ | 30./ |
| | Sky | They |
| :: | | |
| | | |
| ··- | · | |

| None Roy Codewoux, | Date: |
|--------------------|-------|
|--------------------|-------|

| Date: | 5-5 | ·o <u>3</u> | |
|-------|-----|-------------|--|
|-------|-----|-------------|--|

| | START Prior to Well Field Adjust | END After Well Field Adjust |
|--------------------|-------------------------------------|--------------------------------|
| RAKE TEMP | 1530 | 1520 |
| Pless (apm) | 118 cm | 115 da |
| CHY, COL, OZ | 44.8 32.6 1.502 | 12.9 al 3/5 as 2.6 oz |
| ALEBURE (IN. W.C.) | / ,0 | /.0 |
| Vacuum (in. in.) | 8.3 | 8.8 |
| INLET GAT TEMP | 54 04 | 54.k |
| AN. | | |
| AN. | | |
| | | |
| , 1G | | |
| Temp | 56 % | 56 'F |
| | | |
| JIME SPECK | of mych. | 4 m/L |
| WIND DIRECT | W | l ω |
| Adometra | 30.2 | 30.7 |
| | | |

Name: Roy Carmasine

Date: 5/19/03

| | START Prior to Well Field Adjust | END After Well Field Adjust |
|------------------------------------|--|--|
| FLARE TEMP (F) | 1530 | 1527 |
| FLOW (clm) | 110 | 107 |
| CH4, GO2, G2 (%) | 45.4, 36.1, 0.3 | 48.0, 38.0, 0.3 |
| Pressure (in, w.c.) | 1 | 1 |
| Vacuum (-in.w.c.) | 11.5 | 10.5 |
| INLET GAS TEMP (F) | 72 | 80 |
| BLOWER AMP 1 | | |
| BLOWER AMP 2 | | |
| BLOWER HOUR 1 | | aran da kasa da katama da aran kanya aran da karan ya da da aran da da aran da d |
| BLOWER HOUR 2 | <u>a ann an t-ann an t-a</u> | the state of the s |
| WEATHER GEN | | |
| TEMP (F) | | <u></u> |
| HUMIDITY (%) | | |
| WIND VELOCITY | 4 mph | 4 mph |
| WIND DIRECTION | E | £ |
| SAROMETER | 30.4 | 30.4 |
| GROUND CONDITION Wet, Frozen, Dry) | dry | dry |

| NOTES: | | · · · · · · · · · · · · · · · · · · · | · · · · · · · · · · · · · · · · · · · |
|--------|-------------|---------------------------------------|---------------------------------------|
| | | | |
| | | | · |
| | | • | • |

Name: Roy CARLUASINE

Date: 6-3-0 3

| | START Prior to Well Field Adjust | END After Well Field Adjust |
|--|-------------------------------------|--------------------------------|
| FLARE TEMP (F) | 1570 | 15 28 |
| FLOW (cfm) | 111 | 109 |
| CH4, CO2, C2 (%) | 39. lay, 6.102, 27.000 | 39.2 cm , 5.102 , 28.4 coz |
| Pressure (in. w.c.) | 1.0 | 40 |
| Vacuum (- in, w.c.) | -115 | -11.2 |
| NLET GAS TEMP (F) | 60 °F | 62 °F |
| BLOWER AMP 1 | | |
| BLOWER AMP 2 | | |
| BLOWER HOUR 1 | | |
| BLOWER HOUR 2 | | |
| WEATHER GEN | | |
| TEMP (F) | 66.7 | 66°F |
| HUMIDITY (%) | | |
| WIND VELOCITY | 8 mpl | 874 |
| WIND DIRECTION | W | W |
| BAROMETER | 30.02 | 30.02 |
| GROUND CONDITION (Wet, Frozen, Dry) | Wes | WET |

| NOTES: | |
|--------|--|
| | <u>,, in the second of the secon</u> |

Name: Roy Galuinsini

Date: 6-16-03

| START Prior to Well Field Adjust | END After Well Field Adjust |
|----------------------------------|--|
| 1510 | 1507 |
| 1/2 | 127 |
| 41.0, 28.6, 5.1 | 44.3 , 30.8 , 3.0 |
| 1.0 | 1.0 |
| -11.5 | - 11.5- |
| 68 % | 72 % |
| | |
| | |
| | |
| | |
| | |
| 66 °F | 744 |
| | |
| 6 mph | 6 mg/L |
| 58 | 25 |
| 30.3 | 30.3 |
| WEF | Ver |
| | Prior to Well Field Adjust 15/0 1/2 4/.0, 28.6, 5.1 1.0 -1/.5 68 % 6 mph 5 £ 30.3 |

NOTES: _____